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LARGEST PRODUCERS OF OXYGEN IN THE WORLD

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AR stimulates the invention of destructive devices and promotes the adaptation of machines to offensive purposes for which they were not originally The importance of road transportation in times of war and peace warrants the presentation of this article on the design and construction of the Holt Mfg. Co.'s caterpillar tractor, which is the foundation of the British and French "tanks," and in many respects the most remarkable machine ever developed for any purpose.

planned. One of the strange developments of the European struggle is the so-called "tanks," those lumbering land battle-ships, invulnerable to machine-gun fire, that travel over ground plowed by shells, and cross ditches, crawl up precipitous banks, push down walls, and accomplish that which would be impossible for any of the four-wheel type motor trucks. The tanks are adaptations of an American invention, being reconstructed caterpillar tractors built in the United States and invented by Benjamin Holt, president of the Holt Mfg. Co., of Stockton, Cal., and Peoria, Ill.

Benjamin Holt was born in New Hampshire and had New England thrift and native Yankee inventive ability. He went to California in the early eighties, and with his brothers established a factory at Stockton for building wagons and farm implements. The vast agricultural areas, the forests and the great mines of the Pacific coast all demanded new methods of farming, lumbering and mining. Twenty-five years ago Mr.

Holt invented the Holt combined harvester and thresher, which cuts and threshes the grain at one operation. This machine quickly came into extensive use in the Pacific coast states. Mr. Holt then began the manufacture

of steam traction engines for pulling gangs of plows and other tillage implements, but these engines were only partially successful, as the soft lands of the San Joaquin valley could not support the weight, although driving wheels were built as large as eight feet wide and twelve feet diameter. These were too heavy and cumbersome and did much damage to the surface traversed. Then realizing that the reason for using such enormous driving wheels was simply to obtain the projected area on the ground required to support the weight, Mr. Holt, in 1904, discarded the large-diameter, wide-tire wheels and designed a virtually flat wheel in the form of an endless sectional track which the tractor first lays down, rolls over and then finally picks up one section at a time, thus giving a solid steel road-bed to travel on. The belts were provided with guide wheels similar to an animal tread power, and, in fact, the driving elements or track assemblies are identical in principle with tread powers; they are laid on the ground

'The term "Caterpillar" used throughout this article is copyrighted, and has reference only to the tractor made by the Holt Mfg. Co.



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per unit horse-

power. The 75-

horsepower trac-

tor is driven at

two speeds, either

21/8 and 3, or 11/2

and 21% miles per

hour. The slow

speeds, of course,

give the greatest

tractive power

and are used in

heavy pulling.

When climbing a

bank or getting

out of a mud-hole,

the operator uses

the\_ multiple-disk

master clutch to increase the trac-

tive power mo-

mentarily. He lets

the engine speed

up and then jams

in the clutch, thus utilizing the in-

ertia of the fly-

wheel and obtain-

and pushed by engine power instead of being pushed by animal The enpower. gine drives through sprocket wheels, which engage the links of the belt or chain. This form of driving element can be proportioned to give almost any required area to support the load, and it was found to have certain other valuable characteristics not possessed by the traction engine. It not only had great tractive power, but could maneuvered much more easily. It is possible to turn a caterpillar

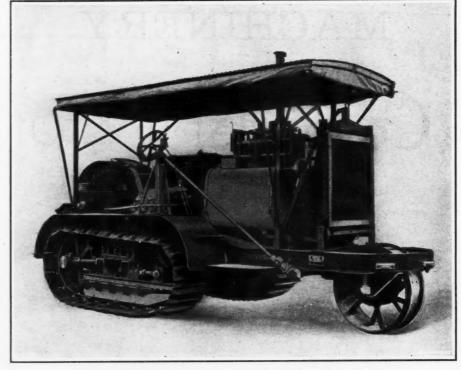


Fig. 1. Seventy-five-horsepower Internal-combustion Motor Caterpillar Tractor

would stop any wheel vehicle. The reason for the latter is that the belts bridge narrow ditches and support the engine without dropping in and having to climb out. If the ditch is broad, the great tractive power enables the machine to cross even if the sides are inclined at as steep an angle as 45 degrees.

The Holt Mfg. Co.'s caterpillar tractors are built in four sizes, viz., 18, 45, 75 and 120 horsepower. The 18- and 45horsepower sizes have no pilot or leading wheel. The larger sizes with greater power and a longer wheel-base are employed for heavy hauling, as well as for agricultural work, having power sufficient for pulling large gangs of plows or several loaded trailers, doing construction work and other labor requiring great tractive power. The 75-horsepower tractor weighs 24,000 pounds and develops a draw-bar pull of 9000 pounds; the 125-horsepower tractor develops 12,000 pounds draw-bar pull.

The tractors are equipped with internal combustion fourstroke cycle engines with four and six cylinders. The sixcylinder engines are used on the 75- and 120-horsepower tractors, while the 18- and 45-horsepower sizes have four-cylinder engines. The 45- and 75-horsepower motors are built in the Stockton plant, and the Peoria plant is devoted princi-

pally to the construction of the frames, track assemblies, clutches, transmission gears. and all the other principal parts. A few six-cylinder engines with certain special features for military tractors are built in the Peoria plant. The general design of the engine does not differ radically. however, from that of the engines for motor trucks except in general ruggedness and strength, being comparatively slow speed and heavy

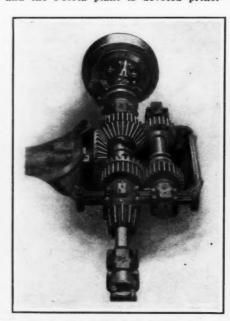


Fig. 2. Master Clutch and Transmission Assembly of 75-horsepower Tractor

ing a tremendouswithin its own length and to traverse broken ground that ly increased tractive power momentarily. It is because of the peculiar features of the driving gear and the low unit pressure of the tractor on the earth that the Holt caterpillar can cross gullies, plow through mud, and pull a load where other tractors would be practically helpless.

The control of the Holt tractor is different from that of the ordinary motor truck. On the 45-horsepower tractor the operator's seat is at the rear, where he has at his hand and feet three clutches to operate, two for steering and one-the master clutch-for controlling the transmission of power from the engine to the driving gear. The master clutch must be pressed into engagement by the operator when he wishes to drive, instead of employing the pressure of a coiled spring, as in the transmission of the ordinary motor car. The two steering cone clutches are located in the jack-shaft. To turn the tractor to the right, the operator releases the right-hand clutch partially or entirely, depending on the shortness of the turn required, and drives with the left-hand clutch, causing the machine to curve to the right. If a very short turn is to be made, the right-hand clutch is fully disengaged and the brake applied to the clutch drum, thereby locking the driving gear on the right-hand side and causing the machine to pivot on the

> center of the righthand track assembly. Thus it is possible to turn the tractor easily within its own length.

Caterpillar tractors are manufactured, but all the parts are not made strictly interchangeable, although they are practically so. For instance, the bearings for the transmission shafts are babbitted with babbitting jigs and are afterward reamed. scraped and fitted to their respective shafts, thus securing close fits,

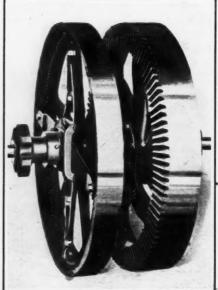


Fig. 3. Main Drive Gear and Friction Wheel

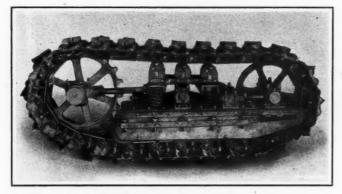


Fig. 4. Track Assembly of 75-horsepower Holt Caterpillar Tractor

smooth action and durability. When replacements are necessary, some refitting may have to be done. The frame is bent to shape over forms and the bearing castings are set, the holes are drilled and then reamed in position. The general practice is the same as that followed by locomotive builders. The effort is to secure a strong, well-knit construction that will withstand indefinitely the shock and wear of use.

Cut gears are used throughout the transmission. The bevel gears are planed on Gleason bevel gear templet planers. Great

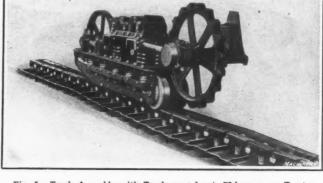


Fig. 5. Track Assembly with Track opened out, 75-horsepower Tractor

eral thousand pounds and that propels the machine under the most severe deteriorating influences is an accomplishment worthy of the highest commendation. The structure is made to exclude dirt to a considerable extent, but it works without trouble or rapid wear when submerged in mud or sand.

The steel track of the caterpillar is composed of links, connected by casehardened pins and bushings, and plow steel plates pressed into shape while hot. Each link is a double rail over which the track rollers revolve. A plow steel plate



Fig. 6. Machine Shop of Holt Mfg. Co., Peoria, Ill.

care is exercised to obtain perfect alignment of engine crank-shaft bearings, the boring being done on Lucas horizontal machines.

The working parts of the caterpillar that excite the liveliest interest in the mechanic are the track assemblies. In these we have a mechanism exposed to dust, sand, mud and water, while working under heavy stress. To have designed and constructed a flexible steel track that sustains a load of sev-

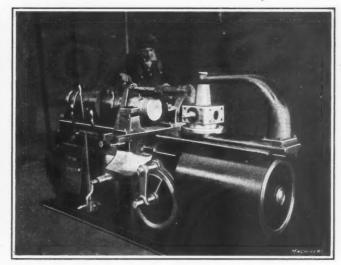


Fig. 7. Potter & Johnston Automatic Lathe turning Pistons

of high tensile strength is attached to each link. The plates have curved ends and overlap, so there is no opening between them in any position. They are made sufficiently heavy to withstand severe use and, owing to the design and materials used in construction, are extremely durable. There is little or no friction between the plates and the ground, the track being merely laid down and picked up again, one section at a time.

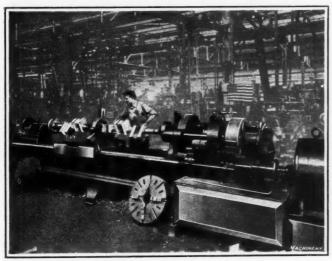


Fig. 8. Turning Six-throw Crankshafts for 120-horsepower Engine

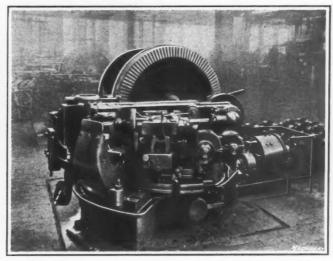


Fig. 9. Gleason Templet Gear Planer planing Bevel Main Drive Gears

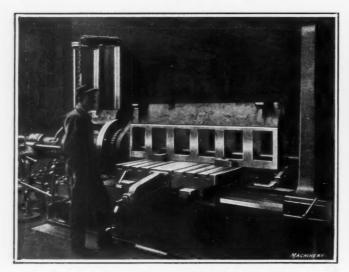


Fig. 10. Lucas Horizontal Milling and Boring Machine boring Bearing for Six-cylinder, 126-horsepower Crank-cases

The extraordinary capacity of the caterpillar to travel over soft ground is due in large part to the low unit pressure imposed on the supporting track. There are usually eight track links or shoes on each track of a 45-horsepower tractor in contact with the ground, so that with the standard 13-inch width tracks the total bearing surface is 2080 square inches and the ground pressure is only 6½ pounds per square inch. For very soft ground, special 30-inch width tracks are provided, giving a total bearing surface of 4800 square inches and reducing the ground pressure to 3 pounds per square inch, or 432 pounds per square foot. This pressure is much less than the foot pressure of either man or horse; hence it is obvious that

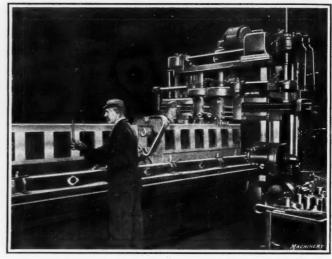


Fig. 11. Ingersoll Milling Machine working on Crank-case of Six-cylinder, 120-horsepower Engine and Radiator Headers simultaneously

the heavy tractor can work over soft soils, and will pack the ground less than horses.

The load is transferred on each side of the 45-horsepower caterpillar to five truck wheels or rollers, spring-supported beneath the main frame. The driving sprocket is at the rear and small rollers are provided at the top for supporting the chain as it travels to the blank sprocket or idler at the forward end. The truck rollers have chilled faces and revolve on heat-treated shafts fitted with long phosphor-bronze bearings provided with grease cups. The hubs are counterbored to receive washers that are ground to size. The washers act as a thrust bearing and exclude dust, sand and dirt.



Fig. 12. Main Erecting Shop of the Holt Mfg. Co., Peoria, Ill.



Fig. 13. Babbitting Jig used for Bearings of 75-horsepower Tractors

The gasoline tanks are made of galvanized sheet steel, rolled and spot-welded closely at the seams. The heads are formed with shallow flanges and set in place with the flanges outward in the spot-welded shell. The heads are closely spot-welded to the shell and then all seams are soldered. The spot-welding process of uniting the seams is rapid and effective; the spot-

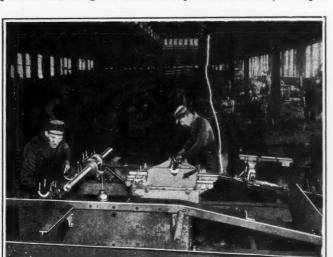


Fig. 15. Scraping Bearings for 75- and 120-horsepower Tractors

welds give the seam the necessary strength to hold and the solder seals the joints.

All tractors are subjected to a shop test of several hours' duration, running under brake load, to tune them up and get the bearings broken in. After the brake test, each tractor is taken out and driven about under heavy load until the operator is satisfied that it is fit for average road conditions.

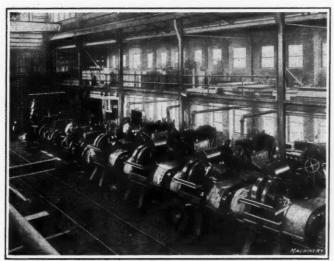


Fig. 17. Holt Caterpillar Tractors undergoing Shop Test on Blocks

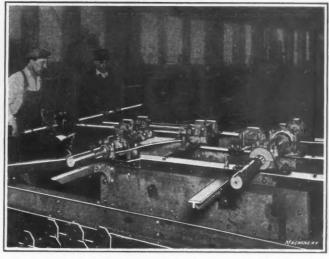


Fig. 14. Power Reamer for reaming Bearings on 75-horsepower Tractor

Motor trucks and tractors are being widely used in the European war for hauling in place of horses. The movement of great guns and supply trains with the speed and rapidity accomplished would have been out of the question if the armies had to depend on horses. The extent to which mechanical traction is used is indicated in a manner by the fact that the

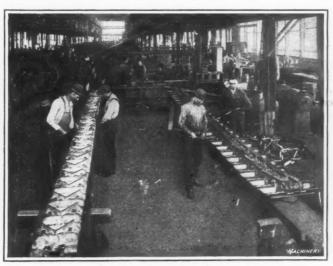


Fig. 16. Assembling Tracks for 75-horsepower Tractors

Holt Mfg. Co. has sold over three thousand caterpillar tractors to the European countries, chiefly Great Britain and France. The advantages of motor-driven tractors are greater concentrated power than is possible with horses, freedom from disease, smaller number of men required to drive and care for them, capacity to travel continuously over rough roads, and possibility of being restored to use when damaged by shells.



Fig. 18. Seventy-five-horsepower Tractor, hauling Supply Train in Texas



Fig. 19. Seventy-five-horsepower Tractor crossing Deep Gully on Expedition





Fig. 21. Holt Caterpillar having crossed Gully and ascended Opposite Bank

In view of the advantages of mechanical traction, particularly as shown in the European war, the United States Army has made an exhaustive study of the general problem of haulage and military supply trains. These tests began in 1915 and have steadily continued; they have included all the various field operations of the Quartermaster Corps, Engineers' Corps, light and heavy Field Artillery, Signal Corps, etc. Caterpillar tractors were found indispensable in building and maintaining roads for the motor truck trains during the expedition into Mexico in 1916; they are being used for hauling supply trains through the Big Bend District, Texas, where the troops guarding the Rio Grande boundary are from sixty to one hundred miles from the base of supply at Marfa. The Big Bend District consists principally of steep, rough mountain grades and desert roads. For the first time in the history of the United States Army, tractors were used in March, 1917, for hauling supplies in connection with marching troops. The initial trip was made from Fort Sam Houston to Laredo, a distance of 170 miles, where caterpillar 75-horsepower tractors accompanied the 37th Infantry, and after reaching Laredo, made the return to Fort Sam Houston with the 9th Infantry. It was necessary for the tractors at all times to maintain the speed of the marching regiment, so as to make camp each day on time with the regimental supplies. Although many severe road conditions were encountered, the tractors successfully met all requirements without mishap or breakage. Fig. 18 shows the supply train accompanying the 37th Infantry, consisting of fifteen Troy trailers, fourteen of which were of 11/2 ton capacity and one of 3 tons capacity. The total weight of the trailers is 15 tons and of the cargo 30 tons, making a net hauling weight of 45 tons. One of the regular army escort wagons was later added, making the total hauling weight 53 tons. It would have required thirty army escort wagons with four mules each to handle this same tonnage.

Tractors are formidable in war, but they will achieve greater victories in times of peace. There is no doubt that agricultural work on large farms of the West and on many of the smaller farms of the East will eventually be done almost exclusively by means of tractors, and this, of course, applies also to agricultural work in all the countries of the world. The machine that has great pulling power, which can be used on soft soils and turn within its own length is at an advantage as compared with those requiring a large turning radius and firm soils to work efficiently for purely agricultural purposes. For long overland hauling, especially where bad roads exist, the caterpillar tractor has proved capable of hauling at a lower cost per ton mile than by other methods. For road hauling where greater speed is required and comparatively small tractive power is needed by reason of uniformly good roads, the four-wheel motor truck has some advantage, but no wheel vehicle can follow the caterpillar type tractor through muddy, sandy and rough roads or over steep grades or where no roads of any kind exist.

The by-products of the 48,000 sawmills in the United States, in the form of sawdust, shavings, slabs, etc., is estimated at 36,000,000 cords a year. About one-half of this is used as fuel, but the remaining 18,000,000 cords is a source of danger to the mill and requires the expenditure of time and money for its disposal. As the production of this waste is unavoidable, the forest service is seeking some way of turning it to account.

# INDUSTRIAL EXPOSITION AND EXPORT CONFERENCE

The first annual Industrial Exposition and Export Conference of the allied industries of the United States was held at the Eastern States Exposition Grounds, Springfield, Mass., June 23 to 30. The purpose of this exposition and conference is to develop export opportunities for American manufacturers and to discuss problems incident to the supplying of foreign markets with American goods.

Thursday, June 28, was "Metals Day," and at the morning session, presided over by Charles E. Hildreth, general manager of the National Machine Tool Builders' Association, the following papers were presented:

"After the War—What of Machinery Export?" by C. O. Smith, Export Manager, Norton Grinding Co., Worcester, Mass. "American Tools in Foreign Markets," by Oren O. Gallup, New York City Export Manager, Simonds Mfg. Co., Fitchburg,

"Metal Fittings in Overseas Markets," by Adolph W. Gilbert, Chapman Valve Mfg. Co., Indian Orchard, Mass.

At this session Machinery's motion picture, depicting the manufacture of 9.2-inch high-explosive howitzer shells, was shown, accompanied by an explanatory lecture by Chester L. Lucas of Machinery's staff.

In connection with the exposition there were interesting exhibits by 160 concerns, among whom were the following:

Bilton Machine Tool Co., Bridgeport, Conn. Gear-cutting machinery, sensitive drill presses, milling machines, and riveting machines.

Cowan Truck Co., Holyoke, Mass. Elevating electric and hand trucks, transportation systems.

Fitchburg Grinding Machine Co., Fitchburg, Mass. Grinding machines.

Peter A. Frasse & Co., Inc., Hartford, Conn. Tubing, steel, tools and supplies.

C. G. Garrigus Machine Co., Bristol, Conn. Machine tools. General Electric Co., Schenectady, N. Y. Electrical apparatus.

Graton & Knight Mfg. Co., Worcester, Mass. Leather belting, leather specialties.

Greenfield Tap & Die Corporation, Greenfield, Mass. Screw cutting tools and machinery; gages, reamers, etc.
Hampden Corundum Wheel Co., Springfield, Mass. Grinding wheels and polishing abrasives.

Holyoke Truck Co., Holyoke, Mass. Transfer and elevating

trucks. Napier Saw Works, Inc., Springfield, Mass. Metal cutting saws and sawing machines

National Scale Co., Chicopee Falls, Mass. Counting machines, calling system, elevating trucks, sectional steel shelving. Noble & Westbrook Mfg. Co., Hartford, Conn. Marking and filing machinery, grinders and buffing lathes, steel dies.

Norton Co., Worcester, Mass. Grinding wheels, grinding machinery.

Norton Grinding Co., Worcester, Mass. Grinding wheels, grinding machinery.

Reed-Prentice Co., Worcester, Mass. Lathes, drilling machines, vertical surface grinding machines.

Springfield Grinding Co., Chester, Mass. Grinding wheels.

L. S. Starrett Co., Athol, Mass. Fine mechanical tools. Union Twist Drill Co., Athol, Mass. Twist drills, gear and

milling cutters. Van Norman Machine Tool Co., Springfield, Mass. Machine tools, milling machines and grinders

Walworth Mfg. Co., Boston, Mass. Valves, fittings and tools

r steam, water and gas.
Whitcomb-Blaisdell Machine Tool Co., Worcester, Mass. Engine lathes and metal planers.

# PYROMETERS OF THE PAST, PRESENT AND FUTURE

A REVIEW OF DEVICES FOR MEASURING THE TEMPERATURE OF FURNACES, THEIR LIMITATIONS AND POSSIBLE FUTURE DEVELOPMENTS

S far as we know, the ancients, who baked excellent bricks and forged iron, measured temperature by a means still used today, but with ever-diminishing success-the eye. But at a very early date attempts were made to measure temperature by the expansion, contraction, or fusing points of clay. Even today the heat of brick and pottery kilns is determined by placing side by side, where they can be seen through a peep-hole, three cones with fusing points, for instance, of 2100, 2120 and 2140 degrees F. When the first cone softens and falls over, it indicates that a temperature of 2100 degrees F. has been attained, and the firing is stopped. If the other cones are still standing, the temperature has not exceeded 2120 degrees F. Unfortunately, though, the cones are affected by both time and temperature, and will soften or fall over at a higher temperature when heated up slowly for 100 hours than when heated to the softening point in an hour or two. They are not suitable for use in heat-treating furnaces for this reason, although attempts have been made to use them. However, some fusible salts have recently been brought out that seem to give reasonably satisfactory results. The capsules containing them are placed on a piece of steel in the furnace and the salts indicate, by melting, when a certain temperature has been attained.

Another of the early devices is the mercurial thermometer, with which everyone is familiar. For temperatures up to 600 degrees F., these have a vacuum above the mercury column. Thermometers graduated above 674 degrees must have the mercury column under pressure to prevent boiling; but 1000 degrees is about the limit for thermometers of this kind.

The first mechanical pyrometers depended on the difference in the expansion of iron and brass for their operation. This form of pyrometer has a tendency to change in its reading with time and temperature, due to the coefficient of expansion of the metals changing through continuous heating and cooling. This occasions frequent readjustments of the pointer to compensate for this error. Another early device was formed by placing a pipe in the furnace, through which water flowed under constant pressure. Thermometers at the inlet and outlet measured the temperature of the water, and the rise in temperature of the water was equivalent to a certain actual temperature in the furnace. The trouble with this device was that leaks occurred which it seemed impossible to prevent. The Siemens water pyrometer is used quite largely by armorplate manufacturers for heat-treatment. It consists of a copper ball, which is placed on the steel in the furnace and left until it has fully attained the temperature, when it is quickly removed and dropped into a vessel containing a thermometer and a measured quantity of pure water. The rise in temperature of the thermometer in the water is read off in actual temperature degrees on a corresponding scale. An accuracy within about 25 degrees F. is usually attained with this instrument.

There have also been developed a number of pyrometers that compare either a light or different colors with the piece of steel in the furnace. The trouble with all of these is that no two operators get the same results. Resistance thermometers operate on the principle that the electrical resistance of metals changes with the temperature. This instrument is an exceedingly accurate one for measuring low temperatures, but is hardly to be recommended for high temperature service.

#### Thermo-electric Pyrometers

For measuring temperatures above 1000 degrees F., the thermo-electric method has come to be by far the most largely used. A thermo-electric pyrometer consists of a thermo-couple, a measuring device, and the wires connecting the thermo-couple and the measuring device. If two pieces of wire of different metals are joined at one end and the junction is heated, a small current of electricity will be generated. At

<sup>1</sup>Abstract of a paper by Richard P. Brown, read before the Steel Treating Research Club of Detroit, Mich.

2000 degrees F., a couple formed of iron and copper-nickel wires will generate 50 millivolts. For measuring temperatures up to 200 degrees F., a thermo-couple of bismuth and antimony is best; for temperatures up to 1000 degrees F., a satisfactory thermo-couple consists of one iron wire and one 60 per cent nickel and 40 per cent copper; for temperatures as high as 1800 degrees F., a very satisfactory base-metal thermo-couple is one wire of 90 per cent nickel and 10 per cent chromium and the other wire of 98 per cent nickel and 2 per cent aluminum. For constant service above this, a thermo-couple, one wire of which is chemically pure platinum and the other 90 per cent platinum and 10 per cent rhodium, is recommended.

Thermo-couples of base metal are manufactured with wires from 0.01 inch up to 0.25 inch diameter. Some particular tests require thermo-couple wires of exceedingly small diameter to secure sensitiveness and quick readings. There is no doubt but that heavier wires forming the thermo-couple will increase the life where a base-metal thermo-couple is in constant service at temperatures up to 1600 or 1800 degrees F. While a heavier thermo-couple slightly increases the lag, this is not noticeable in heat-treating furnaces.

If after a base-metal thermo-couple has been used for some time another couple is made from the same wires, the voltage produced might vary as much as 50 degrees at a temperature of 1400 degrees F. Thermo-couples of nickel-chromium wire will vary as much as 30 degrees F., that is, 15 degrees plus or minus, depending on the particular coils from which the wire was cut.

The wires forming a thermo-couple must be insulated from each other throughout their length. A common method is to wrap base-metal thermo-couples with asbestos and paint the asbestos winding with a solution of sodium silicate; another method is to fit lava or porcelain beads over the thermo-couple wire. For the platinum thermo-couple, the insulation must be of porcelain or high-grade fireclay, free from impurities.

The life of a thermo-couple installed in a furnace largely depends on its protecting tube. For temperatures up to 1200 degrees F., a high-grade wrought-iron tube gives satisfactory results. Calorizing, a process recently developed by the General Electric Co., which impregnates the pipe with an aluminum oxide, will increase the life of the pipe about three times when used at temperatures around 1400 degrees F. Tubes of nickel-chromium give excellent results for temperatures as high as 1800 degrees, and they are to be recommended for the protection of base-metal thermo-couples where the temperature exceeds 1200 degrees. Their cost is many times higher than the ordinary wrought-iron pipe and about four times as much as calorized pipe, but their increased life would justify the increased first cost. Platinum thermo-couples must always be protected with a tube that is impervious to gases, such as porcelain, quartz, or alundum.

It is one of the properties of a thermo-couple that the voltage which it generates is dependent on the difference in the temperature of the hot junction and the cold junction, which is the point at which the alloy wires of the thermocouple join the copper leads of the instrument. It is therefore particularly important that the cold junction be maintained at a constant temperature. In recent years, it has been customary to run compensating leads of the same material as the thermo-couple to a distant point, where the temperature is uniform, instead of having the cold junction just outside the furnace wall, where it might vary several hundred degrees. These compensating leads, in duplex form with asbestos insulation, can be run into a pipe driven into the ground, ten or fifteen feet, where the temperature will remain constant within five degrees, winter or summer. Where it is impossible to place the cold junction in the ground, on account of the furnaces being on an upper floor of a building, a compensation box can be used, consisting of a lamp and thermostat, which will maintain the temperature constant within two degrees.

#### Measuring Voltage Produced by Thermo-couple

There are two methods of measuring the voltage produced by a thermo-couple, the millivoltmeter method and the potentiometer method. In the former, the instrument consists of a permanent magnet with its pole pieces, in the field of which a copper-wound coil swings in jeweled bearings. The millivoltmeter reads the temperature across the scale and is calibrated in actual temperature degrees. It indicates the temperature from zero to the maximum scale range and relies entirely on the voltage of the thermo-couple for its operation. No outside sources of current are necessary.

In the potentiometer method, the electromotive force produced by the thermo-couple is measured by opposing to it a known variable electromotive force, usually that of a dry cell contained in the instrument, so that when a balance is reached no current flows. A galvanometer is used to indicate the point at which no current is flowing, and the pointer on the galvanometer then indicates zero as the voltage of the thermo-couple is opposed to the dry cell. The advantages of the potentiometer method of measuring temperature are its extreme precision and its independence of resistance changes throughout the thermo-couple circuit. Its disadvantages are that it is not direct reading and some outside source of current is necessary.

#### Radiation Pyrometers

The radiation pyrometer is a development of the thermoelectric pyrometer. Instead of placing the thermo-couple inside the furnace, where the temperature is so high as to destroy it, it is placed in the back of a tube in front of a mirror. The rays of heat from the furnace enter the tube and, striking the mirror, are brought to a focus on the thermocouple junction, which attains a heat of only 200 or 300 degrees. It is possible to secure an accuracy within one to two per cent with this instrument, if the instructions for its use are properly carried out. It is not recommended for service where a thermo-electric pyrometer with a base-metal or platinum thermo-couple can be used.

#### Methods of Standardizing Pyrometers

It is essential, if accurate results are to be secured from pyrometers, that they be restandardized at frequent intervals. The frequency depends on the precision necessary in the work and the equipment available. Some plants check their thermocouples once a week; it should be done at least once a month. This checking can be satisfactorily accomplished by maintaining a standard platinum thermo-couple and using an electric furnace that is not less than 10 inches deep, so that a basemetal thermo-couple can project at least 6 or 8 inches inside. The base-metal and standard thermo-couples should be tied together with asbestos string with the junctions almost touching each other. Thermo-couples should never be tested in their protecting pipe. A base-metal thermo-couple should not be tested in a furnace with an insertion of less than 6 inches, for the cross-section of the thermo-couple wires is large and they conduct the heat from the furnace. The temperature of an electric furnace should be maintained constant for at least fifteen minutes before a reading is taken, and the tests should preferably be made at the working temperature of the thermocouple. If the thermo-couple under test reads low and has no adjustable resistance, it must be junked. If it is furnished with a resistance for adjustment purposes, this adjustment can be easily made with a soldering iron.

The freezing point of pure salt is reliable for testing thermocouples or the complete pyrometer. The thermo-couple should be inserted in a small crucible containing pure salt (ordinary table salt is satisfactory), heated to about 1600 degrees F. and then allowed to cool. At the freezing point of the salt, which will be indicated by the temperature remaining reasonably constant for four or five minutes, the pyrometer should read 1474 degrees. The melting point of a number of metals may also be used. The melting points of the metals most generally used for this purpose are: tin, 450 degrees F.; zinc, 787 degrees; silver, 1761 degrees; and gold, 1945 degrees.

#### The Future for Pyrometry

It would seem that the greatest development work in temperature-measuring instruments will be in the perfection of optical pyrometers, resistance thermometers, and thermoelectric pyrometers. There is a field for a high-grade optical pyrometer that can be used by any number of operators, all of whom can secure the same results from the instrument. Resistance thermometry will continue to be limited to low temperatures unless some more suitable metal than nickel can be used to form the bulbs. In thermo-electric pyrometry, it is possible to develop better materials for base-metal thermocouples; the insulation or protecting tube will be difficult to improve upon. The direct-reading millivoltmeter and the potentiometer methods of temperature measurement will doubtless be improved.

However, the greatest future in pyrometry will be along the line of automatic temperature control. There is already an instrument that automatically controls the temperature of an electric furnace, maintaining it constant within 10 degrees F. In connection with this instrument, there are two lights which indicate whether the temperature is high or low. We can place a neutral point, 10 or 20 degrees in width, between the two contact points operating these lights, so that both lights will be out when the temperature is correct and the red or blue light will flash to indicate that the temperature is too high or too low. If a third contact is put in the instrument for this neutral point, it will cause a white light to glow when the temperature is correct. It is much easier to instruct a fireman to keep the white light burning and the other lights out than to get him to maintain 1380 degrees on the pyrometer. He can see the lights from some distance, and these are easily understood by him. It is only a question of time when a switching device will permit one instrument to operate the signal lights at a number of furnaces.

One of the greatest difficulties experienced by pyrometer manufacturers is to induce the user of these instruments to install them properly. Frequently this is left to someone who has absolutely no knowledge of pyrometers, and the instructions of the manufacturer are not carried out in a satisfactory manner. Recently, the service man of one pyrometer company found pyrometer equipment giving incorrect readings because it had been wired up throughout with small diameter uninsulated iron wire.

## MILLING AND GRINDING

The use of milling machines and grinding machines has increased greatly during the past ten years, and these machines are now regarded generally as standard machine tool equipment. There is little question of the superiority of the milling machine over the planer or shaper for manufacturing parts in large quantities. Nor can the place of the grinding machine as a follower of the lathe for finishing cylindrical surfaces be longer denied. But notwithstanding the great increase in the use of these machine tools, the lathe is still the recognized leader of all. More lathes are built and sold than any other machine tool except drilling machines. Planers have their place in the machine shop and will always be used for jobbing and repair work and probably for planing the working surfaces of machines that must be highly accurate. The shaper and slotter have their recognized places also. The point to be made is that the development of any type of machine tool does not necessarily, if ever, result in displacing another; it may, in fact, make a broader and better market for all.

# FOUNDRY AND MACHINE SHOP EQUIPMENT AND SUPPLIES EXHIBIT

The twelfth annual exhibit of foundry and machine shop equipment and supplies will be held in the Mechanics Bldg., Boston, Mass., under the auspices of the American Foundrymen's Association, September 25 to 28, inclusive. Copies of the rules and regulations may be obtained from C. E. Hoyt, manager of exhibits, 123 W. Madison St., Chicago, Ill.

# MACHINE-CUT ELLIPTICAL GEARS

LAYING OUT AND MACHINING ELLIPTIC AND OVAL GEARS

BY REGINALD TRAUTSCHOLD 2

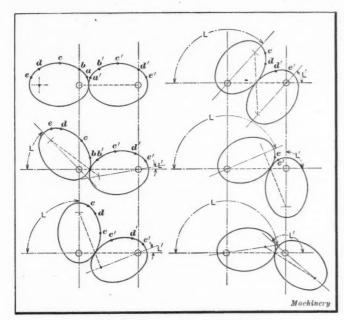


Fig. 1. Rolling Contact of Ellipses with Bore at Focus

THE correct proportioning of elliptic or elliptical gearing presents one of the most intricate problems confronting the gear designer, but, fortunately, it need not present the same difficulties to the machinist if the work is correctly laid out for him in the drafting-room. To cut elliptic gears successfully requires a high degree of skill and careful workmanship on the part of the machine operator, but the real problem is one of design. This is fortunate, for it permits the derivation of reliable formulas which, though they necessitate considerable accurate figuring on the part of the designer, greatly simplify the calculations and enable the problem to be put to the operator as a definite and concrete task: one that requires, in its execution, simply careful workmanship and proper attention to the adjustments of a comparatively simple fixture.

Elliptic gearing furnishes a comparatively cheap, efficient and positive mechanism for imparting a quick-return motion to the ram of shapers, planers and a large variety of machine tools. The variation in speed of these gears is from a maxi-

<sup>1</sup> For previous articles on the design of gearing, see "Epicyclic Gear Trains" in the July, 1917, number of Machinery, and articles there referred to. <sup>2</sup> Address: 39 Charles St., New York City.

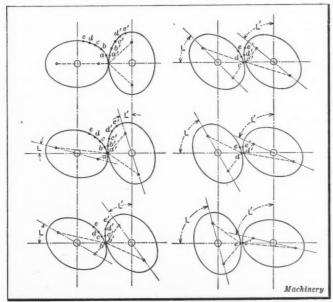


Fig. 2. Non-contact of Ellipses with Bore at Center

mum to a minimum, the bore being located at one of the foci of the ellipse. So-called "elliptical" gears with the bore at the center of the gear are also employed. These have not a true elliptic outline, but their circumference is appreciably greater than is that of a true ellipse of similar major and minor axes. To differentiate it from the one of true elliptic outline, this second variety of gear may be arbitrarily designated as an "oval gear"; while the term elliptic gear may be taken to designate a gear of true elliptic form.

The rolling actions of the two forms of mountings, those with the bore at the foci and those with the bore at the center, are depicted in Figs. 1 and 2. In the case of ellipses with the bore at one of the foci, any point on the circumference of one of the ellipses, a, b, c, d, e, will be in contact with any similarly located point on the circumference of the other ellipse, a', b', c', d', e', in the plane of the bores and a line connecting the stationary foci of the two ellipses will lie in this plane and intersect a plane tangent to both ellipses at the point of contact. In the case of the ellipses with the bore at the center, points on the circumference of one of the ellipses, a, b, c, d, e, will not be in contact with similarly located points on the circumference of the other ellipse, a', b', c', d', e', on the bore plane, the centers of the bores being fixed as in the other instance, but will be separated by an amount depending on the

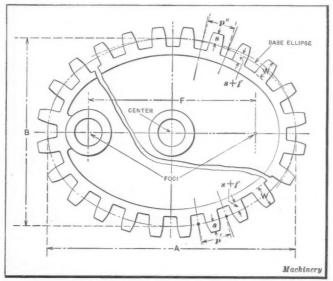


Fig. 3. Elliptic and Oval Gear Diagrams

proportions of the ellipses. Only when the major and minor axes of the ellipses are at right angles can the ellipses be in intimate contact. To secure contact at all points, the elliptic outlines must be increased by an increment that will fill in the gap between the ellipses; and in order that the two figures may be similar in outline, the increment should be the same for each ellipse.

The similarity between elliptic and oval gears lies only in the fact that they are both developed from ellipses. In one case the ellipse is the final outline; and in the other, the ellipse has to be modified by an increase in the length of curve included between the two axes' planes in each of the four quadrants. The lengths of the axes are not changed, nor should the degree of curvature at points of contact be altered; the variation in curvature is simply limited to sections between the required points of contact. Elliptic and oval gear sections are illustrated in Fig. 3 in a manner that brings out their similarity in general appearance as well as their difference in pitch outlines.

# The Ellipse

The basic form of either the elliptic or the oval gear is the ellipse, so the characteristics of this figure should be clearly

understood before taking up the derivation of working formulas. An ellipse is shown in Fig. 4. Its governing peculiarity is that the sum of the distances of any point P on the circumference from the two foci is constant, and the normal passing through such point bisects the angle included between lines drawn from the point to the foci. The angle between the tangent to the point and one of the axes of the ellipse is equal to the angle between the normal to the point and the other axis of the ellipse. The distance between the two foci, the "focus distance," is equal to the square root of the difference of the squares of the major and minor axes. These definite relations establish the equation of the ellipse, which, though simple, necessitates an application of analytical geometry and calculus to establish the location of any particular point on the circumference, the angularity of tangents, etc. This involves much calculation that, from a practical point of view, is quite unnecessary.

The curvature of an ellipse really decreases in each quadrant, from the major to the minor axis, but for all practical purposes, there are but two degrees of curvature in each quadrant of any elliptic gear encountered in practice, or that is capable of practical use, so that a close approximation of a true ellipse may be drawn with circular arcs of but two radii. These radii, which, for convenience, will be designated as major and minor, are equal to the major axis minus one-half the minor axis and to three-quarters the minor axis minus one-quarter the major axis. The first is the radius of the curve straddling the minor axis, and the second is the radius of the curve straddling the major axis. In workable ellipses, such curves become tangent to each other at definite points, so that the length of the major-radius curve is an arc included by an angle of 73 degrees, 44 minutes, as shown in Fig. 4, and the minor-radius curve is an arc included by an angle of 106 degrees, 16 minutes. These angles may be arbitrarily taken as the same for all ellipses, irrespective of the axes' lengths.

#### Dimensions Required by the Machinist

Fig. 5 depicts the method of cutting both elliptic and oval gears, the rotary cutter being tangent to the pitch line at mid-tooth space. The angle of tangency, the angle included between the center line of the rotary cutter and the major axis, is the same for either type of gear, but the location of the bore in respect to the center line of the cutter differs. If the outlines of the two varieties of gears were similar, the difference in both vertical and horizontal coordinates would be controlled by the distance from the focus to the center of the gear. In fact, much of the trouble encountered in cutting oval gears with the bore at the center comes from just this particular point. Oval gears with the bore at the center are not elliptic in outline and cannot be successfully cut with settings that would be satisfactory were it not necessary to modify the elliptic form in order that the gears may roll together in intimate contact.

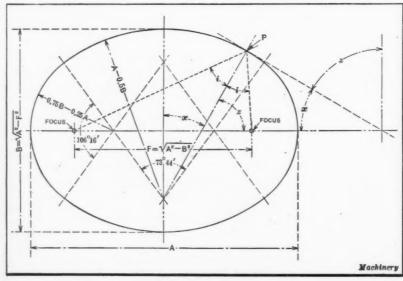


Fig. 4. The Ellipse

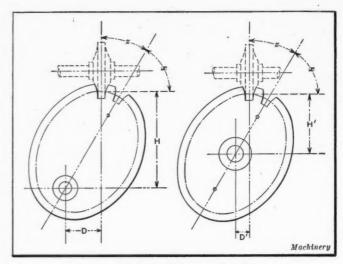


Fig. 5. Machining Elliptic and Oval Gears

#### Laying Out Elliptic Gears

The elliptic gear is the simpler variety to design, as an oval gear must first be proportioned as if it were truly elliptic in outline and then modified by the necessary increments. Both varieties are frequently laid out to a suitable scale and the required dimensions scaled; the "lay-out method" and a certain dependence on graphic depiction is a material aid even when employing the more accurate method of calculation of the necessary angles and dimensions.

The pitch outline of an elliptic gear is shown in Fig. 6. This may be drawn by the common "gardener's ellipse" method or by the use of the circular arcs, as has been described. The pitch circumference is then divided into as many equal sections as there are teeth in the gear, the points of division locating the centers of the tooth spaces. Preferably, the number of teeth in an elliptic gear should be odd, so that a tooth space at one end of the gear is opposite a tooth at the other end, thereby permitting both gears of a pair to be identical. If the number of teeth is even, a double set of calculations becomes necessary, as the tooth spaces of one of a pair must coincide with the teeth of the mating gear.

The coordinates of the center of the tooth spaces, with reference to the stationary focus, are readily calculated for an ellipse laid out with circular arcs, and are, for all practical purposes, the same as those of similar points about a true ellipse. The distance of each tooth-space center from the stationary focus is then readily obtained, as it is the length of the hypotenuse of a right-angle triangle having for its other sides the coordinates of the tooth-space center with respect to the stationary focus. These coordinate dimensions are the horizontal and vertical settings required by the machinist, and the angular setting of the blank is the angle included between

the tangent at mid-tooth space and the major axis of the ellipse.

#### Laying Out Oval Gears

Oval gears should have an even number of teeth, so that but one set of calculations is necessary, and the teeth should be arranged so that they do not come on the axis of the ellipse, but so that the transverse pitch line on the profile of a tooth falls on the axes of the gear, as shown in Fig. 7. This illustration depicts the basic oval outline of the gear, not its final pitch outline.

The coordinates of the tooth-space centers, with reference to the center of the gear, are found in a manner similar to that employed for elliptic gears. The distance of each tooth-space center from the center of the gear on the base ellipse is then found and normals through each of the tooth-space centers are drawn. The horizontal setting D' is found directly from the triangle formed by the line connecting the center tooth space on the ellipse and the rectangular

coordinates of such point about the center of the gear. The ordinate of the point is also calculated, though it is not equal to the vertical setting, which is controlled by the amount of increment added to the ellipse at each tooth space.

The distance between shafts of mating oval gears is constant and equal to one-half the sum of the major and minor axes of the gear, so that if the sum of the distances from the tooth-space center of conjugate tooth spaces is made equal to the distance between shafts, constant contact is secured. The proper total increment required in order to secure such intimate contact between mating gears is the difference between the sum of the distances of center tooth points on the ellipse of conjugate tooth spaces and the distance between the shafts of the respective gears. Half of this total increment added to each gear will keep the gears similar in outline. The increment is not added to the oval outline normally. but so that the distance from the pitch center of the tooth space on the mid-tooth space normal

to the center of the gear is equal to the distance from the center of the gear to the center of the tooth space on the ellipse, plus half the total increment required for intimate contact, see Fig. 8. A smooth curve passing through the points thus located on the tooth space normals gives the required pitch outline of the gear. To this must be added, in the gear blank, sufficient metal to accommodate the addendum of the teeth, etc. The correct vertical setting is then obtained by direct proportion, the same relationship existing between the distance of the mid-tooth space point on the ellipse and this same dimension plus the necessary increment as exists between the ordinate of the center tooth space on the ellipse and the correct vertical setting.

#### Notation for Elliptical Gearing

•	
Major axis (pitch)	A
Minor axis (pitch)	
Focus distance, distance between foci	
Pitch circumference of ellipse	
Quick-return ratio of elliptic gears	
Number of teeth	
Circular pitch of elliptic gears	p'
Major radius for ellipse	
Minor radius for ellipse	
Angular pitch of major radius segment	
Angular pitch of minor radius segment	
Angle included between tooth-space tangents and major axis	
Angularity of ratchet index	
Ordinate of tooth-space center on ellipse	
Abscissa of tooth-space center on ellipse	
Distance between tooth-space center on ellipse and focus axis	
Angle included between Y and major axis	
Angle included between Y and tooth-space tangent	
Vertical setting for machining fixture	
Horizontal setting for machining fixture	
Effective circular pitch of oval gears	
Distance between tooth-space center on ellipse and gear	P
center	Y''
Sum of conjugate Y"	
Correction increment	j
Distance between tooth-space pitch center and gear center.	Y'
Angle included between Y" and major axis	u'
Angle included between Y" and tooth-space tangent	
Vertical setting on ellipse	
Vertical setting for machining fixture	
Horizontal setting for machining fixture	
Horizontal Setting for machining nature	D

#### Formulas for Elliptic and Oval Gears

$$B = \sqrt{A^2 - F^2}$$
 (1)  $F = \frac{A(R-1)}{R + 1}$  (2)

$$R = \frac{A + F}{A - F}$$
 (3)  $r' = A - 0.5B$  (4)

$$r'' = 0.75B - 0.25A$$
 (5)  $C = 1.6464A + 1.4952B$  (6)

$$p' = \frac{C}{N}$$
 (7)  $a = \frac{57.295p'}{r'}$  (8)  $a' = \frac{57.295p'}{r''}$  (9)

$$h' = r'' \sin z$$
 (in minor-radius segments) (10)

$$h' = r' \cos x - r' + 0.5B$$
 (in major-radius segments) (10a)

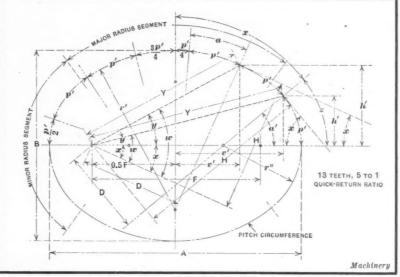


Fig. 6. Elliptic Gear Diagram

$$v'=r''\cos z+0.5A-r''$$
 (in minor-radius segments) (11)  $v'=r'\sin x$  (in major-radius segments) (11a)

$$Y = \sqrt{h'^2 + (\pm 0.5F \pm v')^2}$$
 (12)  $\operatorname{Tan} y = \frac{h'}{\pm 0.5F \pm v'}$  (13)

$$w = y \pm x \qquad (14) \qquad \qquad H = Y \sin w \qquad (15)$$

$$D = Y \cos w \qquad (16) \qquad \qquad p'' = \frac{C}{N} \qquad (17)$$

$$Y'' = \sqrt{h'^2 + v'^2}$$
 (18)  $j = 0.5(0.5A + 0.5B - X)$  (19)

$$Y' = Y'' + j$$
 (20)  $\operatorname{Tan} y' = \frac{h'}{v'}$  (21)  $w' = y' + x$  (22)

$$H'' = r'' + (0.5A - r'') \cos(90 - x)$$
 (in minor-radius

$$H'' = Y'' \sin w'$$
 (in major-radius segments) (23a)

$$D' = (0.5A - r'') \sin (90 - x) \text{ (in minor-radius segments)}$$
 (25) 
$$D' = Y'' \cos w' \text{ (in major-radius segments)}$$
 (25a)

### Discussion of Formulas

The relationships existing between the major axis, the minor axis, and the focus distance are the ordinary characteristics common to the ellipse. The quick-return ratio of elliptic gears is the ratio between the maximum and minimum distances of the pitch circumference from the stationary, or bore, focus. No such ratio exists for oval gears, as the distance between the shafts of the gears with the central bore is equal to half the sum of the major and the minor axes. Two speed changes occur during a complete revolution of the gears in such an arrangement; one is measured by the ratio of the major axis to the minor axis, and the other by the ratio of the minor axis to the major axis.

The major and minor radii of the ellipse are the radii of circular arcs straddling the minor and the major axes, respectively; the former contains 73 degrees, 44 minutes, and the latter 106 degrees, 16 minutes. The sum of the lengths of the two major-radius segments and the two minor-radius segments equals the circumference of the ellipse. This divided by the number of teeth gives the circular pitch for elliptic gears.

The circular pitch multiplied by 360 degrees and the product divided by the circumference of a circle having a radius equal to the major radius of the ellipse gives the angular pitch in the major-radius segments. The same product divided by the circumference of a circle having a radius equal to the minor radius of the ellipse gives the angular pitch in the minor-radius segments.

To obtain the ordinate of the tooth-space center on the pitch ellipse necessitates two formulas: one for cases where the tooth-space center falls within the minor-radius segments, and

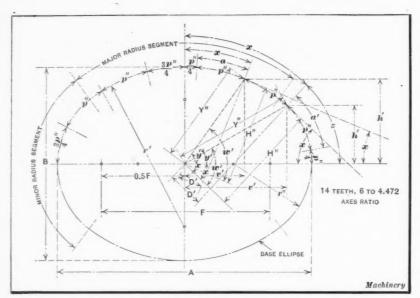


Fig. 7. Base Ellipse for Oval Gear

the other for points that fall within the major-radius segments. In the former, the ordinates are equal to the minor radius times the sine of the angle included between the normal passing through the tooth-space center and the major axis. Within the major-radius segments, the ordinates are measured by the product of the major radius and the cosine of the angle included between the normal passing through the tooth-space center and the minor axis, minus the difference between the major radius and one-half the minor axis. This value, by which the product of the major radius and the cosine of the angle is reduced, is the distance from the major axis to the center of the major radius.

The abscissa of the tooth-space center on the pitch ellipse is found in a similar manner, two formulas being required. For centers within the minor-radius segments, the abscissas are equal to the product of the minor radius and the cosine of the angle included between the normal passing through the tooth-space center and the major axes, plus the difference between half the major axis and the minor radius. Within the major-radius segments, the abscissas are equal to the major radius multiplied by the sine of the angle included between the normal passing through the tooth-space center and the minor axis.

The distance between the tooth-space center on the ellipse and the stationary focus in elliptic gears is equal to the square root of the sum of the square of the ordinate plus the square of the distance of the projected center on the major axis from the stationary focus. When the projection of the center on the major axis falls on the farther side of the minor axis from that on which the stationary focus is located, this

distance is equal to one-half the focus distance plus the abscissa; when between the near center of the minor radius and the minor axis, it is equal to the focus distance minus the abscissa; and when between the near minor radius center and the near end of the major axis, it is equal to the abscissa minus half the focus distance.

The tangent of the angle included between Y and the major axis is equal to the ordinate of the tooth-space center divided by the distance of the projected center on the major axis from the stationary focus. This angle plus or minus the angle included between the tangent to the tooth-space center and the major axis equals the angle included between Y and the tooth-space tangent. When the tooth-space center lies on the far side of the minor axis, the angle included between Y and the tooth-space tangent is the sum of the two smaller angles; when on the near side, it is equal to the difference of the two angles.

The vertical setting for the machining fixture, the distance between the plane of the rotary cutter and a parallel plane passing through the stationary

fecus of the gear, is equal to the distance between the tooth-space center and the stationary focus multiplied by the sine of the angle included between Y and the tooth-space tangent; while the horizontal setting for the machining fixture is equal to the product of this same dimension by the cosine of the angle.

The effective circular pitch of oval gears corresponds to the circular pitch of elliptic gears and is found in the same manner; namely, by dividing the pitch circumference of the base ellipse by the number of teeth in the gear.

The distance between the center of the tooth space on the ellipse and the central bore of the gear is equal to the square root of the sum of the squares of the ordinate and abscissa dimensions of the tooth-space center on the base ellipse.

The correction increment is equal to half the sum of the major and minor axes of the gear, minus the sum of the distances of conjugate tooth-space centers on the base ellipse from the center of the gear divided by 2. Conjugate

tooth spaces are a tooth space on one gear and the space opposite the tooth on the mating gear that will engage the tooth space on the first gear. For instance, in a pair of mating oval gears with fourteen teeth, the conjugate tooth space of the first tooth space on the driving gear is the fourth tooth space on the driven gear, counting tooth spaces from similar points on the two gears. Similarly, the conjugate tooth space for the second tooth space on the driver is the third on the driven gear, and for the remainder of the tooth spaces the conjugates are the third and second, fourth and first, fifth and fourteenth, sixth and thirteenth, seventh and twelfth, eighth and eleventh, ninth and tenth, tenth and ninth, and so forth.

The correction increment added to the distance between the tooth-space center on the base ellipse and the central bore gives the distance of the actual pitch center of the tooth space from the center of the gear.

The tangent of the angle included between the line connecting the tooth-space center on the base ellipse with the center of the gear and the major axis is equal to the ordinate dimension of the point on the base ellipse divided by its abscissa dimension. This angle plus the angle included between the tooth-space normal and the minor axis (the complement of the angle included between the tooth-space normal and the major axis) equals the angle included between Y" and the tooth-space tangent on the base ellipse.

The vertical setting on the base ellipse, when the normal of the tooth space crosses the minor-radius segment of the base ellipse, is equal to the minor radius plus the product of the cosine of the complement of the angle included between the

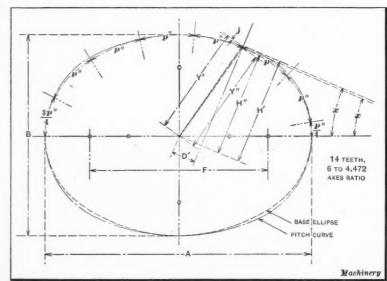


Fig. 8. Oval Gear Diagram

tooth-space tangent and the major axis by the difference between half the major axis and the minor radius of the base ellipse. When the tooth-space normal crosses the major-radius segment, the vertical setting on the base ellipse is equal to the product of Y" by the sine of the angle included between Y" and the tooth-space tangent.

The vertical setting on the base ellipse multiplied by the quotient of Y' divided by Y" equals the vertical setting for the machining fixture. This dimension is the distance between a tangent to the pitch curve at the tooth-space normal and a parallel line passing through the central bore of the gear.

The horizontal setting for the machining fixture, in minorradius segments, is equal to the product of the sine of the complement of the angle included between the tooth-space tangent and the major axis by the difference between half the major axis and the minor radius of the base ellipse. The horizontal setting for tooth spaces crossing the major-radius segment is equal to the product of Y'' by the cosine of the angle included between Y" and the tooth-space tangent. For tooth spaces lying to the right of the gear center, the horizontal settings are also measured to the right; and for tooth spaces lying to the left of the gear center, the horizontal settings are in the same direction.

Example 1-Required, a pair of elliptic gears: 6-inch centers, 5 to 1 quick-return motion, 13 teeth; bore at focus.

\* 
$$F = \frac{6(5-1)}{5+1} = 4 \text{ inches}$$
 (2)

$$B = \sqrt{36 - 16} = 4.472$$
 inches (1)

$$C = 1.6464 \times 6 + 1.4952 \times 4.472 = 16.5649$$
 inches (6)

$$p' = \frac{16.5649}{13} = 1.2742 \text{ inch} \tag{7}$$

$$r' = 6 - 0.5 \times 4.472 = 3.764 \text{ inches}$$
 (4)  
 $r'' = 0.75 \times 4.472 = 0.25 \times 6 - 1.854 \text{ inch}$  (5)

$$r'' = 0.75 \times 4.472 - 0.25 \times 6 = 1.854 \text{ inch}$$
 (5)  
 $a = \frac{57.295 \times 1.2742}{} = 19.396 \text{ degrees}$  (8)

$$a' = \frac{3.764}{57.295 \times 1.2742} = 39.377 \text{ degrees}$$
 (9)

x, Degrees	z, Degrees	Tooth-space Number	x, Degrees	z, Degrees
90.000	0.000	8	70.312	199.688
50.623	39.377	9	33.943	236.057
24.245	65.755	10	14.547	255.453
4.849	85.151	11	4.849	274.849
14.547	104.547	12	24.245	294.245
33.943	123.943	13	50.623	320.623
70.312	160.312			
	Degrees 90.000 50.623 24.245 4.849 14.547 33.943	Degrees         Degrees           90.000         0.000           50.623         39.377           24.245         65.755           4.849         85.151           14.547         104.547           33.943         123.943	Degrees         Degrees         Number           90.000         0.000         8           50.623         39.377         9           24.245         65.755         10           4.849         85.151         11           14.547         104.547         12           33.943         123.943         13	Degrees         Degrees         Number         Degrees           90.000         0.000         8         70.312           50.623         39.377         9         33.943           24.245         65.755         10         14.547           4.849         85.151         11         4.849           14.547         104.547         12         24.245           33.943         123.943         13         50.623

# Tooth-

#### h' = 0.000 inch

-	n = 0.000  men	
2	$h' = 1.854 \times 0.63451 = 1.175$ inch	(10)
3	$h' = 3.764 \times 0.91176 - 1.528 = 1.902$ inch	(10a)
A	1/ 9 704 \ 0 00040 1 500 9 907 imphor	(100)

4 
$$h' = 3.764 \times 0.99642 - 1.528 = 2.227$$
 inches  
5  $h' = 3.764 \times 0.96793 - 1.528 = 2.114$  inches  
6  $h' = 3.764 \times 0.82960 - 1.528 = 1.592$  inch  
7  $h' = 1.854 \times 0.33682 = 0.625$  inch  
8  $h' = 0.625$  inch
(10a)

- 9 h' = 1.592 inch
- h'=2.114 inches 10
- 11 12 h'=2.227 inches h'=1.902 inch
- 13 h' = 1.175 inch

# Tooth-

# Number Number

1 
$$v' = 3.000$$
 inches  
2  $v' = 1.854 \times 0.77292 + 1.146 =$ 

- $v' = 3.764 \times 0.55830 = 2.106$  inches  $v' = 1.854 \times 0.94157 + 1.146 = 2.890$  inches
- v'=2.890 inches
- v'=2.106 inches
- v' = 0.947 inch v' = 0.318 inch 10
- 11 12 v'=1.549 inch
- 13 v'=2.578 inches

# Tooth-

# space Number

- 1  $Y = 0.5 \times 4 + 0.5 \times 6 = 5.00$  inches
- 2  $Y = \sqrt{(1.175)^2 + (2 + 2.578)^2} = 4.72$  inches

- 3  $Y = \sqrt{(1.902)^2 + (2 + 1.549)^2} = 4.03$  inches (12)
- 4  $Y = \sqrt{(2.227)^2 + (2 + 0.318)^2} = 3.22$  inches (12)
- 5  $Y = \sqrt{(2.114)^2 + (2 0.947)^2} = 2.32$  inches (12)
- $Y = \sqrt{(1.592)^2 + (2.106 2)^2} = 1.60$  inch (12)(12)
- $Y = \sqrt{(0.625)^3 + (2.890 2)^3} = 1.09$  inch
- Y = 1.09 inch Y = 1.60 inch
- 10 Y = 2.32 inches
- 11 Y = 3.22 inches
- Y = 4.03 inches
- Y = 4.72 inches 13

# Tooth

# Space Number

1 Tan 
$$y = 0.000$$
;  $y = 0.000$  degrees (13)

2 Tan 
$$y = \frac{1.175}{2 + 2.578} = 0.257$$
;  $y = 14.416$  degrees (13)

3 Tan 
$$y = \frac{1.902}{2 + 1.549} = 0.536$$
;  $y = 28.199$  degrees (13)

4 Tan 
$$y = \frac{2.227}{2 + 0.318} = 0.962$$
;  $y = 43.883$  degrees (13)

5 Tan 
$$y = \frac{2.114}{2 - 0.947} = 2.007; y = 63.516$$
degrees (13)

$$6 \quad \text{Tan } y = \frac{1.592}{2.106 - 2} = 15.03; \quad y = 86.200 \text{ degrees}$$
 (13)

7 
$$\operatorname{Tan} y = \frac{0.625}{2.890 - 2} = 0.703; \quad y = 35.1 + 90 \text{ degrees} = 125.100 \text{ degrees} \quad (13)$$

- y = 125.100 degrees
- y = 86.200 degrees
- 10 y = 63.516 degrees y = 43.883 degrees
- y = 28.199 degrees 12
- y = 14.416 degrees

#### Toothspace Number

- $\begin{array}{lll} 1 & w = 0 + 90 = 90.000 \ \mathrm{degrees} \\ 2 & w = 14.416 + 50.623 = 65.039 \ \mathrm{degrees} \\ 3 & w = 28.199 + 24.245 = 52.444 \ \mathrm{degrees} \\ 4 & w = 43.883 + 4.849 = 48.732 \ \mathrm{degrees} \end{array}$
- (14)
- (14)w = 63.516 - 14.547 = 48.969 degrees
- w = 86.200 33.943 = 52.257 degrees  $w = 35\,100 \pm 70\,312 = 105\,412$  degrees (14)
- w = 105.412 degrees 9 w = 52.257 degrees
- w = 48.969 degrees
- 11 w = 48.732 degrees
- w = 52.444 degrees
- w = 65.039 degrees 13

#### Toothspace Number

1 
$$H = 5 \times 1 = 5.000$$
 inches  
2  $H = 4.72 \times 0.90659 = 4.275$  inches  
3  $H = 4.03 \times 0.79276 = 3.190$  inches (15)

- $H=5 \times 1=5.000$  fiches  $H=4.72 \times 0.90659=4.275$  inches  $H=4.03 \times 0.79276=3.190$  inches  $H=3.22 \times 0.75165=2.420$  inches  $H=2.32 \times 0.75433=1.750$  inch (15)
- $H = 1.60 \times 0.79076 = 1.265$  inch  $H = 1.09 \times 0.96402 = 1.050$  inch (15)
- H=1.050 inch H = 1.265 inch
- 10
- H = 1.750 inch H = 1.750 inch H = 2.420 inches
- 11
- H = 3.190 inches H = 4.275 inches
- 13

# Tooth

# space Number

1 
$$D = 5 \times 0 = 0$$
  
2  $D = 4.72 \times 0.42192 = 1.99 \text{ inch}$  (16)

- (16) (16)3
- (16)(16)
- (16)
- $D=5 \times 0=0$   $D=4.72 \times 0.42192=1.99$  inch  $D=4.03 \times 0.60960=2.456$  inches  $D=3.22 \times 0.65956=2.123$  inches  $D=2.32 \times 0.65650=1.523$  inch  $D=1.60 \times 0.61213=0.980$  inch  $D=1.09 \times 0.26584=0.290$  inch (16)
- D = 0.290 inch
- 9 D = 0.980 inch
- D=1.523 inch
- 11 D=2.123 inches
- 13 D = 1.990 inch
- Example 2-Required, a pair of oval gears; major axis, 6 inches; focus distance, 4 inches; 14 teeth; bore at center
- (12) of gear.

(11a)

(11)

```
B = \sqrt{36 - 16} = 4.472 inches
                                                                                                       . (1)
                                                                                                                                     5.236 - (2.59 + 2.59)
                                                                                                                                                                                                                            (19)
                                                                                                                                                                                = 0.028 inch
                                                                                                                         6 \quad j = -
            C = 1.6464 \times 6 + 1.4952 \times 4.472 = 16.5649 inches
                                                                                                       (6)
                                                                                                                                                       2
                                       16.5649
                                                                                                                                       5.236 - (2.92 + 2.31)
                             p'' = -
                                                      = 1.1832 inch
                                                                                                       (17)
                                                                                                                                                                                                                            (19)
                                                                                                                                                                                 = 0.003 inch
                                                                                                                         7 j = -
                                                                                                                             j = 0.000 inch

j = 0.013 inch

j = 0.013 inch

j = 0.000 inch

j = 0.003 inch
                         r' = 6 - 0.5 \times 4.472 = 3.764 inches
                                                                                                                         8
                   r'' = 0.75 \times 4.472 - 0.25 \times 6 = 1.854 inch
                                                                                                         (5)
                            57.295 \times 1.1832
                                                                                                                       10
                                                           = 18.010  degrees
                                                                                                         (8)
                                       3.764
                                                                                                                       12
                                                                                                                               j = 0.028 inch
                             57.295 \times 1.1832
                                                                                                        (9)
                                                                                                                               j = 0.003 inch
                                                           = 36.565 degrees
                                                                                                                       14
                                   1.854
                                                                                                                     Tooth-
Tooth-space x,
Number Degrees
                                                           Tooth-space x,
Number Degrees
                                                                                                                    space
Number
                                      z,
Degrees
                                                                                                   z,
Degrees
                                                                                                                             Y'=2.99+0.000=2.990 inches Y'=2.78+0.013=2.793 inches Y'=2.43+0.013=2.443 inches Y'=2.25+0.000=2.250 inches Y'=2.31+0.003=2.313 inches Y'=2.59+0.028=2.618 inches Y'=2.92+0.003=2.923 inches Y'=2.990 inches
                                                                                                                                                                                                                            (20)
                80.859
                                        9.141
                                                                             80.859
                                                                                                  189.141
                                                                 8
                                                                                                                                                                                                                            (20)
                44.294
                                       45.706
                                                                             44.294
                                                                                                  225,706
       3
                22.512
                                       67.488
                                                                             22.512
                                                                                                  247.488
                                                                                                                                                                                                                            (20)
                                                                                                                                                                                                                            (20)
                                      85.498
                                                                                                  265.498
                                                                                                                         4 5
       4
                  4.502
                                                                  11
                                                                               4.502
                13.508
                                     103.508
                                                                             13.508
                                                                                                  283.508
                                                                                                                                                                                                                            (20)
                                                                                                                         6
       6
                31.518
                                     121.518
                                                                  13
                                                                             31.518
                                                                                                  301.518
                62.576
       7
                                     152.576
                                                                                                  332.576
                                                                                                                                                                                                                            (20)
Tooth-
                                                                                                                         8
space
Number
                                                                                                                               Y' = 2.793 inches
                                                                                                                               Y'=2.443 inches
          h' = 1.854 \times 0.15888 = 0.294 inch

h' = 1.854 \times 0.71569 = 1.327 inch

h' = 3.764 \times 0.92377 - 1.528 = 1.952 inch

h' = 3.764 \times 0.99692 - 1.528 = 2.232 inches

h' = 3.764 \times 0.97234 - 1.528 = 2.132 inches

h' = 3.764 \times 0.85249 - 1.528 = 1.682 inch

h' = 1.854 \times 0.46046 = 0.853 inch

h' = 0.294 inch

h' = 1.327 inch

h' = 1.952 inch
                                                                                                                       10
     1
                                                                                                       (10)
                                                                                                                              Y' = 2.250 inches Y' = 2.313 inches
                                                                                                                       11
     2
                                                                                                       (10)
                                                                                                                       12
                                                                                                     (10a)
                                                                                                                      13 Y' = 2.618 inches
14 Y' = 2.923 inches
                                                                                                      (10a)
                                                                                                      (10a)
                                                                                                                    Tooth-
     6
7
                                                                                                     (10a)
                                                                                                       (10)
                                                                                                                                               1.952
                                                                                                                                                           = 1.354; y' = 53.550 degrees
                                                                                                                         3 Tan y' = -
          h' = 1.327 inch

h' = 1.952 inch

h' = 2.232 inches

h' = 2.132 inches

h' = 1.682 inch
                                                                                                                                                1.442
   10
                                                                                                                                                2.232
   11
                                                                                                                                                                                                                            (21)
   12
                                                                                                                         4 Tan y' = -
                                                                                                                                                           y' = 7.560; y' = 82.466  degrees
                                                                                                                                                0.295
   14 h' = 0.853 inch
                                                                                                                                                2.132
Tooth-
                                                                                                                                                           = 2.425; y' = 67.591 degrees
                                                                                                                                                                                                                            (21)
                                                                                                                             \operatorname{Tan} y' =
space
Number
                                                                                                                                                 0.879
          v'=1.854 \times 0.98730 + 1.146 = 2.978 inches v'=1.854 \times 0.69842 + 1.146 = 2.442 inches v'=3.764 \times 0.38295 = 1.442 inch v'=3.764 \times 0.07846 = 0.295 inch v'=3.764 \times 0.23359 = 0.879 inch v'=3.764 \times 0.52275 = 1.970 inch v'=3.764 \times 0.88761 + 1.146 = 2.791 inches v'=2.978 inches
                                                                                                                                                 1.682
                                                                                                       (11)
                                                                                                                                                           = 0.854; y' = 40.500 degrees
                                                                                                     (11)
(11a)
                                                                                                                         6 Tan y' = -
     2
                                                                                                                                               1.970
                                                                                                      (11a)
                                                                                                                       10 y' = 53.550 degrees
                                                                                                                       11 y' = 82.466 degrees
12 y' = 67.591 degrees
                                                                                                      (11a)
     6
                                                                                                       (11)
                                                                                                                       13 y' = 40.500 degrees
          v' = 2.442 inches v' = 1.442 inch
                                                                                                                     Tooth-
                                                                                                                    space
Number
   10
          v' = 0.395 inch

v' = 0.879 inch
                                                                                                                            w'=53.550+22.512=76.062 degrees w'=82.466+4.502=86.968 degrees w'=67.591+13.508=81.099 degrees w'=40.500+31.518=72.018 degrees w'=76.062 degrees w'=86.968 degrees w'=81.099 degrees w'=72.018 degrees w'=72.018 degrees w'=72.018 degrees
                                                                                                                         3
   12
                                                                                                                                                                                                                             (22)
           v'=1.970 inch
                                                                                                                                                                                                                            (22)
   14
          v'=2.791 inches
                                                                                                                                                                                                                            (22)
 Tooth-
                                                                                                                       10
space
Number
                                                                                                                       11
                                                                                                                       12
          Y'' = \sqrt{(0.294)^2 + (2.978)^2} = 2.99 inches
                                                                                                       (18)
                                                                                                                       13
         Y'' = \sqrt{(1.327)^2 + (2.442)^2} = 2.78 inches
                                                                                                       (18)
         Y'' = \sqrt{\frac{(1.951)^{2} + (1.442)^{2}}{(2.232)^{2} + (0.295)^{2}}} = 2.43 \text{ inches}

Y'' = \sqrt{\frac{(2.232)^{2} + (0.295)^{2}}{(2.232)^{2} + (0.295)^{2}}} = 2.25 \text{ inches}
     3
                                                                                                                     Tooth-
                                                                                                       (18)
                                                                                                                    Number Number
     4
                                                                                                       (18)
                                                                                                                        1 H'' = 1.854 + 1.146 \times 0.98730 = 2.984 inches

2 H'' = 1.854 + 1.146 \times 0.69835 = 2.654 inches

3 H'' = 2.43 \times 0.97056 = 2.356 inches

4 H'' = 2.25 \times 0.99860 = 2.248 inches

5 H'' = 2.31 \times 0.98796 = 2.281 inches

6 H'' = 2.59 \times 0.95115 = 2.460 inches

7 H'' = 1.854 + 1.146 \times 0.88760 = 2.871 inches

8 H'' = 2.984 inches
         Y'' = \sqrt{(2.132)^2 + (0.879)^2} = 2.31 inches
     5
                                                                                                                                                                                                                            (23)
                                                                                                       (18)
                                                                                                                                                                                                                            (23)
           Y'' = \sqrt{(1.682)^2 + (1.970)^2} = 2.59 inches
     6
                                                                                                       (18)
                                                                                                                                                                                                                           (23a)
           Y'' = \sqrt{(0.853)^2 + (2.791)^2} = 2.92 inches
                                                                                                       (18)
                                                                                                                                                                                                                           (23a)
           Y''=2.99 inches
                                                                                                                                                                                                                           (23a)
     9
           Y'' = 2.78 inches
           Y'' = 2.43 inches Y'' = 2.25 inches Y'' = 2.25 inches Y'' = 2.31 inches
                                                                                                                                                                                                                          (23a)
    10
                                                                                                                                                                                                                            (23)
    11
    12
                                                                                                                              H'' = 2.654 inches H'' = 2.356 inches
    13
           Y'' = 2.59 inches
          Y'' = 2.92 inches
                                                                                                                        10
    14
                                                                                                                       10 H'' = 2.350 meles

11 H'' = 2.248 inches

12 H'' = 2.281 inches

13 H'' = 2.460 inches

14 H'' = 2.871 inches
 Tooth
space
Number
                   5.236 - (2.99 + 2.25)
     1 j = -
                                                           = 0.000 inch
                                                                                                       (19)
                                                                                                                    Tooth-
                                  2
                   5.236 - (2.78 + 2.43)
                                                                                                                        1 H' = 2.984 inches
      2 j = -
                                                                                                       (19)
                                  2
                                                                                                                                        2.654 \times 2.793
                                                                                                                         2 H' = -
                                                                                                                                                                   -=2.667 inches
                                                                                                                                                                                                                            (24)
                   5.236 - (2.43 + 2.78)
                                                                                                                                                 2.78
                                                           = 0.013 inch
                                                                                                       (19)
                                  2
                                                                                                                                          2.356 \times 2.443
                                                                                                                                                                  -=2.370 inches
                                                                                                                         3 \quad H' = -
                                                                                                                                                                                                                            (24)
                   5.236 - (2.25 + 2.99)
                                                                                                                                              2.43
                                                           - = 0.000 inch
                                                                                                       (19)
                                    2
                                                                                                                         4 H' = 2.248 inches
                   5.236 - (2.31 + 2.92)
                                                                                                                                         2.281\times 2.313
                                                           -=0.003 inch
                                                                                                       (19)
                                                                                                                         5 H' = -
                                                                                                                                                                   = 2.283 inches
                                                                                                                                                                                                                            (24)
                                                                                                                                                 2.31
```

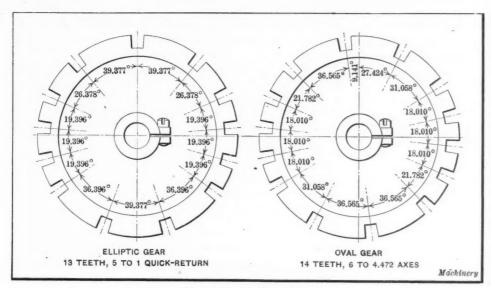


Fig. 9. Index Ratchet Wheels

Machining the Gears

Of the numerous dimensions and calculations required for the correct design of the gears in the drafting-room, but three are of interest to the operator cutting the gears, after the proper cutter, or cutters, have been selected. These are the angle included between the tooth-space tangent and the major axis of the gear (or the angularity of the ratchet index), the horizontal and the vertical setting for the machining fixture. Any other information given to the machinist is likely to create confusion and lead to errors in his exacting task. A machining fixture secured to the table of the milling machine employed for cutting the teeth is the only special equipment required.

A simple and essentially practical fixture employed by the Bilgram Machine Works carries an arbor that may be set at any predetermined angle, upon which the blank to be cut is mounted on its bore. The angle at which the arbor is set is the angle included between the tooth-space tangent and the major axis, or the complement of such angle, and varies for the different tooth spaces. The distance between the parallel planes of the machining-fixture arbor and of the rotary cutter is adjusted for each individual tooth space so that the distance between the plane of the arbor and the parallel plane tangent to the pitch circumference of the rotary cutter in the cutting plane equals the vertical setting for the machining fixture previously determined. The coordinate setting of the fixture (or the horizontal setting for the machining fixture) is the distance between the plane of the rotary cutter and a

parallel plane passing through the arbor of the fixture. This is similarly set, for each individual tooth space, to conform to the calculated value. These three adjustments must be made for each tooth space, and it is this multiplicity of adjustments that makes the cutting of elliptical gears intricate.

The teeth should be cut in consecutive order, so that the angular adjustment of the fixture arbor, though varying in amount from tooth space to tooth space, is always in the same direction. In the multiple production of elliptical gears, this is taken advantage of by mounting on the fixture arbor a ratchet wheel with notches that conform to the angular adjustments for the various tooth spaces. The most convenient ratchet wheel

is circular and concentric with the fixture arbor so that the notches in its circumference are of varying pitch, their angular pitch conforming to the angle included between the center line of the rotary cutter and the major axis of the gear blank in successive positions. The 0—180 degree ratchet diameter should conform to the major axis of the gear. The ratchet angle for the normal for any particular notch is referred to in the notation and the examples as the "angularity of ratchet index." For any particular tooth space, this is the complement of the angle included between the tangent at such tooth space and the major axis. This arbitrary fixing of the ratchet angularity is dependent on commencing the cutting of the teeth at the small end of the gear; the first tooth space to be gashed is that on the major axis for elliptic gears, or that immediately to the left of the major axis for oval gears.

Fig. 9 illustrates the location of ratchet notches for the gears proportioned in the examples. The use of such ratchet indexes materially simplifies the question of the angular adjustment of the fixture and at the same time aids in securing uniformity in the product, the operator being relieved of much of the difficulty in making adjustments. Still further accuracy can be secured, when the gears are not of unusually wide face and can be securely bound together, by cutting several blanks at the same time. This is not always advisable, however. If the hubs of the gears are appreciably longer than the face of the gears, little time is saved; and should there be any variation in the metal of the blanks, there is increased danger of error through the work being forced out of alignment.

When the gears do not differ greatly in their major and minor axes-when their pitch outline does not vary much from a circle—the same cutter may be employed for all teeth; but when the ellipse is comparatively flat and there is considerable difference between the major and minor axes, a different cutter should be used for the major-radius segments from the one used for cutting the tooth spaces falling within the minorradius segments. The cutter is selected, not for the number of teeth in the elliptical gear, but for the number of teeth of the same circular pitch that would be required for a circular gear having a diameter equal to twice the segment radius. For instance, the minor radius of the elliptic gear of Example 1 is 1.854 inch, the major radius is 3.764 inches, and the circular pitch is 1.2742 inch. The cutter for the spaces within the minor-radius segments should then be selected for a circular gear of the same pitch but with from nine to ten teeth  $(2 \times 1.854 \times 3.1416/1.2742)$ ; and the cutter for the spaces within the major-radius segments the same as for a circular gear with from eighteen to nineteen teeth (2 × 3.764 × 3.1416/1.2742).

Men who strive to build themselves up by tearing down the work of their fellows generally succeed in undermining their own foundations and falling into the common ruin. The secret of success is cooperative effort and giving to everyone credit for that which is his due.

# MODERN TOOLMAKING METHODS

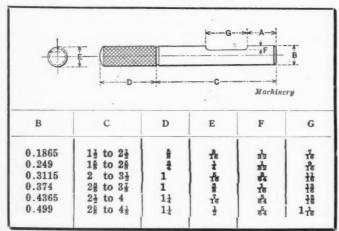
Progress is being made rapidly in manufacturing methods, and the mechanic who does not keep posted is likely to be left hopelessly behind the times. Many still have the conception that toolmaking is the making of odd tools from time to time as required in the shop; they do not fully realize that modern toolmaking is a highly developed business, carried along on manufacturing lines. A toolmaking concern that made tools as they are made in the tool-rooms of many manufacturing plants would soon close its doors. By pursuing manufacturing methods, however, a modern toolmaking concern is able to produce a great variety of small tools that are of superior quality at a comparatively low labor cost.

Many of the operations of toolmaking which have been regarded as within the capacity only of an experienced toolmaker are not necessarily those that cannot be performed satisfactorily by apprentices or other beginners. As a mat-

TABLE 1. REMOVABLE TONGUES

30		1-m	2 1 4	3"	
A.	D	н, е	F	16 K	Machinery H
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TABLE 3. PUSH-PINS



Dimension A varies with the part to be held in the jig, and should be given on the tool drawing.

ter of fact, an apprentice may be taught quickly to do a variety of lapping operations, for instance. It does not require a great deal of skill and experience to be able to lap the holes in milling cutters after hardening so that a plug gage will fit freely but without shake.

It is by specializing and dividing tool work into its elementary parts and assigning them to mechanics of moderate skill, that the economies of modern manufacturing toolmaking practice are realized.

#### CORRECTION

The elevating truck shown in Fig. D on the first page of "Factory Transportation" in the July number is a Stuebing truck made by the Stuebing Truck Co., Cincinnati, Ohio, and not a Barrett-Cravens truck, as stated in the caption.

# MISCELLANEOUS STANDARDIZED PARTS FOR JIGS<sup>1</sup>

BY R. F. POHLE 2

Tongues in the base of small fixtures are generally shaped from the casting itself. At times, however, it is desirable to be able to remove a tongue; for example, to reset it at right angles to its former position, thereby enabling an operator to mill, plane or slot a right angle without disturbing the work. In a fixture of this sort, grooves are milled in the base, into which the tongues are inserted. Tongues of this kind are also used to fasten into the base of long fixtures, say 12 inches or over. They will not collect dirt as readily as a planed tongue, and will thus eliminate the danger of improper seating and enter the platen slots more readily. It is not necessary to mill grooves for these tongues. They should, however, be doweled in place. Tongues are made of steel as shown in Table 1. The 30-degree angle at the lower corners is of no consequence. The tongues may be made square just as well.

TABLE 2. POPPETS

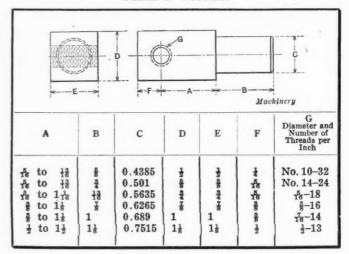
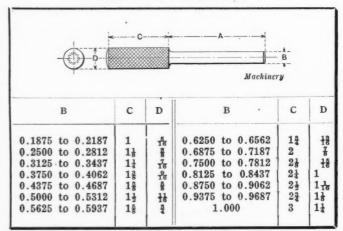


TABLE 4. KNURLED PINS



Dimension A varies with the part to be held in the jig, and should be given on the tool drawing.

In Table 5 are shown the proportions of what are generally called "seats." Seats are solid supporting points that come in direct contact with the work. The question of whether a seat should be of cast iron, finished, or of steel, hardened and ground, is decided by the conditions under which the designer is working. Where the number of pieces to be operated upon is not very great, or where the dimensions of the work show that it does not require to be very accurate, a cast-iron seat will probably give satisfaction. When tools are expected to produce duplicate parts within small limits of variation, hardened and ground steel seats, Table 5, may be relied upon.

A device known as a poppet is shown in Table 2. Poppets

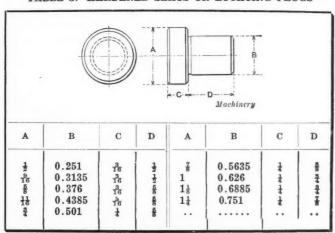
are used quite extensively; they serve as a lug to support an <sup>1</sup>The tables of standards given in this article embody the practice of the General Electric Co., at Lynn, Mass. These standards were developed for the company by R. F. Pohle, when in charge of the tool designing department. <sup>2</sup>Address: 265 Union St., Lynn, Mass.

adjustment or holding screw when it is preferable not to have a lug on the casting itself. For instance, to facilitate the production of the jig or fixture, one might want to shape or plane a surface, an operation that would be difficult and expensive if a screw-supporting lug was in the way as part of the casting. Also, at times, the hole in the lug may not be accessible for drilling and tapping. Poppets are also used to support drill bushings.

Milled push-pins, as shown in Table 3, are used in small jigs and on very delicate work. They provide a removable supporting point for the work, replacing the screws commonly used, and thus eliminating danger of distortion of the work or jig by the operator. Push-pins can also be more quickly removed than a screw, an advantage which may be borne in mind. They are milled as shown, not only to keep the binding screw from burring the pin, but also to keep the pin from falling out.

The knurled pins in Table 4 are simply hardened and ground pins used either to insure the proper placing of the work (after which the pin is removed), or to pin together two loose parts of a jig. In the latter case, the pin, as well as the bushings that it enters, is tapered. It is used, for instance, in a swinging side leaf or a cover that may not otherwise be

TABLE 5. HARDENED SEATS OR LOCATING PLUGS



supported. Tables 6 and 7 simply give information as to the proportions of spring posts and knobs. The functions are quite apparent.

The primary object of this article is to call the attention of designing engineers to the fact that many parts of jigs and fixtures may be standardized, numbered, made by apprentices instead of skilled toolmakers, and kept in stock. It will also do away with the drawing of these parts over and over again by tool designers.

TABLE 6. SPRING POSTS

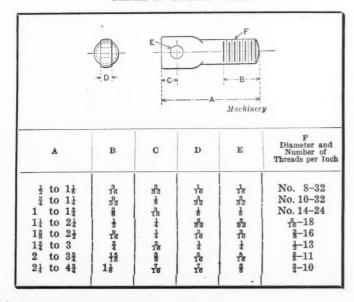
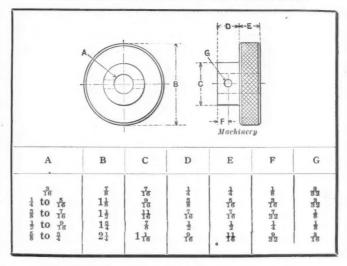
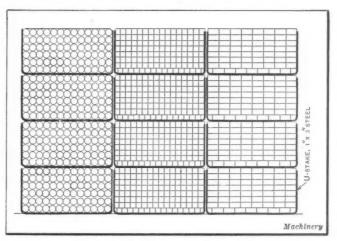


TABLE 7. KNOBS FOR JIGS AND FIXTURES



# U-STAKES FOR PILING BAR STOCK

Racks for bars, strips, rods, pipe and other long metal stock are costly to construct and inconvenient to use. They are also inelastic and difficult to move when changes in the store-room are necessary. Racks may be avoided in many places by using piling stakes made of 1- by 3-inch steel bars bent to U shape, the U having a flat bottom and square corners, instead of a rounded contour. The stock is piled in these stakes, one being placed near each end of the pile. The width of the U-stake or frame may be from 30 to 36 inches and the height about 18 inches. When the pile has reached the top of the frames, another pair of frames is laid on the pile and the piling continued to any height required. Tiers may be ranged side by side, as indicated in the accompanying illustration, which shows piles of rounds, squares and flat stock, each held securely and neatly by the U-frames. When the stock is re-



Illustrating Use of U-stakes for piling Bar Stock

moved, there is no unsightly rack left to encumber the spot; the U-frames may be stored until required again, and new stock may be piled elsewhere if more convenient.

The number of establishments making watches, watch parts, and watch movements in this country decreased from thirty-seven in 1869 to fifteen in 1914. The number of employes increased from 1800 to 12,390; the wages, from \$1,304,000 to \$7,524,000, and the value of the products from \$2,819,000 to \$14,275,000. In the same period the number of watch-case factories fell from forty-nine to thirty-one, while ! .e value of the products increased from \$2,333,300 to \$7,821,000. In 1909, however, twenty-nine establishments produced cases to the value of \$10,514,850. The imports of watches and watch parts have grown from \$2,293,670, in 1911, to \$3,362,720, in 1916, while the exports fell from \$1,560,870 to \$1,524,430. In 1915, only \$914,770 worth of American watches and watch parts were sold abroad.



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We solicit contributions from practical men on subjects pertaining to machine shop practice and machine design. All contributed matter published exclusively in MACHINERY is paid for at our regular space rates unless other terms are agreed on.

### FARM TRACTORS NOW AND AFTER THE WAR

The world is facing a shortage of food, now and after the war, and it is imperative for the farms to produce the maximum of food products at a minimum of cost. Farmers generally depend on animals for tractive power, but it is evident that in this mechanical age animal power must give way to tractors, which are propelled by engines fed by fuels cheaper than hay and grain-the food of the horse. The tractor is economical of farm labor because of the concentration of power under the control of one man. A tractor capable of exerting the draft power of many horses can be readily handled by one man, with comparatively little mechanical knowledge. The high-powered tractor capable of hauling ten plows at a uniform speed of 2 1/3 miles an hour, and operated by two men, will in a day of ten hours plow as much land as could be turned over by twenty single plows drawn by horses.

The adaptable farm tractor is that which can be used for all agricultural purposes, and which may also be used with a fair degree of efficiency for hauling produce to market. This combination of qualities is difficult to secure in one machine, but it is essential for the small farmers in the East to secure in one machine all the draft qualities of the horse in order to minimize investment.

difficulty in the development of tractors and other machines driven by internal combustion motors, is the high price of gasoline and the apparent limitation of the world's supply of petroleum. The prospect of cheap alcohol seems remote. There is, it is true, the possibility of making gasoline from oil-bearing shales, but at present the cost of gasoline so produced is greater than that made in the ordinary way.

The future development of transportation methods on land and sea and in the air, and the improvement of agricultural conditions, hinges on the internal combustion motor. The improvement of motors and the development of cheap liquid fuels are fascinating subjects for invention and investigation.

## . . . REPLACING OLD MACHINE TOOLS WITH NEW

Now is the time for owners of manufacturing plants to consider ways and means for increasing the productive capacity of their plants without adding more buildings, which the present high cost of materials and labor will make an excessive burden in future. Never was it so necessary for owners and managers to give close attention to the interior arrangement of their plants, methods of routing work, and efficiency of machines. Many plants have machine shops in which there are machine tools that should have been scrapped years ago. It is not uncommon to find lathes thirty or forty years old that are still in use. These old-timers take up the same area of floor space as a modern machine tool with a productive capacity of fifty to one hundred per cent more. Obviously, the simplest way-and the cheapest in the end-to increase the productive capacity of an out-of-date machine shop is to discard the ancient tools and replace them with modern equipment. The labor cost will be decreased and the productive capacity of the plant, as a whole, materially increased.

There are few manufacturing plants in which the floor space is utilized nearly to its capacity. The use of efficient machine tools is a step in the right direction; efficient transportation means, and methods which prevent congestion on the floors and which keep the operators supplied with work is another. An important matter to be considered when purchasing new machine equipment is the floor space occupied. In some cases it will be found that the vertical type of machine tool is best suited to the product, and that the floor space required is less for a given production than it would be with machines of the horizontal type. If the horizontal type is required-lathes, for example—they should be no longer than necessary to accommodate the maximum length of piece to be produced. It is a mistake to purchase engine lathes with long beds when the maximum length of the pieces to be turned requires short bed lathes only.

## IMPORTANCE OF STUDY OF SHOP MATHEMATICS

Mathematics may be said to be the foundation of all engineering. Without the aid of the processes of arithmetic, even the simplest mechanical work could hardly be done. In the design of machinery, and still more in the design of great engineering structures, calculations of a more or less advanced nature become absolutely necessary. Any mechanic with a limited education who contemplates the study of mathematics should make certain that he has fully mastered arithmetic. Just as mathematics is the basic science underlying engineering, so arithmetic is the basis of all mathematics. Without a thorough understanding of every process in arithmetic, other mathematical studies become difficult, if not impossible.

Many shop men refrain from using handbooks and other mechanical books containing formulas because they believe that an understanding of algebra is necessary in order to make use of such formulas as are given in handbooks. This idea is erroneous. With few exceptions, the formulas given in handbooks intended for machine shops can be used by anyone who thoroughly understands arithmetic. All that is necessary is to spend an hour or two reading an article explaining the purpose and use of formulas. In mathematics, a number of abbreviations, signs and symbols are also used; and it is of considerable value to the man who reads mechanical literature and occasionally uses formulas to memorize the commonly used signs and abbreviations. This will facilitate his progress and make it easier for him to grasp the meaning of a formula which otherwise would be obscure.

Closely allied to the use of formulas is the use of diagrams. A formula records a mathematical statement by means of symbols or letters, while a diagram records a similar statement graphically by means of lines. Many mechanics regard a diagram as something difficult to understand, but this is not the case, as anyone can easily find by studying a few of the diagrams presented in the mechanical journals.

The student who wishes to go further into the study of elementary mathematics should begin with a simple course in the solution of triangles and elementary geometry. If he wishes to proceed still further, he should take up logarithms and the solution of equations, and in connection with the latter subject he would acquire the rudiments of algebra.

#### THE LAW OF WARRANTIES

BY CHESLA C. SHERLOCK 1

There are two kinds of warranties under the legal conception of the term, viz., express and implied. An express warranty is a special warranty that expressly binds the maker thereof as to the fitness of a particular thing; while an implied warranty is a guaranty implied from the nature of the thing, the relation of the parties, or the agreement between them. Warranties cover a wide field and take in almost every phase of contractual relations. As applied to machinery, some special rules are in force that do not apply in other cases. Especially valuable and interesting is the rule of law as to which warranty governs a sale; that is, does the fact that a manufacturer expressly warrants a machine exclude or include implied warranties, or must the purchaser stand on the express warranty alone?

The Kentucky courts state the general rule to be that where there is an express warranty, there is no implied warranty. In the case under consideration, the contract provided that the machinery was sold subject "to the following express warranty and agreement, and none other." In Michigan, the rule is held to be that if there is "an express warranty as to the working qualities of machinery, there is no implication that the machinery is fit for the purposes for which it was purchased." In Indiana, the court said that although it is true that when a machine or other article is sold for a particular purpose there is an implied warranty that it is reasonably fit for the purpose for which it was made and sold, this rule does not apply where there is an express written warranty, since, in such cases, implied warranties are excluded. In Georgia, it is said that only in the absence of express warranties can resort be had to an implied warranty that a machine is reasonably fit for the use intended. In Illinois, the rule is: "Where a manufacturer furnishes a heating apparatus designed for heating a specific building, he impliedly warrants the sufficiency of the apparatus for the purpose intended. This implied warranty, however, cannot be availed of if the apparatus is sold upon an express warranty as to the temperature to which it will heat the rooms which it is designed to heat." In a Wisconsin case, it was stated that an express warranty of workmanship and material of cream separators excludes an implied warranty of fitness. In a Maine case, the court said: "The existence of an implied warranty that an automatic governor should be suitable for the purposes of the buyer's plant is negatived by the fact that the contract of purchase contained an express warranty as to quality as well as to speed, and the governors were such as the seller in the ordinary course of his business manufactured for the market. the general rule being that where an express warranty is made upon a sale, no other will be implied." The Missouri courts, however, have taken the other side of the question. have held that there might be express warranties that do not exclude implied warranties, as there are any number of implied warranties that were never contemplated at the time the express warranties were made. This exception was not held, however, to apply to an implied warranty which in itself formed an integral element of the express warranty, into which it merged and by which its effect was circumscribed. The holding of the Missouri courts is on the theory that the express warranty is as to something wholly independent of the implied warranty. This distinction is as important as the distinction between express and implied warranties themselves.

It is a general rule, then, that an express warranty as to a particular phase of a thing will exclude all implied warranties as to the same thing. This rule is supported by the great weight of judicial authority and is practically universal. There are, however, some exceptions to the rule that are equally well supported by the weight of authority. In order for the general rule to apply, the character of the article warranted, as well as the express warranty thereto, must include all implied warranties on the same subject. The express warranty must also be of such a nature as to negative any contention that the manufacturer intended to assume any other obligation than the one assumed in his express warranty. If

such a tendency does clearly exist, the courts are likely to declare that the implied warranties and the express warranties are separate in the particular case.

The law of warranties is so comprehensive a subject that it is possible to state here only the rules in force in cases involving machinery. The rules of law are the guide posts that point the way, and when a man is once familiar with these rules, he may proceed without stumbling through a maze of hazy legal decisions and counter decisions. The things to remember are that an express warranty excludes all implied warranties to the same subject, and that implied warranties will be considered either in the absence of express warranties or where it can be inferred from the agreement of the parties or the nature of the thing warranted that implied warranties were not intended to be included in the express warranty.

# RELATION OF RATE OF COOLING TO PHYSICAL PROPERTIES OF FORGINGS

Two locomotive driving axles were used in some experiments recently conducted to study the rate of cooling in different medias and to try to connect the rate of cooling with the physical properties obtainable in quenched and tempered forgings. One of these axles was 11 inches in diameter and weighed 1830 pounds; the other was 12 inches in diameter, had a 3-inch hole bored longitudinally through it, and weighed 2000 pounds. In each case, the axles were heated uniformly as for quenching in the usual course of manufacture. The cutting compound used for quenching was composed of mineralized lard oil and soft soap mixed with equal parts of water. It was later diluted to one part of compound and two parts of water, and still later to three parts of water.

The tests show that in air the solid axles cool at a rate of 10 degrees F. per minute; in heavy oil, 26 degrees Baumé, at the rate of 25 degrees per minute; in the oil solution, at the rate of 35 degrees; in light oil, 29 degrees Baumé, at the rate of 45 degrees; and in water, at the rate of 80 degrees. The bored axle cooled in both the heavy oil and the cutting compound at the rate of 40 degree per minute. It was found that the dilution of the compound had little effect on its quenching properties.

In the case of the bored axle, it was found that when the 25 per cent solution of cutting compound was used, the axle cooled from 1450 to 700 degrees F. in 16.1 minutes. Its elastic limit was 40,500 pounds per square inch; its tensile strength was 78,000 pounds; its elongation in 2 inches, 29 per cent; and its reduction in area, 55 per cent. But when placed in the 33 per cent solution, the bored axle cooled in 13.6 minutes; its elastic limit was 43,000 pounds; its tensile strength, 81,500 pounds; its elongation in 2 inches, 30 per cent; and its reduction in area, 53.5 per cent. It was thought, however, that this more rapid cooling was due to some local condition that affected the convection of the bath.

When a jet of compressed air was introduced into the bath to give it a vigorous circulation, the rate of temperature fall was increased 80 per cent. Carbon steel that in the still bath had an elastic limit of 49,500 pounds per square inch, a tensile strength of 95,000 pounds, an elongation in 2 inches of 20.5 per cent, and a reduction in area of 43.5 per cent, when quenched in the agitated bath had an elastic limit of 68,800 pounds, a tensile strength of 105,300 pounds, an elongation in 2 inches of 21 per cent, and a reduction in area of 42 per cent. Chrome-vanadium steel axles quenched in a still bath had an elastic limit of 80,500 pounds per square inch, a tensile strength of 123,500 pounds, an elongation of 20.5 per cent, and a reduction of area of 57.5 per cent. When quenched in an agitated bath, this steel had an elastic limit of 90,000 pounds, a tensile strength of 124,000 pounds, an elongation of 16.5 per cent, and a reduction of area of 61.5 per cent.

Last year, 4676 automobiles were imported into Argentina, against 1847 in 1915. Most of these were small cars designed particularly for country use, as such cars are becoming popular among the farmers.

If <sup>1</sup>Abstract of a paper by Lawrence H. Fry, read before the Iron and Steel Institute of Great Britain, May, 1917.

# SNAPSHOTS ON THE ROAD

THE RIGHT SIDE OF A PIECE OF STEEL-ASSEMBLING A CLOCK MOVEMENT IN TWO MINUTES-BROACHING CAST IRON-DUPLICATE FORM TURNING-WHAT'S THE MATTER WITH THE MUNITIONS MAKERS?-HOW A DOUBLE-ANGLE MILLING JOB WAS HANDLED-LAPPING GAGES FOR PROFIT-USING UP HIGH-SPEED STEEL DRILLS

BY THE FIELD EDITORS



"-the bottom side hardened to perfection while the face was

HERE are still a few shops in the country that make use of what known as "composite steel" for blanking die work. Composite steel is formed by rolling together a piece of iron and a piece of tool steel. The result is a plate. one side of which is steel and the other iron. It has been claimed that a die made from this steel could be machined with less trouble than a solid steel die, and with practically no danger from cracking in hardening. While looking around through one of these shops where composite steel had

been a great favorite, we heard the following incident, which has a mechanical moral:

"It was in the days when I was toolmaking," said the manager of the jewelry making plant—"and I was considered a pretty good die-sinker, too—that one day we had a little emblem die to make from which but a few strikings were required, so I picked up a scrap of composite steel and commenced to sink the design. After working on this for five or six hours, I tumbled to the fact that it worked too soft, and the horrible suspicion came to me that I had the piece of composite steel wrong side up and was cutting the design in the iron face of the plate instead of the steel. The longer I worked at it, the surer I was that I was wrong, and as soon as I tried to harden the die I was positive, for the bottom side hardened to perfection while the face was as soft as cheese.

"Someone has made the remark that during the few seconds' interval between the time when think you have made a mistake and when you find out whether you have or not, you are getting real experience. Well, I went through those seconds and got the experience, but the next thing was how to get out of the dilemma. It was a rush job and we had no time nor facility for pack-hardening, so I casehardened with cyanide, soaking in the cyanide to get all the depth of case possible. Even then I doubt if the die would have passed, even for the small number of parts required, if I hadn't gotten on the right side of Old Tom, the drop man, and told him that I suspected that die was made of a poor piece of steel and to nurse it along as carefully as possible. Old Tom got out the

order, but he did some cussing and declared at the end that that sure was some bum steel in that die."

# Assembling a Clock Movement

In going about the field, many examples of manual dexterity are seen, especially in factories where girls are employed. Recently, while in a Connecticut clock shop, the superintendent called attention to the assembling of a movement for a cheap alarm clock. The girls on the job had large compartment trays, each space of which contained a quantity of wheels or shafts of one kind. The assembler dropped one of the frame plates of the movement onto a simple little fixture before her and with her right hand rapidly reached for the various wheels and shafts, located them in the frame,

and held them in place with her left hand.

How that right arm did fly! After she had all the wheels in their correct places in the frame plate, still loosely held in her left hand, she fitted on the top plate. With a quick little shake, at the same time rapidly adjusting the various parts with her left hand, she had the shafts and other parts in the proper



"With a quick little shake . . . she had the shafts and other parts in the proper pivot holes"

pivot holes in the two plates. The top plate was held in place by twirling two little nuts on diagonally opposite parts and the job was done—total elapsed time, less than two minutes!

#### Broaching Cast Iron

"We worried a lot over this machining problem," said the chief engineer of the plant that we were visiting, "and you will be interested to know how we finally solved the problem. Now here's what we had to do," said he, as he reached for a piece of paper and rapidly sketched away. "You see, there's an irregular cored slot that runs out of this cast-iron plate, which, by the way, is one inch thick. Of course, you will see we couldn't mill these quickly without a profiler, and our production wasn't great enough to install such a machine. We got through the job very nicely, however, by broaching."

"But we have always considered the broaching of cast iron a rather difficult job on account of the tendency to break out at the end of the broaching cut."

"You're dead right there, and that made the job all the more interesting. See, here's how we overcame that breaking-out tendency. We used three broaches for the job; the first left the outline of the slot in a succession of notches, just as I'm drawing it. We followed this broach by a second one that took 'bites' out of the center of each of the notches. Then we finished up with a plain broach that took the ridges from the slot and left it as finely finished as you could desire and without the sign of a break at the end of the cut."

"That's sure a new wrinkle in broaching," said we, "and a mighty good one to remember."

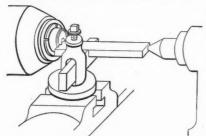
#### Duplicate Form Turning

It is surprising how often you see a new kink in some little shop where you wouldn't expect to find anything more modern than a grindstone. You may have to unearth it from beneath a pile of obsolete practice, but when you get it out it looks pretty good. Such was the case in a little job button manufacturing concern in good old New England. It seems that this company often has a set of fifteen or twenty sample buttons to turn, or molds for making buttons, or possibly punches for press work. It is necessary to face the molds or punches with the concentrically turned form and the exact form of the rings does not matter as long as they are all alike.



"We used three broaches for the job; the first left the outline of the slot in a

The boss lathe hand is an ingenious Yankee, and he has a "universal" form-turning tool that you can understand better from the sketch than from a page full of words. This form tool is made from a rectangular piece of steel about three-eighths by one inch and the shank is fitted in a slot in a block held in the toolpost, and is operated from the tail-center. The operation is simplicity itself. The lathe hand merely adjusts the tool by means of the cross-slide and feeds it in with the tailstock. The slot in the block of the cross-slide insures each punch, each button mold part or punch being turned exactly



"The boss lathe hand . . . has a 'universal'

the same. A great number of variations are possible by merely moving the cross-slide and hence the tool, and as long as the cross-slide is moved the same amount for each operation, the pieces are exact duplicates.

It is a simple little kink and there ought

to be many ways of applying it to general machine shop practice.

#### What's the Matter with the Munitions Makers?

We recently ran into a fine example of "frenzied buying" as done by one of the mushroom munition plants that have been so much in the limelight of late. It was told to us by an efficiency expert who had been called in to straighten out things after they had run so wild that no one knew where they were "at." One of the grinding-room foremen wanted a diamond for truing grinding wheels, and put in his requisition. He stated the approximate size that was required, and one of the buyers of the purchasing department promptly got busy and bought a pure, flawless, blue-white diamond, for which he paid the meager sum of \$900. The interesting part of it is that they did not send the diamond back, but actually put it into service truing grinding wheels.

Another glaring example of inefficiency was in an order of dies that was placed soon after the plant was started. An order for twenty-four duplicate dies for punching one particular part was given to a diemaking concern. The order was delivered promptly by putting every man in the shop on the job. After several months, it occurred to the diemaking concern that there ought to be another order coming for dies if such quantities had been needed before, so the manager went around to interview the purchasing department of the munitions plant. Being somewhat friendly with one of the purchasing agents, he naturally put his proposition to his friend. who simply smiled and said, "Come with me for a minute." Out through the shop they walked and into one of the storehouses, and there, stored in an orderly fashion, were twentythree sets of the dies. These dies were all slushed with grease just as they had been received and had never seen service.

"Well," said the die manufacturer, "what's the answer?"

"Simplicity itself," was the reply. "The engineering department ordered us to secure twenty-four sets of dies for this part before they were sure that the part was exactly what they wanted. After a few thousand impressions had been made from the first set, they discovered that they were on the wrong track, and consequently these twenty-three sets of dies are scrapped."

## How a Double-angle Milling Job was Handled

"Say," said the master mechanic, "we've just finished solving a pretty little milling job for producing a piece like this one I'm drawing, and I'll be interested to hear how you would have done it." The piece referred to was made of carbon steel and its end was dovetailed as shown. The complicated part of it was that the edges were not cut straight

"I yust pull up mein chair side mit de lapping block, light mein pipe, and make one hand go so and so, while I read mein

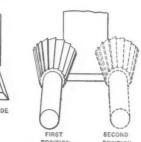
across, but on an angle of about 5 degrees, similar to a milling cutter tooth.

"And before you decide just how you would have handled this," said the superintendent, "remember that it's a manufacturing job on which we must have thousands of parts, and we can't stand for a special machine, because on munition work the styles are apt to change at ten minutes' notice."

We racked our memory for a similar job without success, and, finding none, had to appeal to the superintendent for the explanation.

"Well, the solution was so simple it was funny we didn't strike

it long ago. We simply had a special end-mill made to agree with the dovetail taper, and holding the pieces one at a time in a special fixture on the hand milling machine, ran the work straight up onto the cutter, but not across it; the resulting surface was angular and slightly concave. Next



"the solution was so simple it was funny we didn't strike it long ago"

we dropped the work, ran it around the cutter to the opposite edge and milled it in the same way, and we got as pretty a result as you could want.

"Of course," concluded the superintendent, "you'll say we didn't get a perfectly true angle by using the surface left by a cylindrical end-mill, and you're right, but the resulting slightly concave surface was highly satisfactory and made an even better fit in the slot than it would have if it had been straight."

#### Lapping Gages for Profit

"Before you go," said the tool-room foreman, "sit down here and let me tell you about a big job of gage lapping that we had in the shop some time ago and how we handled it. You see, we only had one good man who could lap work and get away with it, and it was soon evident that we wouldn't be able to get the job out on time if we depended only on his ten-houra-day services, so we asked him about taking some of the work home and doing it evenings; we thought it would be pleasanter than staying at the factory, as none of the other men were working overtime.

"Schwarz was a big, good-natured German of a philosophical turn of mind. Every morning he brought in a good number of lapped gages and soon the contract was over. His overtime work did not seem to tire him, so one day, when the work was nearly done, I asked him how it was he could stand so much extra work without tiring, and he replied:

"'Oh, dot vas easy. I yust pull up mein chair side mit de lapping block, light mein pipe, and make one hand go, so and so, while I read mein paper mit comfort, and pretty soon I look at the gage—maybe he be all right, maybe not; that

makes no never minds, I rub him some more and bimeby he sure be done."

"And so it was. Schwarz's gage lapping was no tax on his strength, because he reduced his right hand to an automaton that worked while he read—which wasn't so bad."

# Using up High-speed Steel Drills

High-speed steel turning tools cost money these days, so anything new in the turning tool line attracts our attention. Not long ago we were walking by the tool stock-room of a shop in Syracuse, where we saw an unusual lathe tool. It seems that the company uses a lot of two-inch high-speed steel drills, and when they are worn down too short for the work, they are forged down and the twist is taken out, turning them into lathe tools. The men say they are the finest kind of turning tools, and they make a saving in the steel bill besides.

# GRIDLEY TURRET LATHE EQUIPMENT

CHUCKS, FORMING AND CUTTING-OFF TOOLS, DRILL-HOLDERS, KNURLING TOOL-HOLDERS, TURNERS, BACK-RESTS, ETC.

BY DOUGLAS T. HAMILTON 2

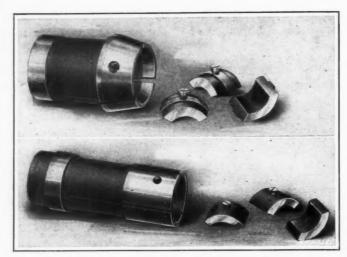


Fig. 1. Master Spring Chuck and Feed Chuck with Gripping Jaws

THE tool equipment and attachments used on the Gridley single-spindle automatic turret lathes do not differ essentially from those used on the multiple-spindle type of machine. The tool-holders, however, are held on flat slides instead of on the corner of the turret, as in the multiple-spindle machines. The standard tool equipment consists of spring chucks, feed chucks, vertical and flat forming tools, blade-type cutting-off tools, drill-holders, facing tools, knurling tools, internal necking tools, turners, high-speed drilling attachments, automatic die attachments releasing tap-holder attachment, and taper turning attachment. Other special tools, of course, can be designed when the character or shape of the work necessitates the performance of operations that cannot be handled with the standard equipment.

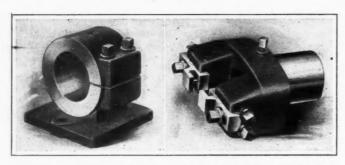


Fig. 2. Standard Type of Toolholder used on Turret Slide of Gridley Automatic Turret Lathe

Fig. 3. Standard Type of Knurling Tool-holder for Use on Turret Slide of Gridley Automatic Turret Lathe

# Spring Chuck and Feed Chuck

The spring chuck and the feed chuck used in the single-spindle turret lathe are exactly the same as those used on the multiple-spindle machines; in fact, the chucks used on the 1¾- and 2¼-inch sizes are interchangeable. On the single-spindle turret lathes, of course, the smallest capacity of the machine is such that the master spring chuck and feed chuck are used exclusively, and these are fitted with bushings to suit the size and shape of the work being handled. The illustration accompanying Table 1 shows the design of the spring chuck, and the principal dimensions are given for the 2¼-, 3¼- and 4¼-inch machines. It will be noticed in this connection that the taper on the front end of the chuck is only 14½ degrees on the 2¼-inch size, whereas it is 15 degrees on the 3¼- and 4¼-inch sizes. Another difference that should be no-

numbers of Machiners, and first installment.

<sup>2</sup>Address: Fellows Gear Shaper Co., Springfield, Vt.

ticed is that the chucks used on the  $3\frac{1}{4}$ - and  $4\frac{1}{4}$ -inch sizes have four slots and four bushing sections, instead of three, as on the  $2\frac{1}{4}$ -inch size.

The illustration accompanying Table 2 shows the type of master feed chuck used and the table gives the principal dimensions. These chucks are also interchangeable with those on the same size of multiple-spindle machines, and the number of slots and bushing sections vary on the  $3\frac{1}{4}$ - and  $4\frac{1}{4}$ -inch sizes, as mentioned in connection with the spring chuck. On the  $3\frac{1}{4}$ - and  $4\frac{1}{4}$ -inch feed chucks, the diameter is not reduced at L, but the diameter A extends from the front back to the shoulder at J; otherwise the feed chucks used on the various sizes of machines are identical in shape. Fig. 1 shows a master spring chuck and a feed chuck with the bushings removed

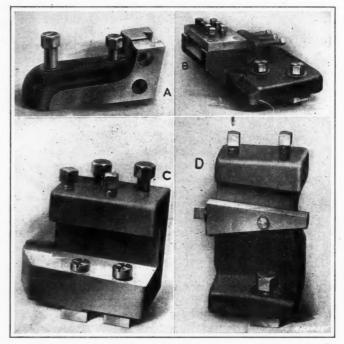


Fig. 4. Forming and Cutting-off Tool-holders used on Gridley Singlespindle Automatic Turret Lathe

and illustrates clearly the shape of the bushings and the method of holding them.

#### Forming and Cutting-off Tools

The forming and cutting-off tools used on the single-spindle turret lathe do not differ materially from those used on the multiple-spindle machine. When an irregular form is to be produced the vertical type of forming tool gives the best results. When several diameters are to be formed and only a small number of parts are to be turned out, individual forming tools consisting simply of blades for covering each diameter are satisfactory. It should be stated, however, that when a large number of parts are to be produced a tool covering the entire form, if possible, is better than a tool made up in separate parts, as it is easier to set up the tool again after

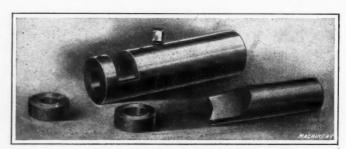
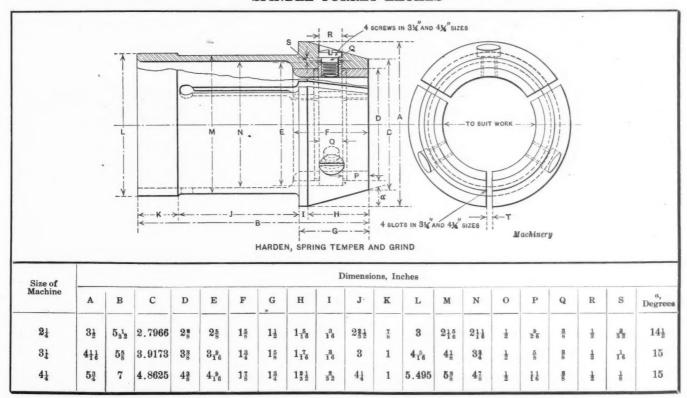


Fig. 5. Facing Tool and Holder used in Standard Tool-holder

<sup>&</sup>lt;sup>1</sup>For other articles on Gridley automatic screw machine practice, see "Gridley Multiple-spindle Automatic Screw Machines" in the June and July, 1917, numbers of Machinery, and the articles referred to in connection with the first installment.

TABLE 1. PRINCIPAL DIMENSIONS OF MASTER SPRING CHUCKS FOR GRIDLEY SINGLE-SPINDLE TURRET LATHES



it has been sharpened. The cutting-off tools are generally of the blade type, except when it is necessary to make them perform some part of the forming operation.

#### Forming and Cutting-off Tool-holders

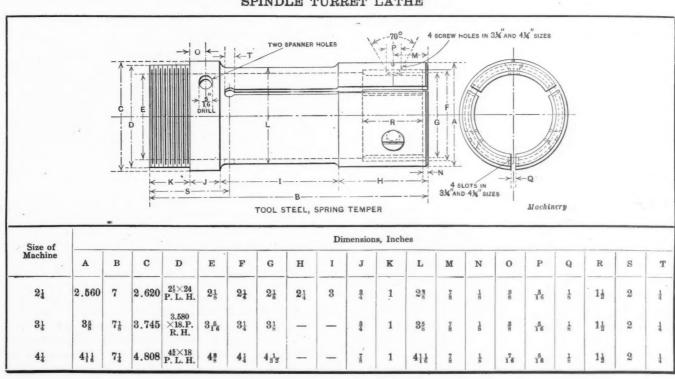
Fig. 4 shows types of forming and cutting-off tool-holders used on the single-spindle turret lathe. That shown at A is known as the vertical tool-holder and is the type generally used, because the cutting tool can be held much more rigidly than in the other designs. The tool also can be ground on its top face without changing the form on the work, and it has a longer life than the straight forming tool.

When the piece to be formed has several plain diameters, the flat forming tool-holder shown at B is sometimes found

convenient. This tool-holder, of course, is only used when there are a small number of pieces to be made and when the expense of making a vertical forming tool would not be warranted. It is also used when several narrow forming tools are required, spacing pieces being put in between the tools and the entire number clamped in the holder. Three adjusting screws are provided, as shown, so that three separate tools can be independently adjusted; they are then clamped by the other set of screws.

The plain forming tool-holder shown at  $\mathcal{C}$  is sometimes used for forming back of the head of a screw or for similar work, so that the cutting-off tool is relieved of considerable work. It is also used for beveling the end of the bars before it is fed out, and thus assisting the turner in starting, especially in

TABLE 2. PRINCIPAL DIMENSIONS OF MASTER FEED CHUCKS FOR GRIDLEY SINGLE-SPINDLE TURRET LATHE



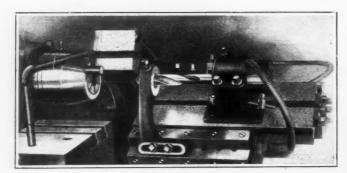


Fig. 6. Standard Type of Drill-holder and Drill-support in Operation

giving the back-rests a chance to support the work when the turning cut starts.

D shows the standard type of cutting-off tool-holder used on the single-spindle machine. This holder, as shown, is fitted with an adjustable taper wedge so that the cutting-off blade can be easily adjusted to correspond with the center of the work. Ordinary forged tools can be held in this holder or almost any type of blade inserted. When a large number of pieces are to be made it is advisable to use a blade-type of cutting-off tool and a holder. This simplifies the sharpening of the tool, as a blade-type tool has clearance all the way back

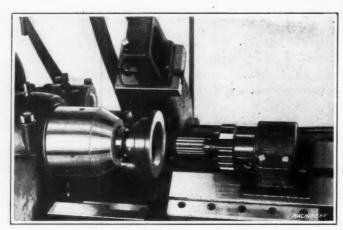


Fig. 7. Standard Tool-holder carrying Reamer

and to sharpen it is simply ground on the front end to the required cutting angle.

#### Tool-holders

The standard type of tool-holder used on the Gridley single-spindle turret lathe is shown in Fig. 2. This tool-holder is bolted directly to the turret slide and is bored out when in place on the machine so that the hole is in direct alignment with the spindle. It is held in place by means of two T-bolts, which, if desired, can be threaded; an adjusting screw laid in the T-slot in the slide can then be used for accurately ad-

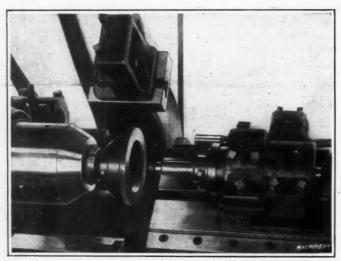


Fig. 8. Standard Holder carrying Reamer and Counterboring Tool

justing the tool-holder longitudinally along the slide. This screw, of course, is provided with a collet head, and a plate attached to the rear end of the slide acts as a stop for adjusting purposes. The various tool-holders are numbered to correspond with the number of the tool-slide to which they are fastened when finished, and should be used only on the tool-slide having that number. They can be used, of course,

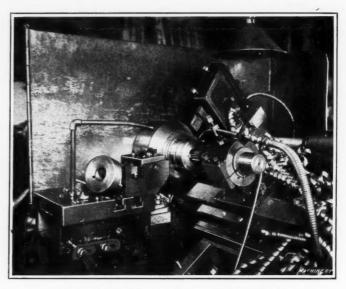


Fig. 9. Standard Type of Reamer Holder at Work

by the substitution of bushings and other independent holders for carrying facing tools, drills, pointing tools, etc. Fig. 5 shows a tool-holder arranged to hold a pointing tool. A separate bushing is provided for guiding the bar, and the pointing tool is held in another sleeve, the latter being retained in the holder.

## Drill-holder and Support

In Fig. 6 is shown the standard tool-holder carrying a twist drill, which is held in a bushing fitting in the holder, so constructed that an oil-tube can be inserted for supplying a coolant to the drill. The drill should be of the oil-tube type, so that the oil can flow directly to the cutting point. In addition, the drill is supported close to the cutting point, by means of an arm which is fastened to the turret in such a position

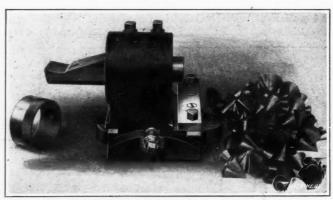


Fig. 10. Set-over Tool and Holder and Chip produced by it

that it is close to the end of the piece being drilled. The arm holds a bushing which fits the drill and accurately guides it in line with the work. This insures the tool starting concentrically and obviates the necessity of using a starting drill.

Fig. 9 shows a standard tool-holder carrying a reamer. The reamer is mounted so that it can float and is carried in a separate bushing in the tool-holder. In this illustration the screw for adjusting the main tool-holder longitudinally can be plainly seen, as well as the forged type of cutting-off tool, and the tool-holder for carrying separate forming tool blades. In Fig. 8 is illustrated another application of a reamer-holder, which is used in conjunction with a facing and counterboring tool. The reamer is of the shell type. The job shown is a

hub which is chucked by hand. Fig. 7 shows still another application of the standard holder. In this case it is used for carrying a boring tool, operating on a chucking job.

#### Knurling Tool-holder

The standard type of knurling tool-holder used on the Gridley automatic turret lathe is shown in Fig. 3. This has a

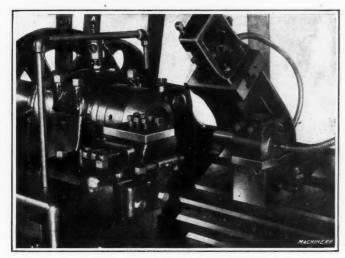


Fig. 11. Internal Necking or Recessing Tool

shank which can be held in the standard tool-holder and carries two adjustable slides that hold the spiral knurls. Two straight knurls can be used when it is necessary to produce a straight knurled effect on the work.

#### Set-over Tool and Holder

An interesting type of tool which takes the place of a drill for producing shallow holes (not more than one and one-half times its diameter) is shown in Figs. 10 and 12. This is known as a "set-over tool-holder," and it can be used with success on the Gridley turret because of the rigid construction of the latter. The cutting tool works the same as a forming tool, but instead of cutting on the outside surface of the bar, as the forming tool does, it cuts into the end of the bar, and as the holder which supports the tool has a set-over adjustment, the same cutting tool can be used for making holes of various diameters. It is not necessary to use a starting drill

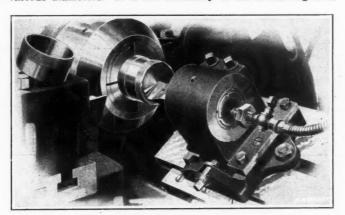


Fig. 12. Set-over Tool-holder in Operation on 3-inch Hole

with this tool and a counterbore can be dispensed with in most cases when the bottom of the hole in the piece is flat.

The cutting tool proper is made from high-speed steel with a hole through its center, so that the cutting edge is thoroughly flooded with cutting oil or compound. This tool is cheaper to make than a drill and can be used for making different sizes of holes, and also as a reamer. Fig. 12 shows the tool in operation, producing a hole that is three inches in diameter. Fig. 10 shows the kind of chips produced with this tool, and the set-over arrangement is also clearly shown. The holder carrying the cutting tool is mounted on a slide which is adjustable at right angles to the axis of the spindle by means of a collar-head screw, as illustrated. This adjust-

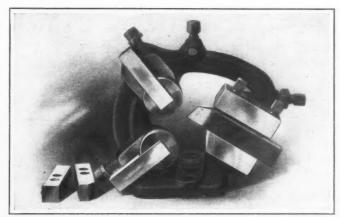


Fig. 13. Standard Type of Turner for Use on Gridley Automatic Turret Lathe

ment is made to secure the desired diameter of the hole in the work.

#### Internal Necking Tool

When it is necessary to make a recess in a hole so as to obtain a bearing at both ends, an internal necking or recessing tool of the type shown in Fig. 16 is used. This tool consists of a base A, which is clamped to the turret slide, as shown, and fulcrumed on this base at B is the main tool-holder C.

This holder carries the recessing tool, which is held by a bushing and a clamping screw, as shown. The recessing tool is centered with the hole by means of the adjusting screw D, which has a collar head that comes up against the bracket E of the holder, and it also is provided with a nut for locking

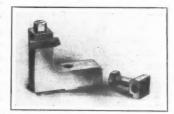


Fig. 14. Knee Turner for Roughing and Finishing Cuts

purposes. The shoulder of screw D is kept against the bracket by means of coil spring F, and after the tool has finished cutting, and the pressure is removed from the holder, the spring returns the tool to the central position. The recessing tool is fed to depth by means of a roller pusher G mounted in a bracket H attached to the edge of the forming slide, as illustrated. The roller bears against a hardened block that is held by screws to the side of the internal necking tool-holder proper. In using this tool for enlarging, or boring a hole, it is necessary, of course, to so arrange the forming cam that the forming slide will be advanced at the proper moment, dwell until the length of bore has been completed, and then be withdrawn. In recessing for a thread or internal form, it is necessary to advance the turret slide and dwell until the forming slide has been fed in to the required depth.

An internal forming or recessing tool that differs slightly from that shown in Fig. 16 is illustrated in Fig. 11. The design in this case is not quite so elaborate; the tool is operated from the forming slide in a similar manner to that shown in Fig. 16.

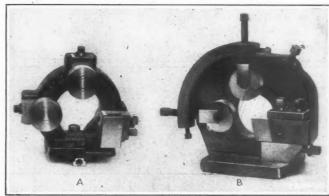


Fig. 15. Standard Turners used on 41/4-incb Gridley Automatics

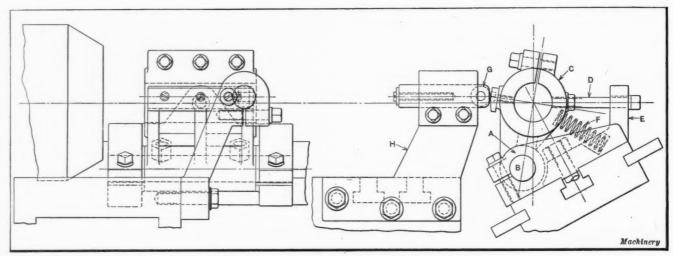


Fig. 16. Another Type of Internal Necking or Recessing Tool-holder

#### Turners and Back-rests

A noticeable feature of the standard turning tool shown in Fig. 13 is the absence of a shank. This holder is in the form of a yoke having a base that is rigidly clamped to the turret slide. At the front it carries a turning tool and at the rear two supports; the latter can be either of the plain type or of the roller type, as shown. The cutting tool in the turner

for the 21/4-inch machine is 1 by 1/2 inch and is ground on the end, as shown. The roller rests permit the use of heavier cuts and coarser feeds, and a cutting speed of two or three times that which can be maintained when the common type backrest is used. These backrests may be used either ahead of or behind the cutting tool, depending upon the character of the work and the cut being taken.

Fig. 17 shows one of these standard turners

at work producing a shoulder screw with the forming tool at because of the heavier duty required in this position. The work at the same time. Forming and turning can be done simultaneously with good results, as the desired rigidity can easily be obtained. This particular setting was used to save time on the single-spindle machine, but if the same job were done on the multiple-spindle machine, two or more turning cuts would be made, thus obviating the necessity for the wide forming cut in the first operation. The same illustration also

shows the adjusting screw for moving the standard tool-holders in a longitudinal direction along the turret slide, to which reference has been made in the foregoing.

At A and B, Fig. 15, are shown two types of standard turners used on the 41/4-inch automatic turret lathe. The one shown at A uses a dovetail turning tool, whereas that illustrated at B uses a forged tool. In both cases adjustable

roller supports are used.

Another type of standard turner, known as an "adjustable stud turner," is shown in Fig. 18. This turner is so arranged that three different diameters can be finished at the same time. It consists of a holder proper, which is clamped to the turret slide and carries individual units, one unit for holding the cutting tool and the other for the back-rest or support. Usually the first support of the group is provided with rollers

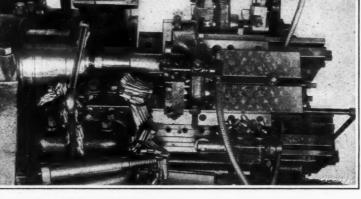


Fig. 17. Standard Turner and Flat Forming Tool working together on Shoulder Screw

turning tools are adjusted by means of a collar-head screw, as illustrated, and adjustment is also provided for the back-rests.

Fig. 19 shows a special stud turner. This is almost of the same design as the adjustable stud turner, except that it is made for a given piece of work and is not adjustable for shoulder distances, that is, longitudinally. The tool-holder proper is solid, as illustrated, and carries, in this case, five turning

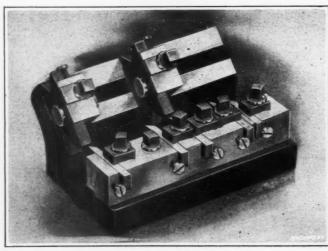


Fig. 18. Standard Type of Adjustable Stud Turner

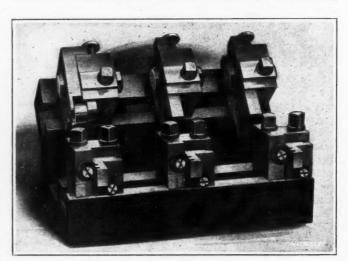


Fig. 19. Special Type of Adjustable Stud Turner

tools. The supports are held so that they can be adjusted along the slide or holder to bring them in the most convenient position relative to the work, that is, where they can give the best support. When the required number of pieces have been made, this tool is put away without disturbing the cutting tools and can be kept until the same piece is to be produced again. In the arrangement shown, it is possible to put the cutting tools much closer together than in the holder shown in Fig. 18.

#### Knee Turner

Fig. 14 shows a type of tool known as a "knee turner," which can sometimes be used to good advantage for removing scale from the work by preceding the drill, reamer or other tool being used. It is narrow, so that it takes up very little space, and can be used in conjunction with some other tool. It cuts on the back side of the bar, so that the forming tool can be operated without backing off the knee turner from the work to get it out of the way.

#### Feeds and Speeds for Turning

The feeds and speeds used on the Gridley turret lathe when using the standard turners vary considerably and are governed entirely by the material and nature of the cut. Because of the rigidity of the machine, it is generally advisable to use a coarse feed and a comparatively slow speed. This statement applies especially in the production of studs or other work when the amount of metal to be removed is considerable. When only light cuts are to be taken, however, it is preferable to increase the speed and decrease the feed, although, as a general rule, the speed can be increased without any corresponding decrease in feed and still give satisfactory results, owing to the elimination of chatter. Each different piece, however, requires a careful analysis of the conditions to be met in order to determine exactly what feed and speed should be used.

#### GRINDING-WHEEL GRADES

"Grade" is a word used to designate the relative hardness of any given grinding wheel. Different methods of indicating grade are in use, the most common employing the letters of the alphabet. One company uses the first letters of the alphabet for the harder grades, the middle letters for the medium grades, and the last letters for the softer grades. Another company uses just the reverse of this method, while others use a system based upon some particular word. Grade is determined by measuring the resistance which a wheel offers to the penetration of a small steel tool resembling a screwdriver. The wheels under inspection are compared with wheels of known hardness, so that all variable factors are reduced to a minimum. The belief is quite common that a grade is an exact value. A grade is not an exact value—it is a range between limits, and all wheels that come within this range are of one grade and carry the same grade letter. A test was made to determine the hardness of each grade as indicated by the tensile strength. A lot of wheels all of the same dimensions and the same size of grain, but of different grades, were slowly speeded up to a point where centrifugal force became greater than the tensile strength of the wheel, and breakage occurred. The number of points per square inch tensile strength to which each wheel was subjected was calculated, and from these figures the following results were plotted: The tensile strength of grade O, Norton scale, ranges between 2100 and 2050 pounds per square inch; grade N, between the limits of 2050 and 1975; grade M, between 1975 and 1875; grade L, between 1875 and 1790; grade K, between 1790 and 1700; grade J, between 1700 and 1600.—Condensed from talk by R. G. Williams of the Norton Co.

The firm of Isaac Best & Co., Ltd., Newton Heath, Manchester, England, recently made what is claimed to be the longest twist drill ever produced. The length of the drill is seven feet. No statement is made of the object of making so long a drill. The makers are patentees of machines for fluting twist drills and reamers and for backing off such tools, and possibly the drill was made merely for advertising purposes.

#### THE TUMBLING BARREL

BY G. R. SMITH 1

One of the oldest and simplest metal-working devices, and perhaps the most useful in its field, is the tumbling barrel. Its operation requires but a small amount of power and the attention of one unskilled workman. The idea involved is not of recent date; it is as old as mankind itself, being simply an adaptation of the oldest of all ideas for cleaning. Have you ever seen your grandmother clean the inside of a stained bottle by shaking in it a few small stones and a little water? That is the principle. The Aztecs cleaned and polished their gold trinkets by placing them in a gourd with a little fine sea sand sifted through bits of porous hides and then shaking the gourd until the gold was clean and bright. The trinkets were brought to a still brighter state by replacing the sand with dry fish scales and again shaking. That is the tumbling barrel in its first form; both the idea and the materials used to help the process and get the desired results are old. In a study of the habits and customs of the savage tribes all over the globe, the same idea is found time and time again; we have simply commercialized it for our use.

About the first tumbling barrel of real commercial value was made by an English inventor, William Lee, between 1585 and 1590; it was used to clean the iron and steel parts of a machine for knitting stockings. The idea was speedily adopted until the tumbling barrel became widely known. Lee's barrel was a crude, hand-propelled apparatus, but the idea was brought out in such a way as to show at once its value. The idea involved, however, is not the product of a certain train of thought, as is the case with many inventions, but rather the development of Nature's own bent. Perhaps the simplest people, the crudest minds, received the idea from seeing the stones whirled around in the pot-holes in the rocks of the streams and rivers receiving a polish by the constant motion caused by the flow of water; be that as it may, the idea is old, simple, cheap and effective.

According to the dictionary, the word tumble or tumbling means to fall suddenly, to roll about, to turn over, a rolling over. That explains the process and is exactly what takes place inside the tumbling barrel when it is in motion and what must take place to make the process a success. This is the one factor the writer wishes to bring out more than anything else. Each piece in the barrel rolls and falls over the other pieces, rubbing and chipping off whatever foreign substance may be clinging to the pieces with which it comes into contact. Whatever material, such as sand, sawdust, etc., may be placed in the barrel with the work is only to aid the process of cleaning; the falling motion of one piece over another is what does the work. If sand and cork, or sawdust, are used with heavy steel work, the sand helps the cleaning process, and the cork, or the sawdust, absorbs the dust that comes from the process and in a way helps to polish the work. If sawdust alone is used, it lessens the severity of the blow of one piece against the others and helps the cleaning process.

#### Cleaning and Polishing Work by Tumbling

In all cases where tumbling is done to clean and polish the work, it is the falling and tumbling of each piece over the others that effects the cleaning and polishing, not the material that is placed in the barrel with the work. The work would clean itself if nothing were mixed with it; therefore, no matter what may be the nature of the work being tumbled, sufficient space must be left in the barrel for it to do its work. Nothing at all will be accomplished if the barrel is filled too full of work or the work mixed with so much sawdust, sand or cork that it is mechanically impossible for the pieces of work to strike against one another. One rule that may be laid down for all classes of work and all sizes of barrels is that the work to be tumbled and the material used to help the process, such as sawdust, etc., should not occupy more than one-third the space inside the barrel, while one-fourth the space is a better ratio to insure success. Many foremen are making a success of tumbling operations by placing in the barrel nothing but the work to be tumbled.

<sup>1</sup>Address: 19 Pond St., Pittsfield, Mass.

So varied is the procedure to get different results on different classes of work that it is out of the question to lay down a set of prescribed rules. Small work, such as very thin sheetbrass blanks, copper blanks, etc., should not be tumbled at all. The same result may be secured much more quickly and at less expense by pickling or the bright dip. There should be little necessity for tumbling punched parts of this kind, for if the blanking tools are kept in shape and ground, there will be no burr, and certainly they should not need annealing in the blank. Small brass and copper castings or drop-forgings may, if really required, be cleaned by tumbling in sand.

One cause of failure is the allowance of insufficient time in which to obtain the desired results. All work must be run until thoroughly treated, whether it takes one hour or ten. The operation costs next to nothing, but it must continue until the result is reached. Nothing can hurry the process and the results of six hours' tumbling cannot be expected in one hour. Another cause of poor results or failure is the amount of sand or sawdust used in proportion to the work. In tumbling five cubic feet of work the writer would not mix more than one and one-half to two cubic feet of sand, sawdust or cork. This must be measured by volume, or quantity, and not by weight, as that is another cause of failure; the sand, sawdust and work will weigh in greatly varying proportions.

Copper and brass punched parts are successfully tumbled for burrs in soft-wood sawdust in from two to four hours. Steel and iron parts may be tumbled in sea sand for burrs, scale in annealing, etc., in from three to six hours' run. Burrs and annealing scale have been removed from steel blanks, say 4 to 6 inches in diameter and 1/8 inch thick, in a five-hour run, with a mixture of sea sand and scrap cork (say two parts cork to two parts sand, by volume, not weight), and this mixture run dry in a ratio of 1 to 4 or 1 to 5 of the steel blanks. Steel blanks 6 inches in diameter and 1/8 inch thick have been tumbled to a good bright finish in a five hours' run in a barrel of one cubic yard capacity, using one-third as much pure sand as work and the whole load being but three cubic feet. Punched copper commutator segments have been successfully tumbled for burrs in a three hours' run in a barrel of one cubic yard capacity, using one-third as much pine sawdust as work and loading the barrel about half full. Machine-steel punched hinge parts that have been annealed and formed have been tumbled for burr and annealing scale and brought to a bright finish in a six hours' run in a one-cubic-yard barrel, using one-fourth as much pure sand as work and limiting the load to three cubic feet. Green-clay and sand molded castings have been successfully cleaned in a four hours' run in a twocubic-yard barrel, nothing being placed in the barrel but the castings, and loading to one-third its capacity.

Partly finished or partly polished steel goods are often successfully tumbled in scrap leather to get a higher polish; this is simply an adaptation of the Aztecs' idea of shaking gold trinkets in a gourd with dry fish scales. The waste shavings and dust that come from the manufacture of fiber parts are also used for tumbling steel goods. In fact, all materials used to help the tumbling process should be, and generally are, wastes from other manufactures.

Silver plating has been done in the tumbling barrel by mixing a heavy mixture of chloride of silver, water and common salt with granulated cork. Small brass parts tumbled in this mixture take a very good plate in from one to three hours. The process is simply the rubbing of this mixture on the brass goods by the granulated cork.

The polishing or glaze mill used in the manufacture of rifle powders is nothing but a tumbling barrel. It is a polished, maple-lined barrel, into which is placed a quantity of powder as it comes from the corning mill; the falling motion of each grain over the others gives it the deep glazed luster.

Wooden handles, knobs, etc., are successfully cleaned and smoothed by tumbling with bits of torn sandpaper, a common oil barrel hooked up on a shaft being generally used. The writer has given a good manufacturing finish, in two hours' run in a sixty-gallon oil barrel, with twenty-four sheets, 10 by 12 inches, of torn sandpaper, medium grade, loading the barrel to one-third its capacity. This gives a good finish for dipping in asphaltum or white enamel broken up in gasoline.

Horn goods, clam- and oyster-shell novelties, bone products, etc., are cleaned and polished by tumbling. They are seldom mixed with any other materials.

All woods, most metals and many compositions may be successfully tumbled for cleaning and polishing. The type of tumbling barrel used has little to do with the process, as one barrel is as good as another, except perhaps in convenience The speed of the barrel is, of course, an important item; it must not be run so fast as to carry the work around in a solid mass, and it must be run slow enough for the pieces to fall and tumble over one another. To be effective, the barrel should make from thirty to sixty turns a minute. Personal judgment and experience must establish the rule in each individual case. In no case should work be tumbled if the same result can be reached more quickly and cheaply by other means, nor should work be dipped, pickled, scratch-brushed or polished that can be satisfactorily tumbled.

# USE OF FORMED SOLDER

In manufacturing articles having many soldered joints difficult to reach, it is good practice to furnish the solder punched or formed to fit the seam, as the time, labor and solder saved are important considerations; moreover, the formed solder is more likely to reach every part of the seam and insure a tight joint.

Fig. 1 shows a solder link stamped from a thin sheet of solder which is used by the Ford Motor Co. in making radia-

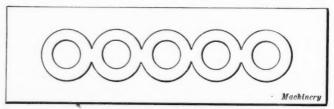


Fig. 1. Solder Link used in making Ford Radiators

tors of the tubular type. The radiator element is built up of vertical rows of tubes pressed through thin copper plates. The ends of the tubes must be soldered tightly into the water chambers. The solder links are dropped over the ends of the rows of tubes and are melted with a blow-torch, as shown in Fig. 2. The solder, being applied all around the tube in link form, runs down the tube to the tube sheet and makes a practically perfect soldered joint on five tubes simultaneously. It is obvious that much time is saved by the use of formed solder links in confined spaces like this; in fact, it would be practically impossible for the workman to apply solder to all the tubes in a reasonable length of time unless it were furnished him in the stamped shape.



Fig. 2. Soldering Vertical Tubes in Water Chambers of Ford Radiators

# SPECIAL-PURPOSE TURRET LATHE WITH BALL-BEARING SPINDLE

BY T. S. MACEWAN

A heavy-duty, 32-inch turret lathe, recently designed by Charles H. Hollup and built by the Vilter Mfg. Co., Milwaukee, Wis., is shown in Fig. 1. The details of the headstock design of bearing combination. The machining of parts is simplified and greater ease in erection is secured through the use of ball bearings. Two ball bearings are also located in the threestep cone pulley, which is bored to correspond with the outside diameter of a standard bearing. When running loose, the gear load for the driven gear mounted on the lathe spindle is taken by one of these bearings.

The operating thrust load, of which there is a small component in turning and a heavy one in boring work, is taken on the set of balls of the double thrust bearing mounted at the rear of the spindle. Where the turning is done toward the direction of the tailstock, the thrust is in the opposite direction to the forward thrust, and the load is properly taken care of by the reversal of the double thrust bearing and the assumption of the load by the other set of balls. When the back-gears are to be brought into play the clutch is thrown in so that gear A drives the corresponding back-gear. With direct drive the clutch is thrown in the opposite di-

drives directly through the spindle to the work. The crossfeed screw of the carriage is provided with a thrust ball bearing, by means of which undue wear and the resulting lost

rection, so that the cone pulley

motion are eliminated.

Methods employed in manufacturing are sometimes directly opposite in principle to those that would naturally be followed when making the parts by hand one at a time. These manufacturing methods have been adopted because they overcome difficulties of handling and promote rapid production. For instance, in making motor car top curtains, the Ford Motor Co. follows the practice of sewing the celluloid windows to the fabric before cutting the openings. The fabric holds its shape during the sewing operation and there are no holes to catch on the machine and interrupt the operation. When the sewing is done, the openings are cut with a sharp forked knife which slides over the celluloid and cleanly cuts or rips the fabric close to the seam. This method not only saves the sewing operator's time, but also permits the openings to be cut much more evenly and expeditiously than would be possible by following the reverse and natural process.

. . . In order that German letters patent issued to American citizens shall not lapse because of the non-payment of taxes, or other necessary fees, a recent presidential proclamation permits such payments to be made throughout the duration of

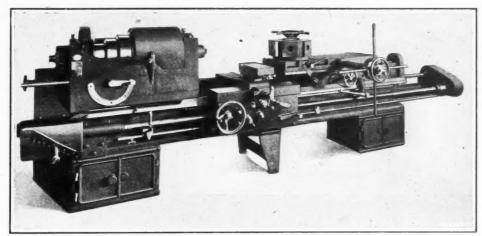


Fig. 1. Heavy-duty 32-inch Turret Lathe

were given the most careful consideration, with the result that ball bearings were used on the spindle and a cone clutch was provided for quickly throwing the back-gears in and out.

A lathe, to be a profitable investment, must be capable of producing properly machined pieces day in and day out with the minimum of attention. This means that the working spindle must be held rigidly and must be free from chatter under operating conditions, and it must be mounted to withstand the tool pressure and thrust imposed. To produce good work, a spindle bearing must be free from shake and hold the spindle tight. A great many people claim that it is impossible to keep a bearing in this condition for any length of time without adjustment, and that wear begins at the time of starting, soon resulting in looseness. While a countershaft bearing. or a bearing for any kind of shaft that does not carry a cutter or work that is being cut, can be slightly loose without serious effect, in a spindle where smooth work is expected, absolute tightness must be preserved. This rigidity of the spindle not only eliminates chatter where heavy cuts are taken with singlepoint tools, but permits a light finishing cut to be taken with a wide shaving tool. Further, any shake during the cut due to the varying cutting depth of the tool is prevented.

In Fig. 2 it will be seen that the front bearing surfaces of this turret lathe comprise two S K F double-row, radial, selfaligning ball bearings mounted in a through bored housing, with end caps bolted to the frame to make an enclosed type Address: S K F Ball Bearing Co., Hartford, Conn.

Fig. 2. Spindle of Special-purpose Turret Lathe

# INDUSTRIAL OXYGEN EXPLOSIONS

CAUSES OF RUPTURE OF STORAGE CYLINDERS USED IN WELDING AND CUTTING OPERATIONS

BY EDWARD K. HAMMONDI

URING the period in which oxy-acetylene welding and cutting were in process of development, the explosion of an acetylene generator was not an unusual occurrence, accidents of this kind being due to generators of unsuitable design and improper methods of handling the gas. An increase of knowledge on this subject was the means of practically eliminating these sources of danger. Recently there have been several serious explosions of oxygen used in connection with acetylene in the welding and cutting of metals. It has become a matter of general knowledge that acetylene must be handled with care, but many users of oxy-acetylene torches do not realize that there are dangers connected with the use of oxygen of unknown purity, and, as a result, serious accidents are likely to occur. This is due in part to the fact that some manufacturers of electrolytic oxygen generators

have unwisely advertised the statement that their machines are fool-proof and can be safely operated by laborers of average intelligence. This may be the case so long as everything goes properly, but it requires a particularly intelligent attendant to detect an abnormal condition of operation before a lot of dangerous gas has been generated and sent out to the welding shop. An inquiry made by MA-CHINERY to ascertain the different sources of danger connected with the use of commercial oxygen or the operation of electrolytic oxygen generators, and the precautions that should be taken to avoid accidents from these causes, has revealed the information outlined in the following article.

In starting upon this discussion, attention is called to the fact that commercial oxygen may be produced by either of two processes. The first is generally known as the liquid air method, which consists of liquefying air by the application of pressure

and reducing the temperature, and then separating the oxygen from the nitrogen by taking advantage of the difference in boiling points of the two liquids. Oxygen produced in this way cannot explode through the presence of impurities, because these impurities are nitrogen and other gases which are chemically inert. The second method of obtaining oxygen is by the electrolysis of water, and here there is a possibility of accidents due to hydrogen being present in sufficient quantity to make a mixture that is highly explosive. This danger is theoretical rather than practical, so long as the proper precautions are taken in the operation of electrolytic generating plants; but where there is lack of care in attending to generators or where the generators are of unsuitable design, this danger may prove serious.

Theoretically, the explosion of a mixture of hydrogen and oxygen results in the combination of two volumes of hydrogen gas with one volume of oxygen; but while this is the mixture required for a complete explosion, experience has shown that there is a wide range of mixtures that constitute what may be called a danger zone, *i. e.*, mixtures that may explode

with violence under certain conditions. This question was considered of sufficient importance to warrant an investigation being undertaken at the Pittsburg Laboratory of the Bureau of Mines, where it was found that mixtures ranging from 9 per cent of hydrogen and 91 per cent of oxygen up to 92 per cent of hydrogen and 8 per cent of oxygen were likely to give trouble. This is more liberal than limits established by the Davis-Bournonville Co., Jersey City, N. J., a well-known manufacturer of welding and cutting equipments, including oxygen generators. In this company's laboratories the danger zone was found to cover a wider range, extending from 6 per cent of hydrogen and 94 per cent of oxygen down to 97 per cent of hydrogen and 3 per cent of oxygen. The idea of this danger zone will be best understood by reference to the tabulated figures, the brackets representing the range of explosive mix-

tures. Here it will be evident that mixtures of hydrogen and oxygen represented by the high and low limits, and all mixtures coming between these limits, may be made to explode under suitable conditions.

Oxygen Hydroger 100 98 2 96 4 6 91 8 92 94 97 2 98 0 100

Note—Brackets inside the columns represent range of explosive mixtures, as determined by Bureau of Mines; and brackets outside the columns cover range of mixtures found to be explosive by the Davis-Bournonville Co.

Investigations conducted with the view of determining the cause of oxygen explosions that have resulted disastrously have led to certain important modifications in the design of electrolytic generators and auxiliary equipments to prevent the recurrence of such accidents. In the operation of an electrolytic cell, decomposition of water results

in liberation of hydrogen at the negative electrode of the cell, while oxygen passes off from the positive electrode. The cells are so arranged that gas collected from each of these electrodes is passed into containers provided for the hydrogen and oxygen, respectively. Should it happen that the polarity of the generator is reversed, it would result in a corresponding reversal of the polarity of the cells, so that oxygen would be collected in the container provided for hydrogen, and vice versa.

As a matter of fact, this has been the cause of some serious accidents, and a study of the subject led to the provision of safety devices which make it impossible for trouble of this kind to occur. The safeguard consists of an automatic switch, which makes connection with the electrolytic cells only after the generator has reached normal speed and is developing its normal electromotive force. The necessity for this provision arises from the fact that at any time when the operation of a generator is stopped there is a tendency, while the armature is still turning over by inertia, for a counter-electromotive force to be built up in the cells. This may reach sufficient proportions to overcome the magnetic force of the field windings

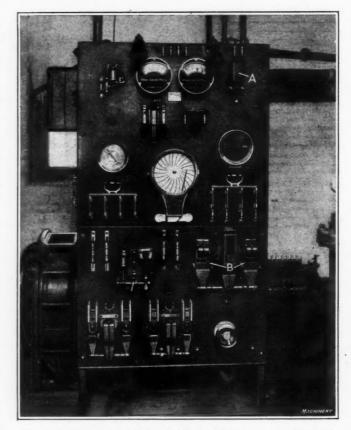


Fig. 1. Switchboard equipped with Automatic Switch to prevent Reversal of Polarity of Generator

<sup>1</sup> Associate Editor of MACHINERY.

of the generator, so that when it is again started the generator will operate with its polarity the reverse of normal and supply energy of a correspondingly reversed polarity to the electrolyzers.

Should such a condition exist, it is obvious that hydrogen would be delivered to the oxygen gas-holder and oxygen to the hydrogen gas-holder, thus forming a dangerous mixture with the gas already in these holders. But with the automatic switch referred to, there is no danger of this trouble, because the generator will have assumed a normal speed and developed its normal electromotive force before the switch can be closed to allow current to pass through the cells. This method of safeguarding the connecting of the electrolyzers to the power supply makes it impossible for a counter-electromotive force in the cells to overcome residual magnetism in the windings of the generator. In the switchboard illustrated in Fig. 1, the switch shown at A is for making connection between the generator and cells, and is automatically closed by magnetic coils B when the generator speed and voltage have reached the normal figure. When the electric generator is stopped, the circuit through the electrolytic cells is automatically broken.

To further assure against trouble from a counter-electromotive force in the electrolytic cells due to causes outside the plant, such as the reversal of phase in the motor supply circuit, transposition of connections at the electrolytic cells, etc., use is made of a polarized relay connected to a special shunt. This provides for opening a single-pole relay in the control circuit, and the only way in which this circuit may be re-established is to close the relay by hand, provided the polarity has been restored to normal. If a plant is equipped with this system of control, reversal of polarity is indicated by failure of the electrolytic cells to operate. It is important to note that the generator used in connection with electrolytic cells should be of the shunt-wound type, because with compound-wound generators there is greater danger of reversal due to the counter-electromotive force in the cells passing through the series turns.

In addition to danger of the generation of explosive mixtures of oxygen and hydrogen through a reversal of polarity of the generator, trouble may also be experienced through improper connection of the terminals of electrolytic cells. As a

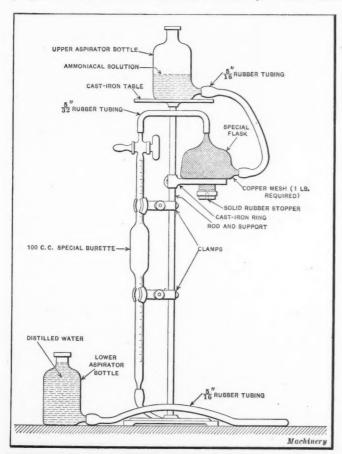


Fig. 2. Apparatus for determining Purity of Oxygen by Absorption with Metallic Copper

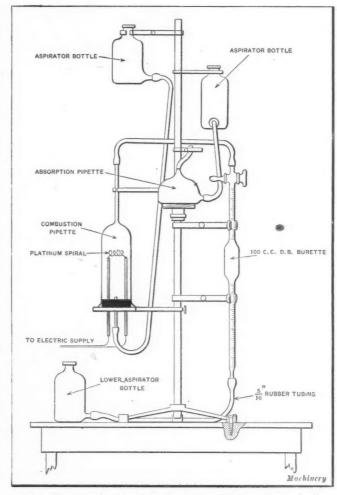


Fig. 3. Apparatus for determining Percentage of Hydrogen by Combustion Method, and Percentage of Oxygen by Absorption with Metallic Copper or Sticks of Phosphorus

matter of fact, this was the cause of a serious explosion which occurred in St. Louis some time ago. With the view of preventing accidents of this kind, the Davis-Bournonville Co. and other manufacturers of electrolytic cells have designed their electrical connections in such a way that it is impossible to connect them with the wrong polarity.

There is only one way to be sure that the purity of oxygen generated in electrolytic cells is up to the required standard, and that is by making chemical analyses at intervals of at least two hours. As a matter of fact, these analyses are simple to make and do not call for extensive technical knowledge of chemistry. Several methods are employed, the most common one being that of measuring one hundred cubic centimeters of gas into a burette and then running this gas over into another burette in which the hydrogen is burnt out by a platinum coil, which is raised to a red heat. The gas is then returned to the first burette and again measured, the contraction in volume expressed in cubic centimeters representing the percentage of hydrogen in the gas.

Other methods of determining the purity of oxygen consist of running the measured volume of gas into a second burette containing either pure metallic copper or sticks of phosphorus. Both these materials have the power to absorb oxygen from the mixture of oxygen and hydrogen, and after this absorption has been completed, the hydrogen is returned to the burette and measured. The contraction in this case represents the percentage of oxygen present. Standard apparatus can be purchased for making all these tests. In practice, it is customary to get a purity of 99.7 to 99.8 per cent for hydrogen and a purity of about 99.5 per cent for oxygen. If the purity of hydrogen runs below 99.5 per cent or the purity of oxygen is found to be below 99 per cent, it is considered that the generator is operating unsatisfactorily, and the man in charge of the station immediately proceeds to look for the cause. Where this precaution is taken, there is little danger of trouble from the use of electrolytic oxygen, because a high factor of safety is provided.

Experience has shown that in the presence of oil there is danger of an oxygen cylinder "exploding" from what may properly be termed "spontaneous combustion" of the cylinder, although the gas is pure oxygen without any trace of hydrogen. This is due to the fact that the action of oxygen under high pressure—usually about 1800 pounds per square inch—results in oxidation of the oil, thus raising the temperature sufficiently to start the oxygen acting upon the iron cylinder, which is burnt away and allows the high-pressure gas to expand rapidly. This could not properly be called an explosion, because an explosion is usually understood to mean rapid combustion accompanied by rapid expansion. However, the condition that exists when the high-pressure oxygen is allowed to expand suddenly is similar to a true explosion, and the results have been serious in some cases. In this connection it is of interest to note that oxygen produced by the liquid air process and oxygen gerated in electrolytic cells are equally likely to give trouble. Recently, the statement was made that this source of trouble could be eliminated by substituting graphite as a lubricant in place of oil, but experiments conducted by the International Oxygen Co., the Davis-Bournonville Co. and others show that graphite is just as dangerous as oil.

Still another hypothesis has been advanced as to a source of danger from the explosion of hydrogen. Reference has already been made to the fact that experimental data show that there must be at least 6 per cent of hydrogen in the oxygen to make the mixture explosive. This refers to 6 per cent of hydrogen uniformly mixed through the entire volume of oxygen. Readers of Machinery are doubtless familiar with the so-called kinetic theory of gases, otherwise known as the theory of uniform diffusion. According to this theory, the constituents of mixed gases are kept uniformly distributed, due to the kinetic action of molecules of the gas. For instance, a mixture of hydrogen and oxygen containing 3 per cent of hydrogen would have the hydrogen uniformly mixed through the 97 per cent of oxygen, and as it has already been mentioned that a minimum of 6 per cent of hydrogen is required to make the mixture explosive, it will be apparent that there would be no danger with this gas under normal

In practice, accidents have occurred through the explosion of oxygen cylinders in which the head has been blown out of the cylinder, and investigations conducted to determine the cause of these accidents have led to the belief that under the high pressure which exists in an oxygen cylinder-amounting to approximately 1800 pounds per square inch—the theory of uniform diffusion is not effective; it is assumed that under these conditions of pressure the gases settle out into strata, according to their specific gravities, the result being that the hydrogen rises to the top of the cylinder. This action may not be complete, but if there were a tendency for such settling out to occur, it could easily result in producing an explosive mixture of hydrogen and oxygen at the top of the cylinder, even though there were not sufficient hydrogen to make the entire mixture explosive. If such conditions can be developed, it is apparent that flashback or other cause of ignition would immediately ignite the mixture and result in the explosion of the gas in the cylinder. The theory is interesting, although it has not been definitely established by a carefully conducted scientific experiment. An accident of the same kind might also be produced through the action of oxygen on the oil used to lubricate the valve.

In handling oxygen cylinders, it should always be borne in mind that the gas is under high pressure, and as a result it requires intelligent care to prevent accidents. Cylinders should not be dropped or handled roughly, and they should not be placed so that they can be easily overturned either by collision with some other object or by the reaction due to the violent escape of their contents through the safety outlet with which each cylinder is provided. The valve regulating devices and other attachments should not be lubricated with oil for reasons to which reference has already been made. Discharge valves should be opened slowly and special care should be taken to avoid twisting or straining the valves by the use of hammers or improper wrenches.

Much valuable information has been gathered by members of the Committee on Production of Electrolytic Oxygen and Hydrogen which has been appointed by the Compressed Gas Manufacturers' Association, Inc., 120 Broadway, New York City, concerning possible dangers connected with the use of oxygen in the operation of cutting and welding torches. Distribution of information concerning the proper way to use oxygen and the safeguards that should be taken to avoid accidents will doubtless be the means of overcoming much trouble from this source.

# TAPER MACHINE REAMERS

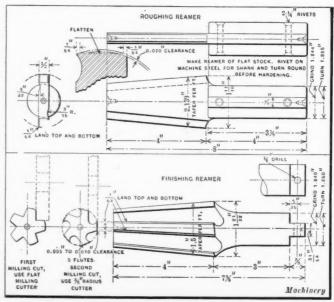
The taper machine reamers shown herewith have been successfully used by the Brown-Lipe-Chapin Co., Syracuse, N. Y., by whom they were developed. The roughing reamer has two cutting edges, and the main body is made from a flat bar of steel, approximately 1/2 inch thick. After being cut to length, it is centered and turned to the desired contour. Two flat pieces of machine steel are riveted to the body to form the shank, and turned, leaving a sufficient amount for grinding. The chief difference between this taper roughing reamer and other types is the way in which it is ground and backed off. Just in front of the cutting edge a liberal radius is milled to a depth of 3/32 inch. This not only gives adequate clearance, but furnishes a well shaped surface for chips to slide upon. The taper is first ground accurately until the large end is of the correct diameter. After this, the curvature of the two flutes is flattened, leaving only 1/64 inch of the curved surface produced by grinding. Next the reamer is oscillated on the centers by hand and a clearance is ground radially on the edge back of the flute. The clearance in this case is 0.020 inch, as shown in the upper view of the illustration.

#### Finishing Reamer

The finishing reamer is five-fluted and is milled from a solid forging. Two cutters are used in milling the reamer. The first is a plain right-angle cutter, which is followed by one of % inch radius. The latter produces the under-cut, which makes these reamers so effective. After the reamer is ground, the flutes are flattened the same as in the roughing reamer. The radial clearance, however, on the back of each tooth is less than in the former case, varying from 0.005 to 0.010 inch. This reamer is fitted at the driving end so that it may float freely when in use.

An advantage that these reamers have over many others is the fact that they actually cut the metal rather than scrape it. Another advantage is the fact that it is impossible to crowd the reamers into the work enough to damage them, since the clearance is a known factor. The economy of the construction of the roughing reamer is worthy of note because of the high price of steel.

V. B.



Details of Roughing and Finishing Reamer

# PUMPS FOR OPERATING HYDRAULIC PRESSES

FORMULAS FOR DETERMINING SIZES OF ONE-, TWO- AND THREE-PLUNGER PUMPS

BY A LEWIS JENKINS

THE pressure required on the ram of a hydraulic baling press increases as the density of the bale increases. The pressure at the beginning of the stroke depends upon the density with which the material is packed in the baling box, and at the end, upon the amount that the bale is compressed. A similar variation takes place throughout the run of an unbalanced hydraulic lift, the required pressure increasing directly as the run of the ram.

Presses for baling cotton, hay and similar materials are usually supplied with water or some other liquid by a belt- or motor-driven pump. The speed and width of the belt are constant, and this means that there is a constant amount of power available, and the plungers of the pumps run at a constant speed. When the pump is provided with only one plunger, its diameter or area is determined by the final pressure required, its velocity and the available horsepower obtained from:

$$\text{H.P.} = \frac{pvz}{33,000 \times 12}$$

where H.P. = available horsepower;

p = maximum or final pressure in pounds per square inch;

v =velocity of plunger in inches per minute;

z = area of ram in square inches.

At the beginning of the stroke of the press ram, a very low pressure is sufficient to move it. Hence, it will be seen from the preceding equation that the power required to deliver the water at the beginning of the ram stroke is very small compared with the power required in producing the final pressure; and the time for one operation is much longer than it would be if the maximum available horsepower could be utilized throughout the entire stroke. This condition could be realized for all positions of the stroke of the baling press if it were possible to make pv a constant, where p is the pressure at any position of the stroke. This has been done to some extent by using a mechanism similar to the Stephenson link, which varies the length of stroke of the pump, making it shorter as the pressure increases, and thereby maintaining a constant required power. Other methods have been tried, such as placing two pump plungers in the same plunger box and adjusting their relative positions by shifting their eccentrics in such a way as to vary the effective displacement. The design of a pump which maintains a constant value of pv is more or less complicated, and such pumps are expensive to construct. The result is obtained by automatically varying the length of stroke or by changing the relative positions of the two plungers working in the same plunger box.

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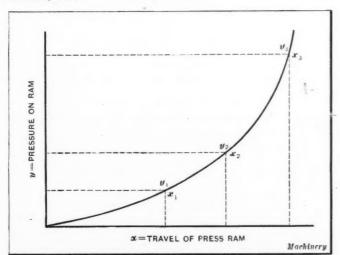


Fig. 1. Diagram illustrating Relation between Pressure of Pump Plungers and Travel of Ram of Press

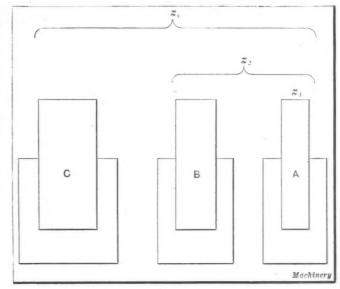


Fig. 2. Arrangement of Multiple-plunger Pump

Another method of maintaining a constant horsepower throughout the stroke of the press is effected by making pz constant; but this cannot be thoroughly accomplished in a commercial machine. An approximation of this method, however, has proved to be the most satisfactory solution. The time required for one operation may be decreased by using more than one plunger and automatically cutting out one at a time as the increasing pressure raises the power required to drive the pump with the active plungers in operation. Thus, a pump provided with three plungers having areas A, B and C, respectively, may have all three plungers in operation for a portion of the stroke of the press ram, and when the pressure times the area of all three of the plungers becomes sufficient to require all the available power, plunger C "knocks out" and A and B continue to operate until the power again becomes equal to the maximum and B "knocks out," allowing the plunger A to finish the operation, which requires the maximum pressure.

All of the plungers A, B and C may be made equal in area, and the pressure at which they should knock out may be determined; but for ordinary baling operations this is not the most economical proportion of plunger areas from the standpoint of available power and the time required to compress a bale. For baling cotton and similar materials the relation between the pressure per square inch on the ram and the travel of the ram in inches may be expressed by the equation:

$$y = kx^3$$

where y = pressure per square inch of the water acting upon the ram of the press after it has traveled a distance x from the beginning of the stroke, and k is a constant depending upon the area of the platen and nature of the material pressed.

Proportions of Plungers for Three-plunger Pump for Baling Cotton

It is desirable to have the plungers of such proportions that they will raise the ram of the press in a minimum time when a given power is available. The relation between pressure y and travel x is shown in Fig. 1, and a diagram showing the arrangement of the plungers of the pump is shown in Fig. 2.

Let  $z_1 =$  area in square inches of the three plungers A, B and C;

 $z_2$  = area in square inches of the two plungers A and B;

 $z_3$  = area in square inches of the plunger A;

v = velocity of the plungers in inches per minute;

 $y_1 =$ pressure in pounds per square inch at which O knocks out;

 $y_2 =$  pressure in pounds per square inch at which B-knocks out;

- $y_3$  = pressure in pounds per square inch at which A knocks out, or the final pressure required;
- $x_1 =$ distance in inches ram of press has traveled when C knocks out:
- $x_2$  = distance in inches ram of press has traveled when B knocks out;
- $x_3 =$ distance in inches ram of press has traveled when A knocks out, or total travel of press ram;
- M =area of press ram in square inches;
- $t_1$  = time in minutes the plunger C operates, or time the area  $z_i$  is in action during working stroke of the press ram;
- $t_2$  = time in minutes the area  $z_2$  is in action during the working stroke of the press ram;
- $t_3$  = time in minutes the area  $z_3$  is in action, or the period during which only the ram A is operating during the working stroke of the press ram;
- T = total time in minutes required for the working stroke of the press ram =  $t_1 + t_2 + t_3$ .

The volume displaced by the press ram for any position, a distance x from the beginning of the stroke, is Mx. The volume displaced by area  $z_1$  of the pump plungers for a travel  $x_1$ of the press ram is  $Mx_1$ . The pump plunger area  $z_2$  is in operation while the press ram travels from  $x_1$  to  $x_2$ ; hence, the volume displaced by  $z_1$  is equal to  $M(x_2-x_1)$ . Similarly, the volume supplied by  $z_3$  is  $M(x_3-x_2)$ .

Substituting the values of x given by the following equation:

$$y = kx^3$$
 or  $x = \sqrt[3]{\frac{y}{x}}$ 

we have:

$$Mx_1 = M \sqrt[3]{\frac{\overline{y_1}}{k}} = \text{volume supplied by area } z_1;$$

$$M(x_z-x_z)=M\left(\sqrt[3]{rac{y_z}{k}}-\sqrt[3]{rac{y_z}{k}}
ight)= ext{volume supplied by area }z_z;$$

$$M(x_3-x_2)=M\left(\sqrt[3]{\frac{\overline{y_3}}{k}}-\sqrt[3]{\frac{\overline{y_2}}{k}}\right)= ext{volume supplied by area }z_3.$$

The time t in minutes required to raise the press ram a distance x with one plunger having an area z and velocity v is:

$$t = rac{ ext{volume displaced by press ram}}{ ext{rate of flow of water from pump}} = rac{Mx}{zv}$$

By substituting the value of x given by the equation

$$x = \sqrt[3]{\frac{y}{k}}$$

we get:

$$t = \frac{M}{zv} \sqrt[3]{\frac{\overline{y}}{k}} = \frac{m}{z} \sqrt[3]{\overline{y}}$$

where  $m = \frac{M}{v \sqrt[4]{k}} = \text{constant}$ 

Similarly,

$$t_1 = \frac{m}{z_1} \sqrt[3]{y_1} = \text{time area } z_1 \text{ is in action}$$

$$t_2 = \frac{m}{z_2} (\sqrt[3]{y_2} - \sqrt[3]{y_1}) = \text{time area } z_2 \text{ is in action}$$

$$t_3 = \frac{m}{z_2} (\sqrt[3]{y_3} - \sqrt[3]{y_2}) = \text{time area } z_2 \text{ is in action}$$

Hence, the total time 
$$T$$
 required to raise the press ram is: 
$$T = t_1 + t_2 + t_3 = \frac{m}{z_1} \sqrt[3]{y_1} + \frac{m}{z_2} (\sqrt[3]{y_2} - \sqrt[3]{y_1}) + \frac{m}{z_3} (\sqrt[3]{y_3} - \sqrt[3]{y_2}) \text{ minutes}$$

In order to have the power equal at pressures  $y_1$ ,  $y_2$  and  $y_3$ :  $y_1 z_1 = y_2 z_2 = y_3 z_3$ 

By multiplying the numerators and denominators of respective terms on the right of the equation for T by  $y_1$ ,  $y_2$  and  $y_3$ 

$$T = \frac{my_1}{z_1y_1} \, \sqrt[q]{y_1} + \frac{my_2}{z_2y_2} \left(\sqrt[q]{y_2} - \sqrt[q]{y_1}\right) + \frac{my_3}{z_2y_3} \left(\sqrt[q]{y_3} - \sqrt[q]{y_2}\right)$$

Since the denominators of these fractions are equal:

$$\frac{T}{m} = \frac{y_1 \sqrt[4]{y_1} + y_2 \left(\sqrt[4]{y_2} - \sqrt[4]{y_1}\right) + y_3 \left(\sqrt[4]{y_3} - \sqrt[4]{y_2}\right)}{y_3 z_2}$$
But
$$y_1 = \frac{y_2 z_3}{z_1} = b y_3$$
and
$$y_2 = \frac{y_3 z_3}{z_2} = a y_3$$
where
$$b = \frac{z_3}{z_1} = \frac{A}{A + B + C}$$
and
$$a = \frac{z_3}{z_2} = \frac{A}{A + B}$$

Substituting the values of  $y_1$  and  $y_2$  in the above equation

$$T = \frac{m}{y_3 z_3} \left( y_3^{\frac{1}{3}} b^{\frac{5}{3}} + y_3^{\frac{5}{3}} a^{\frac{1}{3}} - ab^{\frac{5}{3}} y_3^{\frac{5}{3}} + y_3^{\frac{5}{3}} - y_3^{\frac{5}{3}} a^{\frac{1}{3}} \right)$$

Simplifying this equation, we get:

$$T = \frac{my_3^{\frac{1}{3}}}{z_3} \left( b^{\frac{1}{3}} + a^{\frac{1}{3}} - ab^{\frac{1}{3}} + 1 - a^{\frac{1}{3}} \right)$$

Simplifying this equation,  $T = \frac{my_3^{\frac{1}{3}}}{z_3} \left( b^{\frac{1}{3}} + a^{\frac{1}{3}} - ab^{\frac{1}{3}} + 1 - a^{\frac{1}{3}} \right)$ The relation of a to b that will give a minimum value of T may be found by making  $\frac{dT}{da} = 0$  and  $\frac{dT}{db} = 0$ , and solving

the two resulting equations as follows:

Since 
$$\frac{dT}{da} = \frac{my_3^{\frac{1}{3}}}{z_3} \left( \frac{4}{3}a^{\frac{1}{3}} - b^{\frac{1}{3}} - \frac{1}{3a^{\frac{2}{3}}} \right) = 0$$

$$\frac{my_3^{\frac{1}{3}}}{z_3} \text{ is not } = 0$$

$$\frac{4}{3}a^{\frac{1}{3}} - b^{\frac{1}{3}} - \frac{1}{3a^{\frac{2}{3}}} = 0$$

$$\frac{dT}{db} = \frac{my_3^{\frac{1}{3}}}{z_3} \left( \frac{4}{3}b^{\frac{1}{3}} - \frac{a}{3b^{\frac{2}{3}}} \right) = 0$$
Hence 
$$\frac{4}{3}b^{\frac{1}{3}} - \frac{a}{3b^{\frac{2}{3}}} = 0$$

By substituting 
$$a = 4b$$
 in the equation:  

$$\frac{4}{3}a^{\frac{1}{3}} - b^{\frac{1}{3}} - \frac{1}{3a^{\frac{3}{3}}} = 0$$

$$a = 0.474$$
 and  $b = 0.1185$ 

From the equation:

$$a = \frac{A}{A + B}$$
$$B = A\left(\frac{1 - a}{a}\right)$$

From the equation:

$$b = \frac{A}{A + B + C}$$

$$C = \frac{A}{b} - A - B = \frac{A}{b} - A - A\left(\frac{1 - a}{a}\right)$$

$$C = A\left(\frac{1}{b} - \frac{1}{a}\right)$$

By substituting a=0.474 and b=0.1185 in the preceding equation:

$$B = 1.11A$$
 and  $C = 6.33A$ 

Since the area varies as the square of the diameter, diameter of ram B is 1.05  $\times$  diameter of A; and the diameter of C is  $2.52 \times \text{diameter } A.$  Hence, for baling a material which obeys the law  $y = kx^{s}$ , the diameters of plungers A and B may be made equal and the diameter of C should be about 2.5 times that of A.

#### Time Required to Form Bale

The time required to run a press ram through its entire stroke when  $y = kx^3$  and a three-plunger pump is used, having the diameters of the plungers in the ratio of 1, 1.05 and 2.52, may be found by substituting a = 0.474 and b = 0.1185in the equation for total time T, which gives:

$$T = rac{my_3rac{3}{2}}{z_3} \left( 0.1185rac{4}{3} + 0.474rac{4}{3} - 0.474 imes 0.1185rac{1}{3} + 1 - 0.474rac{1}{3} 
ight) \ = rac{0.42my_3rac{3}{3}}{z_3} = rac{0.42mp
brack }{A} = rac{0.42M}{vA} \sqrt[3]{rac{p}{k}} = rac{0.42Mx}{vA}$$

General Case for Three-plunger Pump

The diameters of plungers for pumps designed to operate any baling machine, regardless of the material to be baled, should be based on the assumption that  $y=kx^3$ . This value may be considered an average for the materials commonly operated upon; but if it is definitely known that a pump is to supply water to a press for compressing any given material, such as tankage, apples, grapes, olives, hay, tin cans, etc., the exact relation between pressure and travel may be easily determined by experiment. The pressure per square inch of the liquid in the cylinder is read from a gage for a number of positions of the ram, and these data plotted on log-log paper or the values of n and k are determined by substituting values of x and y in the equation  $y=kx^n$ , which may be used for practically any material.

By using  $y = kx^n$  instead of  $y = kx^2$ , it is found for a three-plunger pump that:

and

$$b = \frac{a = (n+1)b}{1}$$

$$(n+1)^2 - n(n+1)\frac{n-1}{n}$$

From these equations, values of a and b and the areas and diameters for given values of n are shown in Table 1.

TABLE 1. RATIOS OF PLUNGER DIAMETERS FOR THREE-PLUNGER PUMP

n	b	8	Area of B	Area of C	Diam. B	Diam. C
			Area of A	Area of A	Diam. A	Diam. A
1	0.333	2b = 0.666	0.50	1.50	0.70	1.22
2	0.179	3b = 0.549	0.84	3.69	0.92	1.92
3	0.118	4b = 0.474	1.11	6.33	1.05	2.52
4	0.085	5b = 0.429	1.33	9.33	1.15	3.05
5	0.067	6b = 0.406	1.46	12.29	1.21	3.51

General Case for Two-Plunger Pump

In the case of a pump having two plungers with areas A and B, it may be shown that:

$$a = \frac{A}{A+B} = \frac{1}{n+1}$$

from which

$$B = An$$

The relative values of A and B and their corresponding diameters are shown in Table 2 for different values of n.

TABLE 2. RATIOS OF PLUNGER DIAMETERS FOR TWO-PLUNGER PUMP

n	Area of B Area of A	Diam. B Diam. A
1	1	1.00
2	2	1.41
3	3	1.73
4	4	2.00
5	5	2.24
		Machinery

#### Determination of "Knock-out" Pressures

The method of finding the "knock-out" pressure is illustrated by the following example: A three-plunger pump having a piston velocity of 50 feet per minute, diameters of plungers 1.5 inch, 1.5625 inch, and 3.75 inches, gives a maximum pressure of 1500 pounds per square inch. The efficiency of the pump is 70 per cent.

The maximum horsepower required is:

H.P. = 
$$\frac{1500 \times 50 \times 1.76}{33,000 \times 0.7} = 5.72$$

This is found by using the maximum pressure and the area of the plunger giving that pressure. The maximum horse-power is reached when the product of the pressure into the area is equal to:

$$1500 \times 1.76 = 2640$$

The area of all three plungers is 1.76 + 1.91 + 11.04 = 14.71

square inches, which gives  $\frac{2640}{14.71} = 180$  pounds per square

inch for the first "knock-out" pressure. The sum of the areas of the second and third rams is  $1.76\,+\,11.04\,=\,12.80$  square

inches, and the second "knock-out" pressure is  $\frac{2040}{12.80} = 206$  pounds per square inch.

These pressures are lower than those generally found on pumps for baling presses; but in view of the fact that fibrous materials, such as cotton, approximately compress according

to the equation  $y = kx^3$ , and the ram is at  $\sqrt[3]{\frac{180}{1500}} = 0.49$  and

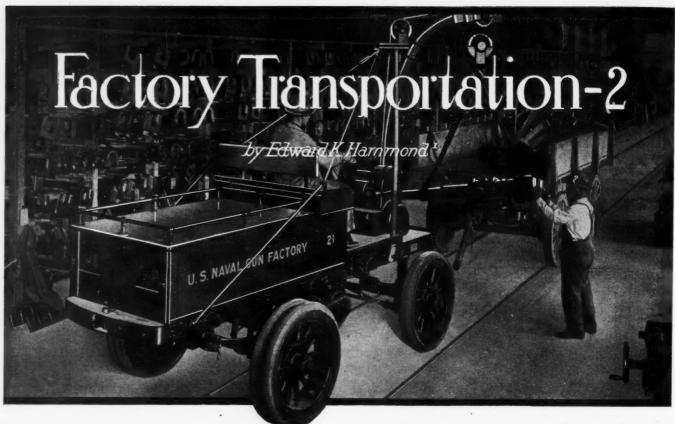
 $\sqrt{\frac{-}{1500}}$  = 0.52 of its total run when these pressures are attained, the advantage of the low "knock-out" pressures is readily appreciated.

# IGNORANCE IN STARTING A MANUFACTUR-ING BUSINESS

A large percentage of business failures are due to the lack of knowledge of the business entered and the equipment and organization required. Men engage in retail selling with little or no business experience. They buy goods unwisely, acquire ill-balanced stocks, and finally fail with a lot of bad accounts which can never be collected. The manufacturing business is no exception to the rule, and many heedless, ill-advised ventures are often met with in manufacturing. It is stated by a machine tool salesman of broad experience in selling new machinery and dealing in second-hand tools that a large percentage of the men who start small manufacturing enterprises know practically nothing of manufacturing principles and are almost totally ignorant of the equipment required to produce their products efficiently. They buy lathes, planers, drilling machines, milling machines, and other standard machines with little discrimination and set them up in orderly rows in their new quarters. Power is turned on and the wheels start in motion, but machinery running does not necessarily result in turning out marketable carbureters, gas engines, egg beaters or anything else. The important elements of directive skill and sales organization are too often lacking. After struggling along miserably for a few months, a lot of machine tools, somewhat the worse for wear, are offered to second-hand dealers.

# \* \* \* ENGINEERING COUNCIL

The first meeting of the Engineering Council was held in the Engineers' Bldg., New York City, June 27. This body is a department of the United Engineering Society and has recently come into being as a medium of cooperation between the four national engineering societies. The function of the council is to speak authoritatively for all member societies on all public questions of a common interest or concern to engineers. It is composed of twenty-four members, five being appointed from each of the four founder societies and four by the United Engineering Society; the founder societies are the American Society of Civil Engineers, the American Institute of Mining Engineers, the American Society of Mechanical Engineers, and the American Institute of Electrical Engineers. At the organization meeting, Dr. I. N. Hollis was elected president of the council; H. W. Buck and George F. Swain, vicepresidents; and Calvert Townley, secretary. Ways and means were discussed by which the societies through the council might be of use to the national government. A resolution was adopted instructing the executive committee to cooperate with the government in procuring the services of engineers, and a committee was appointed to consider the best means of utilizing the inventive ability of members of the founder societies.



OTOR-DRIVEN trucks, provided with their own power plant in the form of an electric storage battery and motor, are now being used in many industrial plants in the United States. Trucks of this type naturally cost considerably more than any of the trucks which are driven by manual labor, and the only justification for investing in equipment where the first cost is higher is if conditions of operation are such that a greater amount of service might be obtained from motor-driven trucks. It is difficult to make statements to cover general conditions, but in the present case it may be stated that the particular field of usefulness of motordriven trucks is where the length of haul is sufficiently great so that a material saving of time and labor may be obtained through the increased speed. Running on hard level surfaces, the speed of these trucks will be about seven miles an hour, and the average truck has a capacity for running about twentyfive miles on a single battery charge.

The driver stands erect on a platform at the end of the truck, with his hands on the controller and steering levers, respectively, and one foot on the brake pedal. Simplicity of operation does away with the necessity of hiring high-priced operators for these trucks. Where motor-driven trucks can be

kept busy, the General Vehicle Co. of Long Island City, N. Y., claims that with hauls ranging from 200 to 800 feet each truck will take the place of from four to six men. An idea of the rate at which these trucks operate will be gathered from the fact that a time study made in unloading bags of cement at a New York pier showed that it took thirty minutes to unload thirty-eight bags of cement and transport them a distance of 500 feet, where four men were employed operating hand trucks. With an electric truck, two men handled seventy similar bags in seventeen minutes and carried them 750 feet instead of 500 feet. It is not claimed that any such saving may be expected in all cases. There are many classes of work where better results will be obtained with hand trucks; but for those classes of service for which motor-driven trucks are adapted, they give highly satisfactory results.

A manufacturer who contemplates the installation of motordriven trucks will naturally ask himself, "What will it cost to operate such equipment?" For the benefit of such men it may be stated that the average cost of running an electric truck and the necessary charging equipment—including maintenance, interest, depreciation, taxes, insurance and charging current—is \$2.50 per working day, exclusive of operator's wages. A single charge of the battery during the preceding



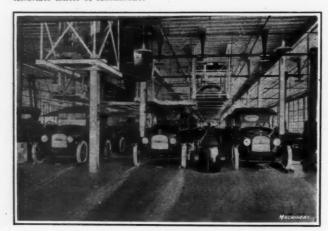


Fig. 55. Progressive assembly of automobiles has been developed to a high degree by engineers of the Willys-Overland Co. Four assembling tracks are provided in the factory, down which cars are run, and conveyors running at right angles to these tracks carry all the different parts to the assemblers. This system has been brought to a high degree of perfection and work is handled very rapidly

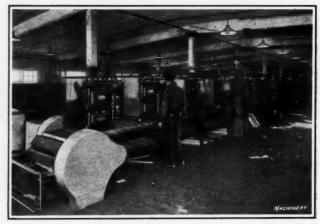


Fig. 56. The benefits secured by progressive methods of assembling in automobile factories have been so marked that this method is now finding application in other industries. The Detroit Stove Works is making use of a conveyor system installed in its plant by the Palmer-Bee Co. of Detroit, Mich., for use in the progressive assembly of gas ranges

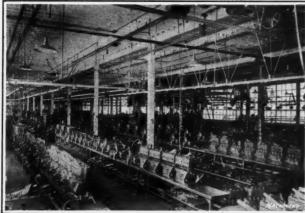
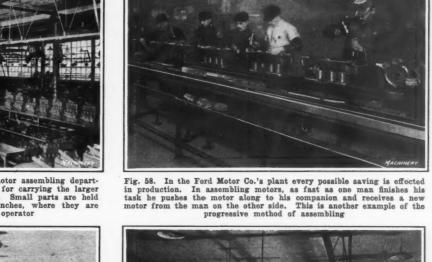


Fig. 57. Overhead conveyors are used in the motor assembling department of the Willys-Overland Co., Toledo, Ohio, for carrying the larger parts of the motors to the assembling benches. Small parts are held in New Britain tote boxes underneath the benches, where they are within convenient reach of the operator



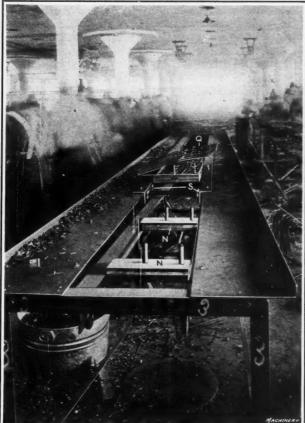


Fig. 59. Progressive methods of assembling are used in manufacturing automobile cushion springs. In the Detroit Wire Spring Co.'s factory, the Palmer-Bee Co. has installed equipment for handling this work. The spring frames are placed on small trucks, on which they are carried along the bench from man to man, and the various parts of the spring are put together

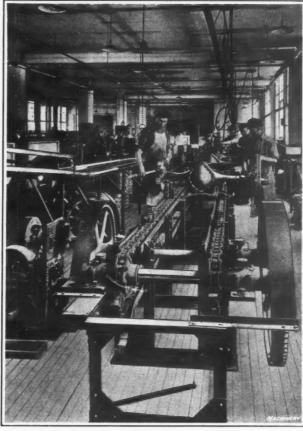


Fig. 60. The Palmer-Bee Co. of Detroit, Mich., makes a specialty of designing and installing time- and labor-saving equipments for handling material in course of manufacture. This illustration shows an outfit installed by this company for assembling automobile transmissions. Two strands of endless chain carry brackets which support the work at each end



Fig. 61. In this case the magnetic generator unit of the motor is carried on an endless belt conveyor, and men with power-driven wrenches are screwing up the nuts. Attention is called to the large number of men at work; this is typical of the intensive production methods in the Ford Motor Co.'s shops

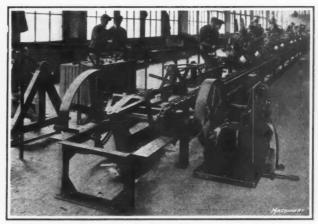


Fig. 62. Formerly the Packard Motor Car Co. assembled clutch units on stands that were distributed over the floor of the clutch assembling department. The Palmer-Bee Co. suggested that the progressive method of assembly be employed in handling them, so a conveyor system was installed, which carries stands similar to those formerly employed



Fig. 63. Where it is necessary to transfer work from an upper floor in a building to an upper floor in another building, much time is lost in taking the work down and up in elevators in the ordinary way. Sometimes it is possible to have a conveyor carry the work right across from one building to the next, as here shown



Fig. 64. In the Studebaker Corporation's factory in Detroit it is necessary to transfer automobile frames from one building to a floor two stories higher up in an adjacent building. For this purpose a conveyor system was installed by the Palmer-Bee Co. It consists of a structural steel frame with rails, over which the automobile frames are pulled by an endless chain conveyor



Fig. 65. Factories engaged in building heavy machinery, structural iron work, etc., find it necessary to have cranes for loading finished product onto cars. This illustration shows the work of loading a keresene tractor onto a flat car. The crane was built by the Northern Engineering Works of Detroit, Mich.

night is sufficient to run the truck with its full load of two tons for 90 to 100 round trips of 1000 feet. Batteries may be charged while in the truck or a complete change of batteries may be made in five minutes. A laborer of average intelligence can be taught to drive one of these trucks in a few hours, and automatic safety control features make it practically impossible to damage the load or for the operator to be injured.

One point that stands out in favor of the use of motordriven trucks is that when a man can ride, little difficulty is experienced in keeping him at work; but when he is required to pull a heavy truck, which is a tiresome job, he is not likely to stay long. Hence the motor-driven truck may be said to constitute a means of saving employers the expense of breaking in new help. In conclusion, it may be stated that motordriven trucks may be furnished with flanged wheels for operation on rails, or with rubber tired wheels to travel on the floor. Signal systems of various kinds may be used-such as electric lamps or flags-to show when aisles are clear for the passage of trucks, or when one truck is likely to meet another before reaching the opposite end of an aisle. Electric trucks are built in many designs to meet the requirements of different classes of work. Elevating trucks are made for use in connection with platforms, boxes, etc., and plain trucks are made for carrying loads directly. In addition, there are the so-called tractors designed for pulling one or more cars on which the load is piled.

#### Demountable Body Trucks

Motor trucks may be employed to advantage in many shops for carrying shipments from a factory to the main line of a railway, shipping dock, etc., or for making quick deliveries within twenty or thirty miles of the plant. Where the tonnage to be handled is large, it may be desirable to use one or more trailers in connection with a truck in order to increase its carrying capacity. A good grade of motor truck is quite costly. and this makes it necessary for the firm employing one or more of these trucks to take advantage of every opportunity to secure the greatest possible return on its investment. One way of greatly increasing the amount of service obtained from motor trucks is to use what are known as "detachable" bodies. Two or more of these bodies may be used in connection with each truck, so that when a truck comes in loaded the removable body can be lifted off and carried away by trolley hoists, after which an empty body is substituted so that it may haul away a new load or go out after a fresh load, as the case may be. While the truck is away from the plant the load brought in on the previous trip-which has been removed with the detachable body—is taken to its destination by the trolley hoist, and the empty body is brought back ready to be exchanged for a full body when the truck returns with its next load. This method is said to be the means of increasing the capacity of motor trucks from 50 to 100 per cent when used under conditions that enable maximum efficiency to be attained. In the case of very heavy loads, the detachable body may be furnished with nests so that the load may be divided to bring it within range of the trolley hoists. In some cases the bodies are mounted on auxiliary casters or wheels upon which they may be moved.

#### Progressive Machining Operations

Where machining operations to be performed on a given part are of such a nature that a battery of planers, milling machines, drill presses, boring machines, etc., is required to finish a piece, it is of the utmost importance to have these machines so grouped that the work passes continuously from machine to machine without delays. In many well organized factories the equipment has been so arranged that conveyors, trucks or some other form of device can be used to carry the work from machine to machine with the least amount of time and labor.

An example of this kind is seen in the milling operations on aluminum crank-cases in the plant of the Buick Motor Co., Flint, Mich. The first four milling operations are performed on Ingersoll planer-type milling machines, which provide for handling five upper and five lower halves of the crank-cases at

a time. In operation, the table is run forward under the crossrail, and castings placed ready on the floor are dropped into position in the milling machine fixtures without any attempt to tighten the clamps on the fixtures. Then as the table starts to feed back, the operator starts with the fixtures nearest the cross-rail and tightens up all bolts so that the work is secured for machining. After all the work has been secured, he goes to a position back of the cross-rail and starts taking out the milled cases, which are swung over onto gravity carriers and rolled down to a position ready to go on the next Ingersoll milling machine. In this connection it is important to note that the gravity carriers are made the same height as the milling machine tables so that the work can be transferred from the carrier to the table and vice versa with the minimum effort.

A more highly developed method of progressive machining consists of having tracks laid between different machines on which trucks run that support jigs and fixtures for carrying the work. Fig. 38, in the first installment, shows a view in the plant of the Packard Motor Car Co., Detroit, Mich., where crank-cases are being drilled. There are 200 holes to be drilled in these cases and the complete drilling operation is finished in forty-two minutes; the actual drilling time is thirty-eight and one-half minutes and three and one-half minutes are allowed for setting up and removing work from the jig. The machine tool equipment consists of seven Baush multiplespindle drilling machines with various numbers of spindles and different types of heads, and one radial drilling machine. The jigs are arranged so that they can be pivoted to bring different surfaces of the work into the operating position. Indexpins enter hardened steel bushings in the jigs, locating them accurately for each successive operation, and clamps are provided which secure the jig trucks in place on the tracks. Handled in this way, a high rate of production may be obtained, because the workman is relieved of all physical strain in lifting work on and off machines, it being merely required for him to set the work up in the jig at the beginning of the row and remove it when the job is finished. One workman follows a single casting right down the line, performing all the machining operations required on it.

For boring, milling and other operations where the fixtures are of such a type that it would not be feasible to use a single fixture for a number of operations, a somewhat similar idea may be employed. Instead of having the work and fixture taken from machine to machine on tracks, a roller type conveyor is run parallel to the line of machines, with switches branching off to individual machines, as was illustrated in Figs. 44 and 45 in the July installment. With an equipment of this kind the operator can push a heavy casting along on the conveyor and run it in on the switch to a given machine. The conveyor and the machine table are the same height, so that the operator merely swings the work over from the conveyor and puts it in position in the fixture for machining. When the operation has been completed, the casting is put back on the switch and run up to the main line, upon which it is carried to the switch leading to the next machine. Where this method has been adopted it has been found the means of saving a great deal of time in the performance of machining operations.

#### Laying Out Gravity Carriers

As the name implies, the pitch of a gravity carrier is relied upon to enable the force of gravity to run the load along the conveyor without the application of power from an external source. In designing this type of equipment it is the practice of the Mathews Gravity Carrier Co., Elwood City, Pa., to make the pitch of conveyors from 2 to 8 per cent, but most of the conveyor systems installed by this company have a pitch of 4 per cent. In the construction of conveyor systems of this type, there is a good deal of variation in the lay-out, according to the nature of the work to be carried. Packages with smooth, flat bottoms may be run on these carriers without guard rails, but where the load is irregular in shape some form of guard rail is necessary.

Various expedients are adopted to keep the load running on these conveyors. The most obvious way is to place a guard



Fig. 66. In foundries where moderate loads are to be handled at fairly frequent intervals, it is convenient to use a crane in which the trolley and bridge are operated by hand, and the hoist is driven by power. Cranes of this type are shown here, equipped with "Imperial" pneumatic motor hoists built by the Ingersoll-Rand Co., New York City

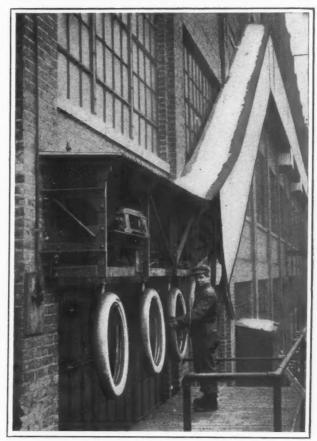


Fig. 67. Where there is considerable congestion in a shop, it may be desirable to hang conveyor systems and similar equipment on the outside of buildings. A case in point is seen in the accompanying illustration, which shows a view of a conveyor system installed in the Studebaker Corporation factory for handling tires, wheels and hubs. The conveyor is an endless chain with hooks for carrying the work

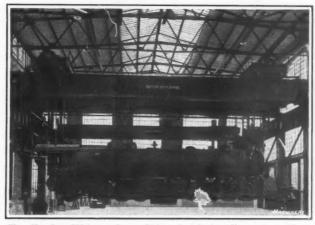


Fig. 68. One 200-ton and one 20-ton electric traveling crane with a span of 75 feet, 6 inches are here shown in use in a railroad shop. These cranes were built by the Niles-Bement-Pond Co., New York City. The weight of the suspended engine is 270 tons. Attention is called to the method of lifting the locomotive from four corners



Fig. 69. This illustration shows a bin at the side of the railroad at the Ford Motor Co.'s plant in Detroit for storing coal, coke, limestone, scrap metal, etc. The Shaw Electric Crane Co., Muskegon, Mich., installed a gantry crane equipped with a grab bucket for handling this material

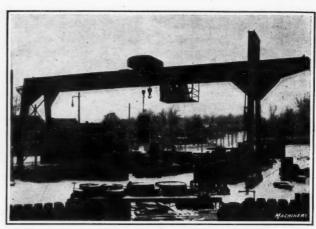


Fig. 70. Gantry cranes are generally used where the amount of service is not great enough to warrant the construction of an overhead runway for a traveling crane. Gantry cranes are more expensive to operate, however, and this may offset the lower first cost. The crane here shown was built by the Northern Engineering Works, Detroit, Mich.



Fig. 71. In large power plants it will often be found necessary to provide special equipment for the handling of fuel, as manual labor is too slow. This illustration shows a monorall bucket hoist built by the Northern Engineering Works for charging coal into boiler hopper storage tanks in a large power plant

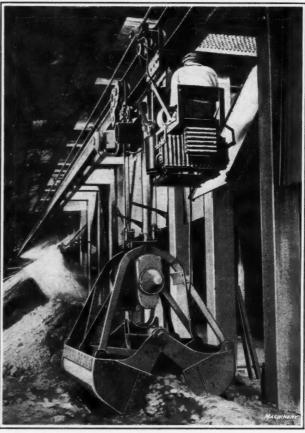


Fig. 72. In foundries where there is a lot of sand, coke and limestone to be handled, it will sometimes be found advantageous to employ a grab bucket. This illustration shows a trolley hoist built by the Sprague Electric Works of New York City, equipped with a grab bucket for use in a foundry. Such an outfit operates at a high rate of efficiency

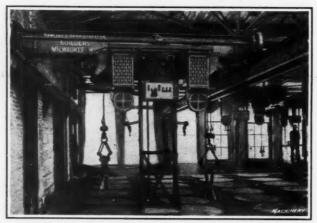


Fig. 73. Crane builders are often called upon to construct special equipments to meet the requirements of various industries. The illustration shows cranes built by the Pawling & Harnischfeger Co., Milwaukee, Wis., especially for handling work in the annealing shop of a car wheel foundry

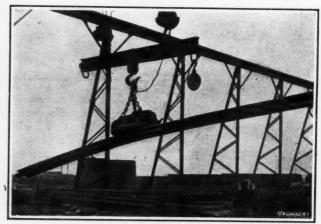


Fig. 74. Lifting magnets are used for handling various iron and steel products. This illustration shows an electromagnet built by the Cutler-Hammer Clutch Co., Milwaukee, Wis., lifting long steel bars. A special arrangement of a beam and two hoists prevents the magnet and its load from rotating

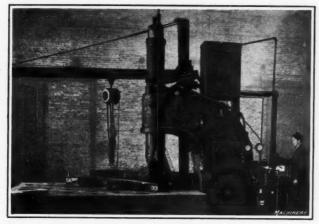


Fig. 75. There are many pieces of work that are a little difficult for one man to handle alone, and if he attempts to do so, he is likely to waste a considerable amount of time in setting up. This illustration shows the use of a jib crane equipped with a Yale & Towne chain block for handling such work

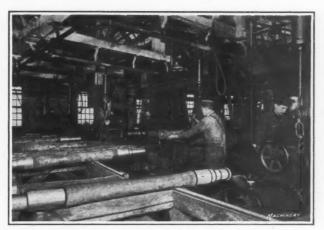


Fig. 76. Car axles are too heavy to be handled by one man. This illustration shows a view in the Griffin Wheel Co.'s plant in Chicago, where each axle lathe is equipped with an air cylinder hoist for setting up work and removing it. Turned axles are rolled on rails to the hydraulic wheel press

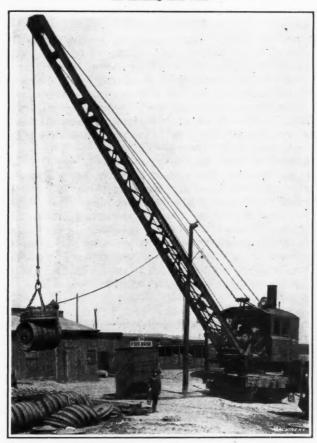


Fig. 77. A locomotive crane is useful for handling materials in factory yards where there is a lot of space to be covered. This equipment may be employed as a switch engine when there is no lifting to be done. The illustration shows a locomotive crane and lifting magnet used by the Griffin Wheel Co., Chicago, Ill., for handling car wheels

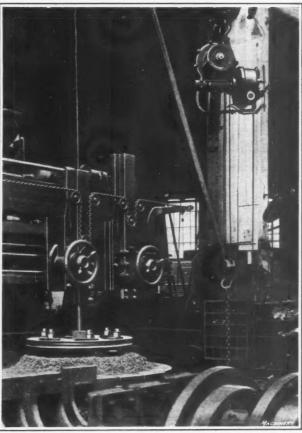


Fig. 78. An "Imperial" pneumatic motor hoist built by Ingersoll Rand Co., New York City, is used to assist the operator in setting up heavy work on a turret lathe and to remove completed work from machine. Having an individual hoist for a machine avoids loss of time by the operator and machine in waiting for assistance

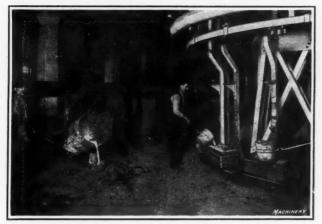


Fig. 79. To facilitate pouring metal into molds in the Ford Motor Co.'s foundry, molds are brought in on a conveyor and transferred to a carousel on which each mold is supported by a pendulum. This swinging support eliminates vibration and prevents molds breaking. Molds are carried away by a second conveyor



Fig. 80. One jib crane can often be arranged to serve a number of machines, molds, etc. In the Griffin Wheel Co.'s foundry, car wheel molds are arranged in a circle, with a jib crane at the center, equipped with an air heist built by the Curtis Preumatic Machinery Co., St. Louis, Mo.

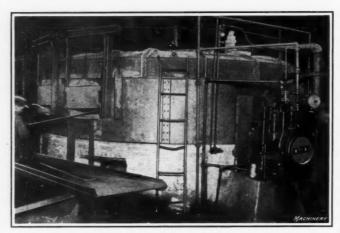


Fig. 81. In the Timken-Detroit Axle Co.'s plant special furnaces with a rotary hearth are maintained at such a temperature that forgings are raised to the proper temperature for heat-treatment by one revolution. These furnaces save space and keep operator busy

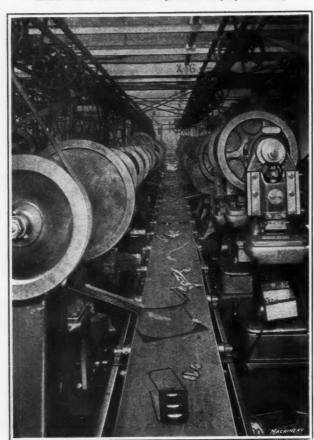


Fig. 82. In the Ford Motor Co.'s plant, use is made of belt conveyors for carrying away the product of power presses. Chutes are provided by means of which the product is transferred from the machines to the belt conveyor which carries it away. This is the means of saving the time ordinarily required for removing the product in trucks



Fig. 83. An elevator raises the work to the upper floor in the Willys-Overland Co.'s plant. This equipment, installed by the Link-Belt Co., Chicago, Ill., consists of an apron-type conveyor with cleats to prevent the work from slipping back. A chute at the left returns the tote boxes to the lower floor

rail at each side so that it is impossible for the load to run off. A simple method and one that is highly satisfactory where the packages or parts to be carried are of fairly regular shape, is to have a small flange at both ends of each roller. This flange rotates with the roller so that there is no loss of efficiency through the retarding action of a fixed guard rail, and still it is effective in preventing work from running off. A still simpler method and one that is effective in cases where the work has a smooth surface to run on is to make the conveyor with two sets of rollers. These rollers are arranged in pairs, with the rollers of each pair inclined at a slight angle, so that the two rollers have a form somewhat similar to the letter V (the angle is much less acute) with the apex pointing in the opposite direction to that in which the load is to travel. The effect of this inclined double roller construction is to keep the load on the conveyor, the tendency of each of the inclined rollers being to force the load toward the center. For handling pig iron and other irregular shaped pieces of this kind, the only way to be sure of keeping the load on the conveyor is to use a guard rail at each side.

#### Use of Revolvator

A machine known as a "revolvator" is built by the New York Revolving Portable Elevator Co., Jersey City, N. J. This is a portable elevator mounted on a revolving base so that the elevator platform may be faced in any direction to receive or discharge a load, as the case may be; ball bearings in the revolving base enable the elevator to be easily swiveled when carrying its maximum load. This type of equipment is used for a variety of different classes of service in industrial plants, but a typical case is where it is desired to raise or lower a load and turn the elevator in the direction in which the load is to be deposited. For instance, suppose that a stock-room is arranged with aisles running over to the wall and the necessity for economizing in the use of space makes it necessary to stack material up almost to the ceiling. Here the revolvator may be used to excellent advantage, as the material is brought on elevating trucks or in any other convenient way and deposited on the platform of the revolvator. The load is then raised to the desired height and the platform turned so that the load may be run off at either side of the aisle onto the top of the material already stacked.

A similar use is where sheet metal and other material is being stacked in racks; the revolvator carries the load down an aisle, and when it reaches its destination, the platform is raised and turned through one-quarter revolution to allow the load to be slid off onto the racks. Another similar example is where heavy dies for use on power hammers and presses are kept in storage racks. These dies are so heavy that they are hard to handle, and work of this kind can be done conveniently by pulling them out on the platform of the portable elevator, which is then lowered to a convenient height. The entire elevator then serves as a truck on which the die is pulled to the machine on which it is to be used. Here the platform of the elevator is adjusted to bring it to the same height as the bed of the machine, so that the die may be easily slid off the elevator platform, into place on the machine.

Portable elevators of this type are made in two standard sizes, with capacities for handling loads up to 800 pounds and 1800 pounds, respectively. By the use of special bracing, elevators have been made for carrying loads up to 2500 pounds. Elevators up to and including seven feet in height are made with the structure in a single piece; but when the height exceeds seven feet, the structure is hinged so that no difficulty is experienced in pulling the elevator through doors from one department to another. The platform is raised by hand by means of gearing turned by a crank. When it is necessary to lower the load, the first step is to take the crank off the squared end of the shaft; the crank is then fitted onto a lowering brake, and until this is done the platform cannot be lowered. By means of the crank, the brake may be adjusted to any required degree while lowering the load.

In revolving the entire structure of the elevator, the first step is to withdraw a locking pin that holds the elevator in one of four 90-degree positions around the complete circle. When this pin has been withdrawn, the elevator is usually turned by hand, taking hold of the elevating crank. Some users of portable elevators employ them as a means of transporting material from one department to another located on a higher or lower floor. This is done by having a trap door in the upper floor through which the elevator platform may be raised or lowered with the material. Such an arrangement would only be recommended where departments are not laid out in the normal way; ordinarily, where there is a demand for equipment to transfer work from one floor to another, some permanent form of elevator would be more desirable.

#### Portable Scoop Conveyor

For handling coal of all grades, coke, ashes, crushed stone, sand, gravel, small castings and a variety of other similar material, the Portable Machinery Co., Inc., Passaic, N. J., is now building the portable scoop conveyor shown in Fig. 87. This equipment consists of a scoop which can be buried in the material to be handled, and an endless traveling belt which carries the material up and discharges it into a wagon, chute or other receiver. The conveyor belt has transverse cleats to prevent the material from slipping back down the incline. One man and this scoop conveyor can handle coal or similar material at the rate of one ton in one and one-half minute, i.e., forty tons per hour. This outfit can be equipped with an electric motor or gasoline engine for driving the belt, and as it weighs only 900 pounds and is mounted on wheels, it may be easily taken to any desired place. The amount of power required to drive the conveyor is 11/2 horsepower.

A special machine is used at the plant of the Boss Nut Co., Chicago, Ill., to charge tumbling barrels with blank punched nuts, take these nuts from the tumbling barrels, and distribute them in bins located convenient to the tapping machines. This apparatus consists of a modified form of the standard tiering machine built by the Economy Engineering Co., Chicago, Ill. It has a cantilever type of platform, open on three sides. The main uprights extend into a pit about three and a half feet below the floor level.

The platform consists of two arms, on which run the flanged wheels of a small transfer car; the latter, in turn, carries a pair of rails at right angles to its direction of movement. On these rails is placed a small hopper-bottomed car with a capacity of about 2000 pounds of punched nuts. The pit extends under the tumbler, and at the bottom are rails to allow the transfer car with the hopper car to be moved to a position directly under the tumbler. A steel frame is also provided above the tumbler so that the transfer car can be moved over the tumbling barrel. At one side of the machine is a row of bins, over the tops of which runs a track on which the hopper car moves.

To charge the tumbler, the platform of the machine, with the transfer and hopper car, is lowered to the bottom of the pit, bringing the top of the hopper car on a level with the floor. The punched nuts are then dumped into it from the kegs in which they have been deposited at the punchers. The platform with its load is then raised to the top position and the transfer car with the loaded hopper car moved to a position over the tumbling barrel, where the gates at the bottom of the hopper are opened and the nuts drop into the tumbling barrel. Here they are tumbled with sawdust until polished. The tumbling barrel is provided with perforations and a wooden tray is placed under it while the tumbling operation is being carried on, so that the sawdust gradually works out and is entirely eliminated by the time the polishing is completed. To empty the tumbling barrel, the transfer car is again moved into the elevator platform and lowered to the position in the bottom of the pit, where it is moved under the tumbler and the polished nuts are deposited in the hopper car. It is then returned to the elevator and hoisted to the level of the track over the bins and then pushed by hand to the proper bin, where the load is deposited by opening the gates in the bottom of the hopper.

The elevator is operated by means of a three-horsepower General Electric motor, through silent chain drive to a series of machine-cut spur gears connected to a drum upon which the steel hoisting cable winds. Automatic top and bottom

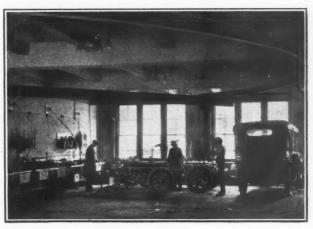


Fig. 84. A jib crane must be provided with support for the outboard end of the beam. This is often done by means of tie-rods. In this case the ceiling is too low to permit of this construction, so the outer end of the beam is furnished with a trolley which runs on a semi-circular rail



Fig. 85. In automobile tire factories there are a lot of heavy molds to be handled, and some means of assisting the operators must be provided. This view shows a chain hoist built by the Wright Mfg. Co., Lisbon, Ohio, in use in the Knight Tire & Rubber Co.'s plant. The molds are being placed in a vulcanizer



Fig. 86. Combinations of equipment are often necessary. This view in the Detroit Wire Spring Co.'s shops shows a conveyor and elevator. Assembled cushion springs are carried to the crating department, where they are packed, and the elevator carries crates to shipping department

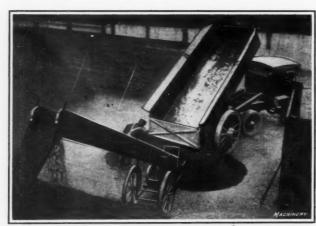


Fig. 87. For handling loose material, such as coal, sand, etc., a scoop conveyor is made by the Portable Machinery Co., Inc., Passaic, N. J. This consists of a scoop and a power-driven belt conveyor that carries the material up an incline and delivers it into a chute



Fig. 88. There is often lack of system in handling metal goods which are to be heat-treated; this results in an unusually heavy charge against the work. The Chain Belt Co. of Milwaukee. Wis., has installed a special apron-type conveyor with chutes for carrying heavy drawn steel shelp.

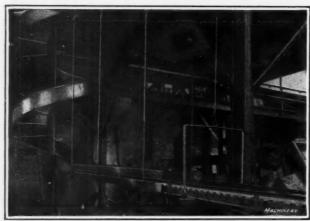


Fig. 89. For unloading flywheel castings from freight cars, the Cadillac Motor Car Co. of Detroit, Mich., has a spiral steel chute leading down from the platform on which the load is discharged. The castings are ejected from the chute onto a gravity carrier

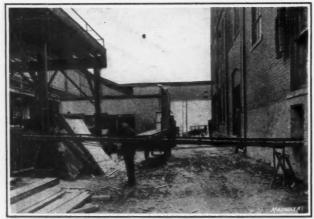


Fig. 90. This illustration shows the gravity carrier leading from the spiral chute shown in Fig. 89 to the machining shop. The carrier is suspended on cables so that it may be raised to provide the necessary head room for a team to go underneath

stops and other safety features are provided, making the machine largely automatic in its action, one ordinary laborer being all the help required.

#### Bringing the Saw to the Shafting

The Mechanical Appliance Co., Milwaukee, Wis., has developed a novel method of handling the steel shafting that it uses in the manufacture of its product. Shafting of from 1/2 to 31/2 inches in diameter is used. It was found that a great amount of time and labor was consumed in bringing heavy shafting to the hacksaw from the racks onto which the shafting was loaded from the trucks. Instead of bringing the heavy shafting to the hacksaw, the motor-driven hacksaw is brought to the pile of shafting. The shafting is stacked onto the racks from the trucks. The hacksaw is raised to the correct level of the shafting by means of a tiering machine built by the Economy Engineering Co. One operator is able by means of this arrangement to take care of the complete operation of cutting off shafting from 1/2 to 31/2 inches in diameter. As many as six men were formerly employed to carry the long pieces of the heavier sizes of shafting to the saw.

#### Adapting Transportation Methods to Requirements of Shop

In working out methods of progressive assembly for use in his factory, a manufacturer must bear in mind the volume of work which is to be handled. It would not pay to install a complex equipment of conveyors, trolley systems, etc., to facilitate handling work unless the volume of product was sufficient to keep equipment of this kind employed so that a reasonable return would be earned on the investment. Even in highly organized shops handling a moderate volume of product each day, little attempt is made to employ a complete outfit of mechanical contrivances for handling the work, because it is realized that there would be little likelihood of obtaining a satisfactory return on the investment. Recently we have seen some exceptions to this rule that are probably due to the condition of the labor market. Unskilled labor has been so scarce and has commanded such exceptionally high prices that some manufacturers have substituted mechanical means of handling as far as possible. This has been particularly true in shops engaged in certain munitions work where the necessity for making deliveries at an early date has demanded the employment of every possible means to increase production rates.

Plants handling an extremely large volume of product are best suited for the installation of complete systems of conveyors, trolleys, gravity carriers, chutes and other forms of equipment arranged in combination, so that as soon as one workman or group of men have completed their task on a given piece of work it may be placed on a mechanical carrier that will convey it to the department where the next operation is to be performed. Aside from the reduced cost of production made possible through the reduction in help, the employment of mechanical carriers has another important feature which commends it to the attention of manufacturers operating large factories in which there is likely to be a congestion of machines and product. Unless mechanical carriers are used, the alternative is to make transfers on trucks pushed by hand or by power, and the handling of a large amount of work in this way is bound to create confusion-especially when aisles are blocked or there is other interference with the movement of the trucks.

In an article of this kind it is the aim to explain fundamental principles and describe methods which the average manufacturer can employ in his own shop. On this account, the methods of handling material and product in extremely large plants are not entered into in detail, inasmuch as they require complete installations of mechanical transporting facilities and an engineering staff capable of laying out all kinds of equipment. Nevertheless, all manufacturers will be interested in reading of the equipment employed in the factory of the Willys-Overland Co., Toledo, Ohio, for the final work of assembling parts of automobiles.

#### General Arrangement of Equipment

The department in which the final assembly is conducted is laid out with four tracks, down which the automobiles are

pulled by chain conveyors that were installed by the Link-Belt Co., Chicago, Ill. The automobile frame is placed on this track and a hook on the chain conveyor takes hold of the front axle to draw the frame along. Features of the progressive method of assembly have been explained previously, so they need not be considered here. The point of greatest interest is the arrangement of the auxiliary carrying systems that bring parts to the main assembling track at the different points where the parts are to be assembled onto the car. There are four of these tracks that run lengthwise down the shop, and a large number of conveyors running crosswise. Each of these cross conveyors brings such parts as lamps, mud guards, radiators, etc., to the four main assembling tracks at those points where the different parts are to be added to the car; and all the time that this continual stream of parts is running across the shop, the automobiles in course of assembly are running lengthwise, so that as each car passes down one of the assembling tracks the different parts which go to make a complete car are brought over to the assembling track and secured in place. This system has been carried to such a degree that when the gasoline tank is delivered to the assembling track by one of the cross conveyors, it contains sufficient gasoline to allow the completed automobile to run out of the assembling department on its own power.

In the various manufacturing departments, as well as in the assembling department, use is made of conveyor systems for handling work in course of manufacture and finished parts. For the parts of a product as complex as a modern automobile, it will be evident that a great variety of carrier systems must be provided, and in the Willys-Overland plant use is made of practically all the standard conveyors, trolleys, etc. For instance, completely assembled motors are handled on aprontype conveyors or on trolley systems, from which they are suspended in a suitable sling. Advantage is taken of the circular form of wheels and tires, and they are rolled down gravity carriers. Gravity is also employed for carrying certain forms of castings and similar parts, but it is necessary to provide some form of roller conveyor, because the castings could not be rolled. In the case of lamps, mud guards and many other parts of a like nature, there is no better method of carrying than on a trolley system, and extensive use is made of this form of equipment. In addition to standard conveyors, many special forms of equipment have been provided for handling parts of unusual form, and a general idea of the diversity of the carriers that have been installed by the Willys-Overland Co. will be gathered from the illustrations presented in this and the preceding installment, showing views in this company's plant. These are by no means complete, but they serve to give an idea of the great variety of methods of handling that have been adopted to meet different conditions and the care that has been taken by this company's engineering department in studying all the available methods and adopting those that have the greatest number of features to commend them.

## Development of Special Forms of Carriers

In working out the transportation system for any factory, the engineer in charge of the work has at his disposal numerous forms of standard equipment that are manufactured by plants making a specialty of this work, and it is desirable, whenever possible, to adopt the use of standard forms of equipment, because a plant specializing in such work can usually furnish equipment at a price considerably lower than that at which special equipment could be made for a given service. There are many cases, however, where the nature of the work to be handled is such that it demands the use of special equipment, and under those circumstances the engineer who is laying out the transportation system would be called upon to design suitable equipment for the work. This may involve the development of special methods of handling, but in many cases it will be found possible to use standard equipment and add special features to adapt it for a given service.

Where it is found that standard equipment cannot be obtained for handling the work, the next step of the engineer should be to ascertain whether certain standard forms of equip-

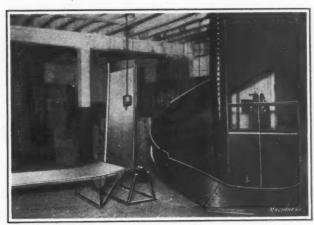


Fig. 91. Where spiral chutes are employed to carry work through a building, it is often desirable to discharge the load on some of the floors through which the chute passes. The chute shown (Mathews Gravity Carrier Co., Elwood City, Pa.) has a branch for this purpose

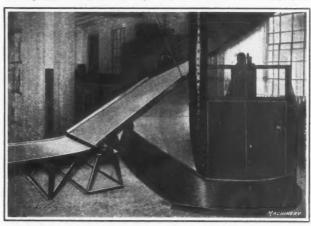


Fig. 92. This illustration shows the same equipment shown in Fig. 91, but here connection is made with the branch chute. Attention is called to the fire door; this is held open by a fusible link, which will melt and allow the door to close automatically in case of fire

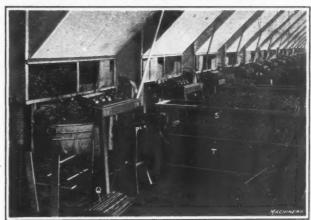


Fig. 93. In the Detroit Wire Spring Co.'s shops extensive use is made of chutes for carrying work from upper to lower floors. Here we see chutes down which coiled springs are delivered to the department in which these springs are assembled into strips

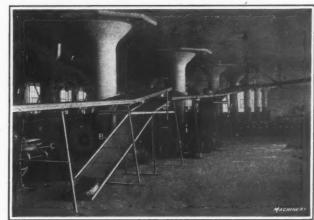


Fig. 94. Where gravity carriers are used it is desirable to provide for discharging the load at different points in the shop. In the illustration provision is made for raising sections of the carrier at different points, so that the load may run under the rollers and slide down the chute

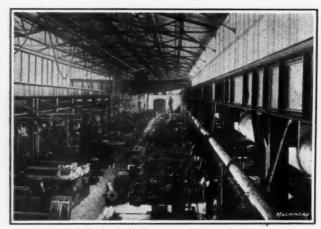


Fig. 95. In some machine shops compressed air is preferred to electric power. Such a case is shown in this illustration. Attention is called to the way in which the hose connection to the pneumatic motors is hung in festoons so that there will be plenty of length to enable the crane to run to the far end of the building



Fig. 96. When a number of trolley hoists are used on rails running parallel to each other, it is desirable to provide means of transferring trolleys from one rail to another. This can be done with a transfer bridge carrying a section of rail that may be lined up with some one of the main rails. The hoist is run onto the rail on the transfer bridge

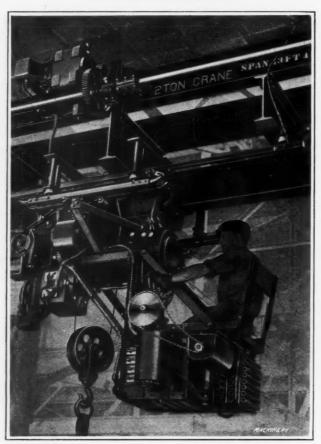


Fig. 97. This illustration shows a close view of the trolley in place on the rail of one of these transfer bridges. The trolley is locked while the bridge is in motion so that it cannot run off the rail. This equipment was built by the Sprague Electric Works, New York City

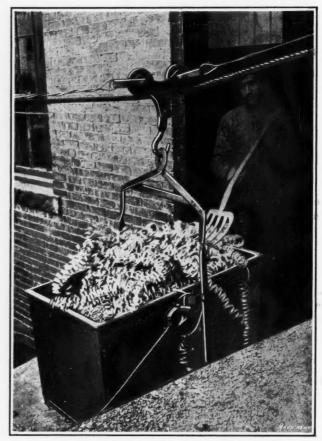


Fig. 98. In machine shops that produce large quantities of chips means must be provided for hauling these chips away to the scrap pile. The illustration shows a skip loaded with chips, which is pulled over to the scrap pile by a laborer, who removes the contents with a pitchfork



Fig. 99. In manufacturing military rifle stocks, each stock must be finished so as to present a good appearance. In the United States arsenals special trucks are used to carry the finished rifle stocks to prevent marring finished surfaces



Fig. 100. Durability is one of the most important features of any form of factory equipment. The Timken-Detroit Axle Co. makes steel boxes for use in connection with elevating trucks for carrying heavy metal parts, which are practically indestructible

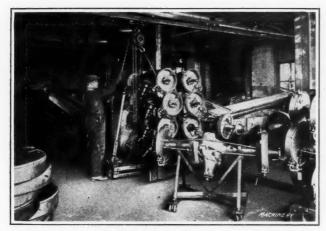


Fig. 101. In the Timken-Detroit Axle Co.'s factory axles are delivered to local factories on special motor trucks. A trolley hoist lifts an axle off the small truck onto a stand; when eight axles have been put on the stand it is picked up on an elevating truck and carried to the motor truck



Fig. 102. This illustration shows how elevating trucks built by the Stuebing Truck Co., Cincinnati, Ohio, are used for handling the product of the Cincinnati Shaper Co. Machines are placed on skids so that they may be handled in the minimum time. The elevating truck enables the machines to be easily picked up and taken to exactly the desired spot

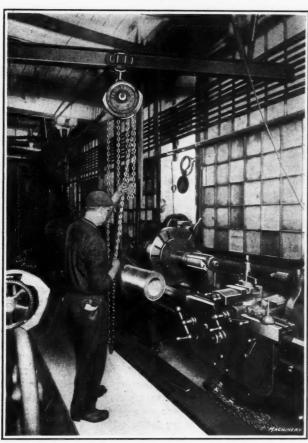


Fig. 103. In setting up heavy work on machine tools, it is desirable to use a trolley hoist in connection with each machine to conserve the operator's time. This illustration shows a chain hoist built by the Ford Chain Block & Mfg. Co., Philadelphia, Pa.

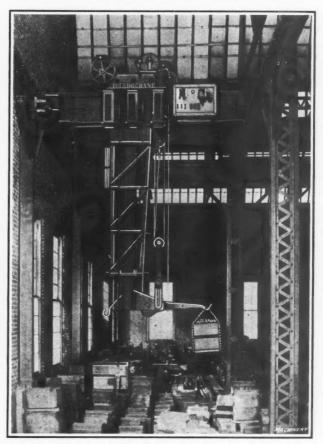


Fig. 104. The crane built by the Toledo Bridge & Crane Co., Toledo, Ohio, is used for placing dies on hammers or presses and transferring them to and from the storage department. The arm that carries the lifting hook is raised and lowered by means of cables



Fig. 105. For handling lumber, the Covel Mfg. Co., Benton Harbor, Mich., manufactures what is known as the "Ross" lumber truck. A load is built up to the desired size, after which the truck is driven over it and the load picked up. It is claimed that the cost of handling is six cents per 1000 board feet

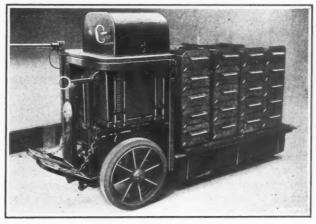
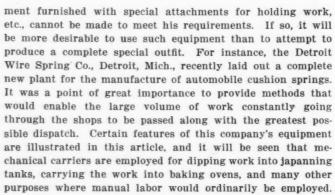


Fig. 106. This illustration shows how steel balls are handled in the New Departure Mfg. Co.'s plant in Bristol, Conn. Balls are placed in steel tote boxes made by the New Britain Machine Co., New Britain, Conn., and stacked up on the platform of an elevating truck built by the Elwell-Parker Electric Co., Cleveland, Ohio



Fig. 107. In handling the progressive assembly of automobiles, the Willys-Overland Co. has tracks down which the cars are run during the process of assembly. Overhead trolley systems running at right angles to the line of travel of assembling tracks carry various parts to the assemblers.



A bundle of coiled wire springs does not weigh very much, but it is of necessity quite bulky and calls for some special method of handling. The Detroit Wire Spring Co.'s transportation equipment consists largely of trolley systems, and to provide for carrying wire springs on trolleys it was necessary to develop special forms of carriers which could be used in conjunction with standard trolleys. This was worked out by arranging baskets for handling bundles of coiled springs and long racks on which a number of assembled cushion springs could be suspended. The adoption of this method enabled the engineering department of the Detroit Wire Spring Co. to buy standard hoists, trolleys and rails from manufacturers of this type of equipment, and then merely make its own racks, so that there was little special work to be done in getting everything ready for use. Needless to say, this was a less expensive installation than would have been a special outfit built for a particular class of service.

# AFTER THE WAR-WHAT OF MACHINERY EXPORT?

Opinions regarding the export of machinery after the war range from extreme pessimism to broadest optimism. England and Germany have been the most potent competitors of America in the machinery market, but Germany is arrayed against us, and it is reasonable to premise that the nations now at war will later cooperate with their present allies along economic lines. Further, for a considerable period at least, the products of Germany will find little favor among the Allies, with the possible exception of Russia. It would thus appear that for some time we may reasonably anticipate having only England as a serious competitor. Later, Canada may become an important factor in the machine-tool industry.

Although the present great demands on the resources of Europe have encouraged in England the highest possible development of those classes of machinery that have a direct bearing on the war, there has probably not been a similar development of automatic and other types of machines that until a few years ago were peculiarly American. Therefore,

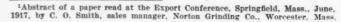




Fig. 108. Reference has already been made to the desirability of using combinations of equipment for handling material and produce which is being passed through a factory. This illustration shows the combination of an elevator, a gravity carrier and an apron-type conveyor for raising work from the lower floor and transferring it through the shop

in many of these lines we may expect to occupy a commanding position in the industry.

Another factor that will loom large in our machine-tool industry is the labor question. While there may be no reduction in wages in this country for a number of years, because of the labor shortage, etc., wages abroad will so increase as to materially aid our export business. Further, the return of those soldiers, from the less enlightened sections, who have been prisoners in Germany will create among their people desires for the better things of life, and they will be satisfied with nothing short of an approximate fulfillment of these desires. However, regardless of the apparently favorable competitive conditions and the essential needs for the work of restoration, as well as the meeting of normal demands, our prosperity following the war will be largely dependent on the restoration program. Will our allies inaugurate a "pay-as-you-go" policy, which contemplates reconstruction through their own resources, or will they avail themselves of America's credit so that the devastated districts may utilize to its fullest capacity the labor of their remaining populations?

Indications are not lacking that Europe contemplates an eventual industrial development far beyond that attained prior to the war, thereby utilizing a large proportion of that great army of metal workers that during the present crisis is supporting the armies at the front. Heavy purchases of machinery are being made, largely for use after the war. Besides, many difficulties have developed during the war which seriously interfere with satisfactory financial arrangements; this has been most evident as affecting sales to Russia. Also for some time after the war we may expect to be handicapped through a lack of shipping facilities.

Assuming that the views here expressed as to the immediate future in Europe are far too optimistic, are there other fields wherein we may develop an outlet for our surplus product? Canada has but recently experienced the prosperity that comes from intensive industrial effort; nothing short of continued development along these lines will satisfy these "Yankees of the North." South America, which has purchased German goods so heavily, is now looking to us for supplies. India, South Africa and Australia will favor England whenever possible, but China, although regarded by Japan, from a commercial standpoint at least, as her rightful heritage, strongly favors American things in her industrial upbuilding.

One factor that will decrease industrial unrest and materially improve our export business is the establishment of fair standards of production and wages. If this problem is correctly solved, one of the greatest handicaps to an aggressive seeking of world trade will be removed. There is also a feeling on the part of the foreign buyer that when our business is good at home, scant attention is given business abroad; as soon as business is less prosperous, there is a rush to dispose of our products in the foreign market. If the foreign buyer of machinery is given value received in the goods purchased and the attention necessary to produce the results to which he is entitled, he will be loyal to his source of supply.

# GAGES FOR TIME-FUSE PARTS1

PROBLEMS IN THE MANUFACTURE OF GAGES FOR RUSSIAN TIME FUSES AND METHODS BY WHICH THEY WERE SOLVED

BY DONALD A. BAKER 2

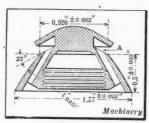


Fig. 1. Cap of Russian Time

ANY of the gages and jigs used in the manufacture of Russian time fuses present unusual problems to the toolmaker. In order that the use of the gages and jigs may be clearly understood, the parts of the fuses are illustrated; Fig. 1 shows the cap, Fig. 2, the top ring of the fuse, and Fig. 3, the body. In Fig. 4 is shown a gage

for testing the relation of the various holes in the top ring. As a number of these gages are required by the inspectors, and as they wear rapidly, a master gage, Fig. 5, is used for testing them and keeping them standardized. This consists of a piece of annealed tool steel, bored out to fit over the center plug of the working gages and having the necessary holes properly located for testing the gages. The special tools and fixtures required for making the master gage were so designed that they could be used in the manufacture of the working gages. The master gage is made as follows: After a piece of steel is roughed out and a 5/16-inch hole reamed in its center,

it is placed on a mandrel and turned and faced to the proper size, enough material being left on the faces to grind them perfectly parallel. After grinding, hole A is bored, the work being strapped to an angle-plate, swung on the bench lathe faceplate. The angle-plate is located the proper distance below the center by plug A, Fig. 6. One end of the plug passes through the hole in the faceplate, and is held in a spring chuck, while the other end is turned to the proper diameter for locating the angle-plate when the plate is brought against it, as shown.

The work is then located approximately on the angle-plate, and the lathe spindle is turned until the face of the plate, with the work attached, is at right angles with the top of the lathe bed; this is tested by placing a parallel across the ways of the lathe and using a square from the surface of the parallel. An indicator attached to a surface gage is then used to set

the work central, being brought first against one edge and then against the other, the lathe faceplate being turned a half revolution for this purpose. After the work is securely strapped, it is tested to see that its position was not changed when tightening the clamps. The work is then center-drilled with a combination drill and counterbore. It is drilled a little smaller than the desired size, and a small boring tool is used to enlarge and true up the hole sufficiently to start a reamer; the starting hole must be of the proper size for the reamer to fit into it. This operation of boring and reaming is repeated several times; for instance, 0.002 inch may be removed with the first reamer, about 0.001 inch with the second, and 0.0005 inch with the third—the last being more of a burnishing than a cutting operation. The finishing reamer should leave between 0.0002 and 0.0005 inch to be removed with a solid lap. The lap is made of either brass or copper, preferably the latter, charged with washed flour of emery. It is held in the fingers and the work revolved against it.

#### Boring Angular Hole in Master Gage

For the next operation, boring the angular hole B and the two half holes C and D, Fig. 5, a special angle-plate is used on the bench lathe faceplate. This consists of a flat plate A,

<sup>1</sup>For other articles on making fuses, see "Manufacturing Parts of Type 80 Time Fuses," in the December, 1916, number of Machinery, and other articles there referred to.

<sup>2</sup>Address: Williams Mfg. Co., Ltd., Montreal, Canada.

Fig. 7, which is ground perfectly parallel, and a plate B, shaped up and ground accurately on the faces and edges, and having accurate angles. An accurate angle-plate and sine bar are used to make the angles correct. The master gage is placed over a plug inserted in a 5/16-inch hole C bored and reamed near the center of this plate. The plate also contains two holes D and E for locating and boring the two half holes in the master gage; while this is being done, plate B is used separately from plate A. These two holes are carefully located by the following method: First a hardened, ground and lapped plug A. Fig. 8, is made. One end of this plug fits the center hole in plate B and the other end is  $\frac{1}{2}$  inch in diameter; near the middle is a disk-like section. The diameter C of the disk is such that when two 1/2-inch standard jig buttons are placed directly opposite, one on each side of the center plug and against its edge, as shown, their center distances will be equal

The position of the buttons having been laid out roughly and the holes for the button screws having been drilled and tapped, the buttons are put in place and held lightly by their screws. The plate is then placed on its edge, as shown, and the sine of the angle having been found by calculation, the

to the center distance of the two holes to be bored.

tool D is used to set one of the buttons in position. This tool consists of a tool steel base A, Fig. 9, which is hardened, ground and lapped on the bottom, and several lengths of drill rod, the ends of which have been hardened, rounded off and lapped smooth. These rods are held in the body and can be clamped securely in place by screw C, the body being split at B. The rods are first set to the proper distance from the base of the tool by the aid of a micrometer, one rod being set to the distance from the bottom of the plate to the edge of a button, and the other to the distance from the side of the plate to the edge of a button. The rods are adjusted by lightly tapping them, as when setting an ordinary firm-joint caliper. Sometimes the rods are threaded, when they are adjusted by screwing in or out. To locate the buttons, the plate is set first on one edge, then on the other, using the tool as a feeler by sliding it along the surface plate

underneath the button, and tapping the button in the direction that the feeler shows it should go, until the "feel" is just right. This method applies to the setting of any button, but as in this case one dimension is supplied by the central plug, only one dimension is needed—that from the bottom of the plate to the edge of the button.

The second button on the plate can be adjusted by using a knife-edge straightedge to get the two buttons and the plug dead in line. The straightedge is tried first on one side and then on the other, and the screw of the second button is tightened, when finally adjusted, so that the straightedge no longer

"rocks." After the buttons are set in the proper position, the plate is strapped lightly to the lathe faceplate and one of the buttons indicated until it runs true. Then the straps are tightened and the button again indicated to make sure the clamping has not disturbed the setting; if it still runs true, the button is removed and the hole bored, reamed

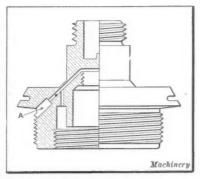


Fig. 3. Body of Russian Time Fuse

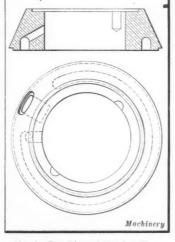


Fig. 2. Top Ring of Russian Time Fuse

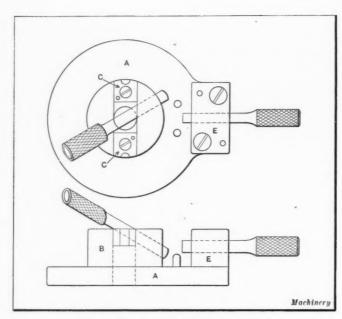


Fig. 4. Gage for testing Holes in Top Ring

and lapped as described for the master gage. After the first hole is finished, the second is treated in a like manner and the plate completed.

To use this master plate, a plug is placed in the center hole and the master gage is placed over this, being held in position by putting a few drops of solder around the edge. Next a special collet with a hole bored through it is placed in the lathe, as shown in Fig. 10. In the end of the collet is placed a piece of 5/16-inch hardened drill rod A, the end of which is ground and lapped to fit the holes in the master plate. After this collet is in place and the end of the plug is ground, the faceplate is put on and indicated on its face, to make sure that it runs true; then the master plate, carrying the master gage, is located by putting it over the center plug in the lathe, and strapped fast in the proper position for one of the two half

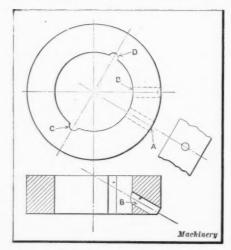


Fig. 5. Master Gage for testing Gage shown in Fig. 4

holes to be bored. The remainder of the operation is the same as described for the other holes. The second half hole is treated in the same manner.

The method of boring the angular hole B, Fig. 5, is one seldom used. Although the locating of this hole is usually considered one of the things that must be found by the most unsatisfactory cut-and-try methods, it may

be accurately done as follows: The two plates A and B are screwed and doweled together, as shown in Fig. 7, converting them into a special boring fixture, or master angle-plate. Then a special plug having a hardened steel ball F at one end is made up. Commercial steel balls are used, as they are readily obtainable and are usually accurate as to sphericity. This plug is placed in the 5/16-inch hole in the plate and the ball is adjusted with micrometers until its center is as far from the face of the plate as the sine of the angle of the hole to be bored. The boring fixture is then strapped to the lathe faceplate and the ball indicated until it runs true, after which the ball and plug are removed, a short, straight plug substituted, and the master gage located in place again over this plug, being held by solder, when it is ready to have the hole B finished in the usual way.

# Finishing Center Hole of Master Gage

The last operation on the master gage is finishing the center hole to size, stock having been left so as to bore the two half holes through solid steel. The gage is held in a castiron spring chuck of the "step" variety, and the hole is roughed out. But as these chucks are not absolutely accurate, the finishing is done in a brass chuck like that shown in Fig. 11. This chuck consists of a special lathe collet A, to one end of which is screwed and soldered the piece of brass B. The collet is placed in the lathe and the brass piece bored out to within a couple of thousandths inch of the size of the outside diameter of the master gage. It is heated with an alcohol lamp

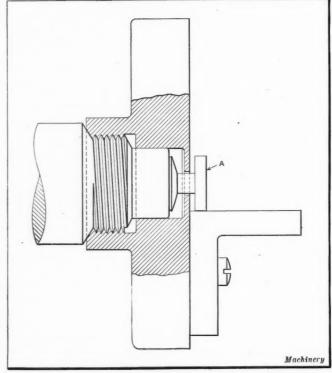


Fig. 6. Angle-plate used to support Master Gage when it is being ground

until the gage will slip into it, and is then cooled with a piece of waste dipped in water; the shrinkage of the brass will hold the gage securely and accurately. The gage is then bored in the regular way, care being taken on the last few cuts not to break down the corners of the two half holes. In boring, 0.01 inch is left for finishing with the bench lathe grinder, and in this operation from 0.0002 to 0.0005 inch is left to be taken out with a lap. When lapped, the gage is ready for use.

#### Making Working Gages

In making the working gages, practically the same methods are used. These gages consist of a base A, Fig. 4, a hardened tool steel locating and gaging nose B, to which are screwed and doweled the half-hole gaging parts C, and hardened steel block E, which is screwed and doweled to the base.

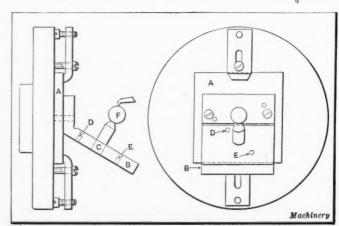


Fig. 7. Special Master Plate for holding Master Gage

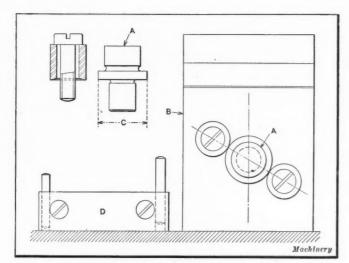


Fig. 8. Plugs for locating Half Holes in Master Plate

In addition there are four hardened, ground and lapped plugs, only two of which are shown; the other two are double ended "Go" and "Not Go" gages for the half holes.

To make this gage, the base A is first machined, the two flat sides being ground parallel and smooth; then the 5/16-inch hole in the center is bored, after which the block E is made in the usual way, placed on the base and located approximately. After the screw holes are located, drilled and tapped, the piece is fastened lightly in place and lined up properly with the center hole in the gage base. It is then fastened securely by the screws, and the dowel-pin holes are drilled and reamed and the dowels placed in them.

The next step is machining the center plug, or locating nose B, which is done in practically the same manner as was described for the master gage, using the same master plate and master angle. A piece of tool steel is roughed out and a hole 0.002 inch less than 5/16 inch is bored and reamed in

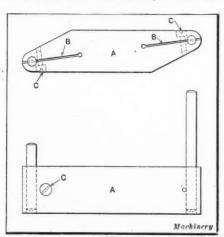


Fig. 9. Tool for locating Plugs shown in Fig. 8

the center. The piece is then placed on a mandrel and the outside turned to within 0.01 inch of size and the top and bottom are faced off. The bottom, being slightly under-cut, leaves a rim 0.004 or 0.005 inch around the edge. This edge makes it impossible for any bulging, caused in hardening, to prevent the bottom from being lapped to a

true surface again without grinding on the surface grinder. After the piece is turned and faced, it is removed from the mandrel and placed on the milling machine, and a 5/16-inch slot, 1/4 inch deep, is milled across the face to take the two pieces that are to gage the two half holes. Screw and dowel holes are then made in it. In boring the angular hole, the same methods and fixtures are used as in making the same hole in the master gage. After this hole is bored and reamed, the piece is hardened. The scale is then lapped out of the center hole, and a short piece of drill rod is caught in the lathe chuck and ground in place until the piece can be wrung onto it. In this position the piece is ground to within 0.0005 inch of size and then lapped, to remove the remainder. Next, the two pieces of soft tool steel are fitted to the 5/16-inch slot milled across the face of the plug, leaving enough projecting at each end so that when the half holes are being made there will be stock all around to support the reamers, etc. In making these holes, the master plate used in making the master gage is again used. In boring, about 0.002 inch is left in the holes, so that after they are hardened and replaced, they can be again set up and ground with a diamond-charged lap used in the bench lathe traverse spindle grinder. Afterward the surplus stock on the ends of the inserted pieces is ground off on the tool grinder freehand, the final finish being given by placing the piece that carries them over a plug, previously ground in the lathe chuck, and finishing with the bench lathe grinder.

The gage is then ready to assemble. This is done by placing the gage over a 5/16-inch plug that is inserted in the hole in the base. Then the master gage is placed over it and the two plugs of the proper size are inserted in the two half holes and in the corresponding holes in the working gage, while a third plug is put through the block E and entered into the proper hole in the master gage. In this position, the center plug, or locating nose of the working gage, is ready to have the dowel and screw holes transferred to the base. After these holes are finished, the dowels inserted and the nose secured

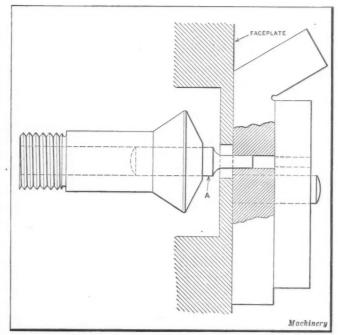


Fig. 10. Special Collet used in making Master Gage

by the screws, the gage is ready for use. The angular hole, and all others that are likely to become out of true in hardening and which cannot readily be trued up by other means, are ground out by using a diamond lap where they are too small for an emery wheel to be used.

#### Height Limit Gage

At B, Fig. 12, is shown a limit gage for testing the height of the under-cut A in the fuse cap, Fig. 1. For the benefit of those who like to work out interesting and practical problems in toolmaking that require a knowledge of simple shop trigonometry, the dimensions of the gage and the cap are given here just as the workman gets them. The gage consists of five pieces; A and B form the body and are doweled and riveted together by the pin D, which is a snug-fitting piece of drill rod. Pins C are driven into body B, the center hole being for clearance to allow the pins to be driven out.

Fig. 15 shows the master plate on which the two parts forming the body were made. This consists of a flat plate A ground parallel on the sides and two long edges. In it are

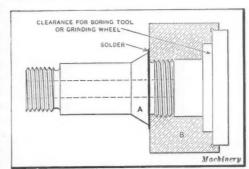


Fig. 11. Brass Chuck for holding Master Gage

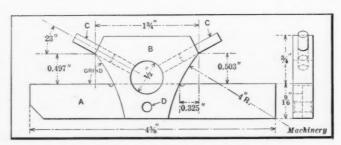


Fig. 12. Gage for testing Under-cut in Fuse Cap

bored four holes B, C, D and E, and two pins F and G are located on it. The positions of the holes, of course, are found by calculations involving trigonometry. After the dimensions have been found, the plate can be laid out roughly, the holes drilled and tapped, and jig buttons screwed in place and then located accurately by using micrometers, a height gage, or other convenient means. In this case, the hole B was first located approximately and the center punched. Then the plate was swung on the faceplate of a lathe, and the hole drilled, bored and reamed to size, but without taking any particular pains to keep it in exact relation to any other part of the plate, as it was afterward to be used as a starting point.

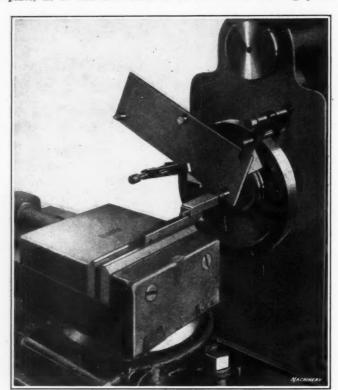


Fig. 13. Locating Holes on the Master Plate

After hole B was finished, the jig buttons were put in place and accurately located for holes C and D. As we had no engine lathe large enough to swing the plate when these holes were being bored, a milling machine was used, as shown in

Fig. 13. Lacking a proper faceplate for this machine, a large internal gear that was part of a high-speed milling attachment was put in place on the machine and a light cut taken off its inside face to make sure that it ran true, holding a lathe tool in the miller vise. Two blocks that had been ground square on the surface grinder were then placed against the trued face of the gear, and the master plate was clamped back against them as shown; then the buttons were trued up by the indicator, which was held fast in the miller vise. After truing them, the work was clamped more securely, again indicated, and the

buttons were removed; a boring tool was put in the miller vise in place of the indicator, and the holes were bored true, using the milling-machine feeds.

After the end holes C and D, Fig. 15, were finished, plugs were inserted and the button for hole E was put in place and trued up from holes C, D and B. As hole E is in the center of the plate, it was bored in the engine lathe in the regular way. The pins F and G were then located. No particular pains were taken with these, as they were under-cut next to the plate; they were then ground on the surface grinder, the plate being stood on edge to get the proper dimension from hole B. Next a drill bushing was inserted in the center hole E and a plug in hole B.

The piece B, Fig. 12, having previously been roughed out of tool steel and the center hole having been bored on the

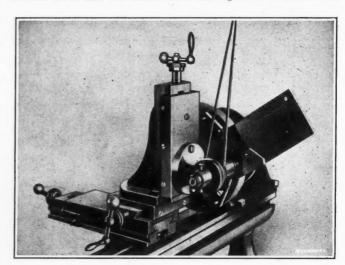


Fig. 14. Milling Edges of Gage and Slots on Master Plate

bench lathe and lapped to a plug fit, was placed over the plug in the hole B on the master plate, clamped fast, and the dowel-hole spot-drilled, drilled and reamed through the drill bushing E. Next, the four-inch radius was milled, about 0.005 inch being left on a side to be ground off. The milling was done on the bench lathe, as shown by Fig. 14. Plugs were inserted through the work and the holes E and B, Fig. 15, in the master plate, while another plug was trued up in place in the lathe spindle from which to swing the plate from either of the corner holes C or D, using the lathe milling attachment as shown. During this operation, the two clearance slots E in the master plate were milled so as to allow a grinder wheel to pass over the work on the following operations.

Next the bar A, Fig. 12, is milled to receive the piece B. This slot is roughed out on the regular milling machine and finished on the bench lathe to within 0.005 inch, using the master plate and the bench lathe milling attachment, as previously described, and locating from the dowel-hole D, which has been drilled and reamed, and the two pins F and G, Fig. 15. Next comes the boring and reaming of the two holes for the pins G, Fig. 12. Figs. 16 and 20 show how the part B. Fig. 12 is located on an angle-plate over the two pins that

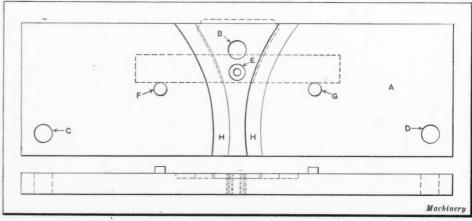


Fig. 15. Master Plate for making Gage shown in Fig. 12

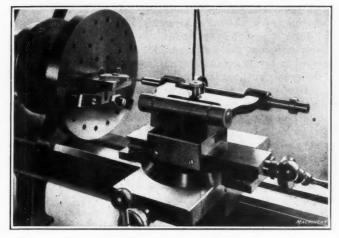


Fig. 16. Lapping Holes in Ends of Gage

were accurately located for holding the piece in the proper position. After the holes are reamed for the pins, the piece is taken to the milling machine and the end milled where it is to fit on the bar, enough stock being left for grinding after hardening. All the pieces are now ready to harden. After hardening, red-hot tongs are used to draw out those parts

that are to be joined together so as to eliminate, as far as possible, any chance of their breaking at this point.

Next the holes for pins *C* are lapped out and temporary pins driven in place, after which the work is taken to a surface grinder and the sides ground parallel with these pins. Then the center holes and the dowel-holes are lapped out until the pieces can be put back in place. Fig. 16 shows the final finishing of the two pin-holes with a diamond lap, using the bench lathe traverse spindle

bench lathe traverse spindle grinder. Next the four-inch radius is ground on both parts A and B, Fig. 12. This work is done on the bench lathe, using the master plate swung from the center plug and the toolpost grinder, as is shown in Fig. 17. The lathe is turned back and forth by hand and the measuring is done from the center plug to the side of the radius with a vernier to get the exact

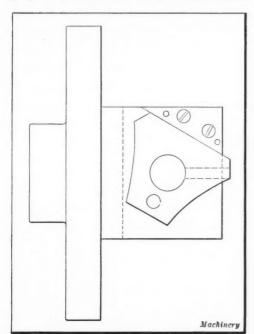


Fig. 20. Holding Gage for boring and lapping Holes in Ends

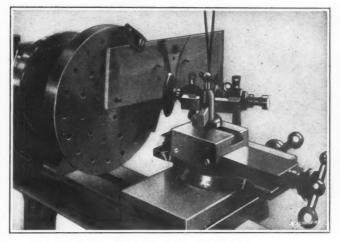


Fig. 17. Grinding Four-inch Radius on Gage

bling them and inserting and heading the dowel, the gage is finished.

Flat Gage for Measuring Depth of Slot in Fuse Ring

At A, Fig. 21, is shown a gage that puzzles the average toolmaker. It is a simple flat gage used to measure the depth

of a milled slot B in the fuse ring; a is the angle of the edge of the ring, and D and E the dimensions given by the part drawing. The dimension X is determined by calculations involving simple shop trigonometry, but measuring this dimension on the piece is another matter. As it cannot be done directly with micrometers, a master gage A, Fig. 18, must be made. This, at first, seems to be as hard a proposition as the working gage, but actually is much easier. A piece of Brown & Sharpe ground tool

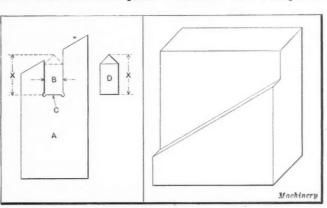


Fig. 18. Master Gage for making Gage shown in Fig. 21

Fig. 19. Master Angle-block for making Master Gage shown in Fig. 18

radius. Parts A and B are then fitted together and the dowel-holes lapped true with each other and a tight fitting dowel inserted, but not headed over. Getting the dimensions 0.503 and 0.497 inch is then a matter of calculation and measurement from a plug inserted in the center hole in part B to the face of bar A, then removing B and grinding A. After assemsteel is roughed out to approximately the shape shown, leaving enough to grind, and is then hardened. It is then placed on a surface grinder, and after the sides and edges, and the surfaces B and C are ground, the angle is ground and dimension X made correct.

But before this can be done, a master angle-block must be

made. This block, shown in Fig. 19, is made of machine steel and is ground perfectly square and parallel on the ends and sides. The angle is obtained with the aid of a sine bar and an accurate angle-plate. When this block is finished, the master gage is clamped to it while the angle is ground on , a surface grinder. To make dimension X correct, a hardened and ground plug D, Fig. 18, is made, the outside diameter and the point being ground at one setting, so as to have the point exactly concentric. The point is rounded with a fine Arkansas oilstone to remove any slight burr

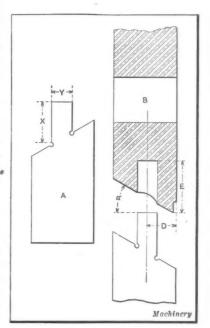


Fig. 21. Flat Gage for measuring Milled Slot in Ring

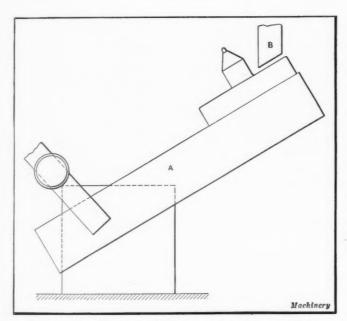


Fig. 22. Using Master Angle-block to get True Angle on Grinding Wheel

or sharpness that can possibly interfere when measuring across it with a micrometer. Care must be taken to remove no more than is necessary. After grinding the outside and the point, the other end is ground, either in the bench lathe or the surface grinder, whichever is most convenient or accurate, until the plug is the proper length. Then the master gage is laid flat on a surface plate and the plug is pressed between sur-

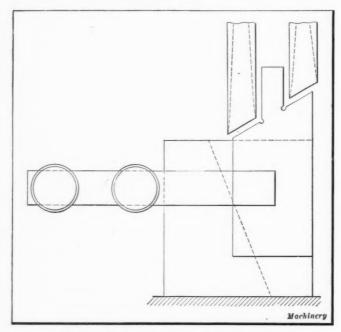


Fig. 23. Method of clamping Gage to Master Angle-block

faces B and against surface C, as shown by the dotted lines, and secured in that position by a drop of melted wax. This wax is made by melting together one part of beeswax and one part of rosin. When the master gage is secured to it, the master angle-block is taken to the surface grinder and ground on the angle until a straightedge will rest on the angular surface and the point of the plug. Great care must be exercised not to grind off too much, as the point of the plug is so small that a ray of light shining through between it and the straightedge may appear to be several thousandths inch, when in reality it is no more than 0.0001 or 0.0002 inch. After the angle is properly ground, the master gage is ready for use.

The working gages are roughed out of Brown & Sharpe ground stock, no particular pains being taken with them other than to leave enough stock on the working faces to grind, after which they are hardened. They are then ground true and parallel on the sides and edges. In order to grind surfaces B, Fig. 18, and the angular faces, the master angle-block is set

up on the surface grinder, as in Fig. 22. After a parallel A is clamped to it, the diamond emery wheel dresser is slid up and down it past the face of the wheel B, thus obtaining the correct angle on the wheel. In Fig. 23, the work is shown clamped to one of the plain surfaces of the master angle-block, in the proper position to grind; the wheel, besides being trued on the face to give the proper angle, is under-cut on the sides with the diamond, as shown by the dotted lines.

In grinding surfaces of this kind, the grinder spindle must have no end play, so it is customary to use a piece of hard wood, sharpened to a blunt point, in the spindle center and keep the spindle in the proper position by lightly pressing against it. If much work of this kind is to be done, a flat spring secured to the wheel guard and pressing against the end of the spindle may be made to answer. After surfaces B, Fig. 18, are ground, the angular faces are ground. As these faces must be parallel and perfectly in line, it is difficult to grind them on the surface grinder, so the bench lathe is used.

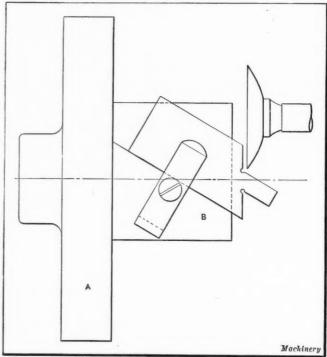


Fig. 24. Grinding Gage in Bench Lathe

In Fig. 24, A is the faceplate and B is the master angle-block, to which the gage is clamped, which, in turn, is secured to and swung from the faceplate of the lathe. The grinding is done with the bench lathe grinding attachments, either the traverse spindle or toolpost grinder being used. Lastly, the end of the gage has to be ground to make dimension X, Fig. 21, correct. This is set up as shown in Fig. 23, only using a straight wheel and trying the work with the master gage.

Gage for Testing Counterbore of Angular Hole in Fuse Body

Fig. 25 shows a gage for testing the depth of counterbore

of the angular hole A in the fuse body, Fig. 3. This consists of the body into which pins are driven. All the parts are of tool steel and are hardened and ground. The hole through the center provides means for driving out the pins easily. The difficulties

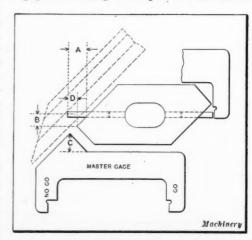


Fig. 25. Gage for Depth of Counterbore of Angular Hole in Fuse Body

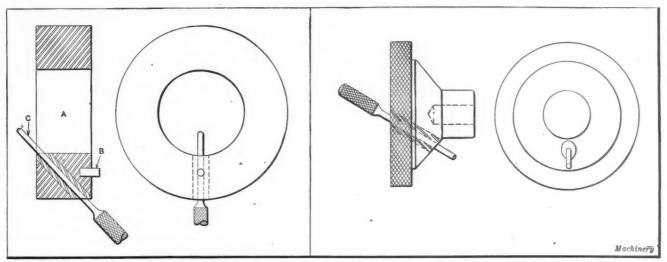


Fig. 26. Gage for locating Angular Hole drilled in Stem of Fuse Body

Fig. 27. Gage for locating Angular Hole, Similar to that shewn in Fig. 26

met in making a gage of this type are in getting the dimensions A and B correct, as neither of these may be obtained direct with ordinary measuring tools.

The method of making these gages is as follows: First the body is roughed out, taking care only to see that the two pins are kept in line with each other. Then the body is hardened, the holes lapped out to receive the pins, the pins put in temporarily, and the sides and edges ground parallel with these, care being taken that both the edges are a given distance from the pins. The pins are then removed and the work is clamped to a master angleblock and the longer of the two oblique sides ground.

0 Machinery

Fig. 28. Testing Slot in Relation to Radius

it is necessary to make up the master gage, which may be tween the master and the gage will look large when they are used to test the working gages. The angles on this master held to the light. After finishing the angle, which makes

gage are generated by a sine bar and an accurate angleplate, grinding them on a surface grinder. The measurement C, which is the difference between B and the edge of the

working gage, is easily obtained with a micrometer. The "Go" and "Not Go" ends of the master gage, which are used to test the length of the pins, are ground in the usual way, as they can be measured direct with the micrometer.

When the short oblique side of the working gage is to be ground, the gage is clamped fast to a master angle-block, set up on the magnetic chuck of a surface grinder and ground little by little. The master gage and a knife-edge straightedge are then used to test it, as shown, until the

Before finishing the short sides and getting dimension B, two edges are perfectly in line. A variation of 0.0002 inch be-

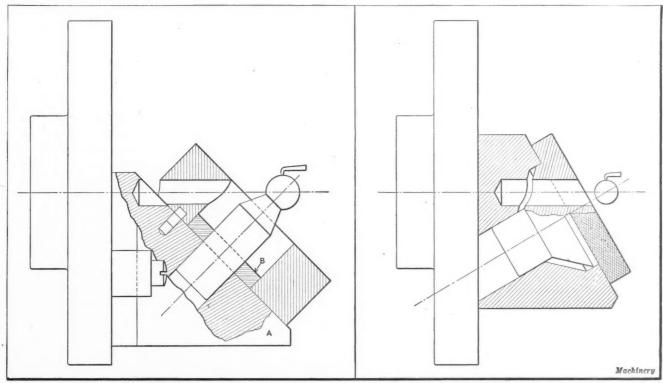


Fig. 29. Method of handling Gage shown in Fig. 26

Fig. 30. Method of handling Gage shown in Fig. 27

dimension B correct, the hardened pins are driven in, leaving just enough projecting to grind. Then, squaring up on an angle-plate, the pins are ground off. the master gage being used to get the dimension D, which has been found, by trigonometry, to bring dimension A right and finish the gage.

Testing Slot in Relation to Radius

Fig. 28 shows a method of measuring a slot in relation to a radius that it is desired to make more accurate than can be done with a height gage or other ordi-

nary means. A is the piece to be measured; B, a special square of hardened and ground steel; C, a smaller square made to fit and slide perfectly in a slot in the larger square and held in place by a flat plate screwed on, as shown. All parts of the tool are made as accurately as possible. The manner of using is clearly shown; the width of the square ends are subtracted from the over-all dimension found by the aid of the micrometer.

## Miscellaneous Examples of Gages and Jigs

Figs. 26, 27 and 29 to 32, show other examples of gage and jig work. Fig. 26 shows a ring A that fits over the stem of the fuse body and down onto the platform, where it is located from the pin B that fits into a hole in the platform. The pin Cis used to gage the location of an angular hole drilled through the stem. The method of handling this gage is as follows: After roughing out the ring A, allowing for grinding and locating the pin B, it is transferred to a master angle-plate A, Fig. 29, which, in turn, is clamped to a bench lathe faceplate, as illustrated. This angle-plate has been previously ground perfectly true on the surface grinder, using a sine bar to make the angles correct; it also has two holes accurately located in it, one for centering the gage and the other for receiving pin B. When the angle-plate has been properly positioned on the lathe faceplate by means of the ball plug, as shown, the latter is removed and another plug inserted; over this plug is placed a ring B that is used to locate the gage. The remainder of the work is performed as has been previously described.

Fig. 27 shows a somewhat similar gage, while Fig. 30 shows the method of handling it on a master angle-plate, using a ball plug as described for the other gages. In all cases, due allowance must be made for grinding all over after hardening and repeating all operations on surfaces that are to be very accurate.

Fig. 31 illustrates a jig for drilling an angular hole in the stem of the fuse body, this being the hole for which the gage shown in Fig. 26 is used. This jig was made in two pieces, being split on center line A on account of trouble experienced from drill breakage. When solid jigs were used and drills broke, they wedged the body fast in the jig and it was difficult to remove them; but by making the jig in two pieces, the upper part can be removed, and the drill easily extracted without removing the jig proper from the drill-press table.

The method of handling this jig is to fasten an angle-iron B to the back side of the jig, then set it up in a lathe, or milling machine, and finish-bore the hole C. At the same setting, angle-iron B is bored to take the ball plug D, thus having the ball plug exactly central. The ball is easily set to the exact apex of the angle by using the depth micrometer E from the face of the jig. After the ball is set, the jig is swung up on a lathe faceplate from the surface F, the top half of the jig is

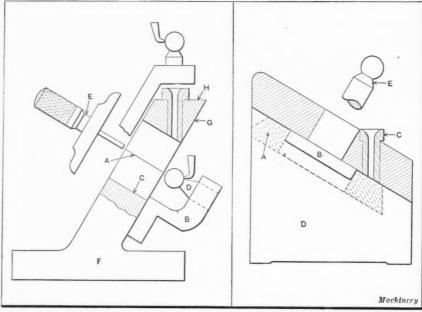


Fig. 31. Jig for drilling Angular Hole in Stem
of Fuse Body

Fig. 32. Jig for drilling Angular Hole in Fuse Ring

Machiner
Fig. 32. Jig for drilling Angular Hole

removed, so that the ball can be reached by an indicator, and the ball indicated until it runs true. The top half of jig G is then put back and bored, reamed, etc., in the regular way.

If the jig had not been made in two pieces, the setting could have been accomplished by locating the ball as already described and then using a second ball fastened to a piece as shown at the top of the view. and transferring the location by means of an indicator, height gage or other means. Another method is to locate a jig button

on face H, using the ball for transferring the location. Fig. 32 shows a drill jig for drilling an angular hole in a time-fuse ring. The ring A is located over the plug B, which, with the drill bushing C, is driven into the jig body D. The manner of using the ball plug E at the apex of the angle is clearly shown.

## RHOTANIUM-A PLATINUM SUBSTITUTE

Rhotanium, a palladium-gold alloy in which the gold content varies from 60 to 90 per cent, is said to form a satisfactory substitute for platinum. It is malleable and ductile and can be welded without the use of a flux or other reagent. Its specific gravity ranges from about 16 to 18.5, according to composition, and its losses by volatilization at temperatures below 1300 degrees C. are less than those of commercial platinum. It can be used, within its temperature limitations, in electric heating units, and is satisfactory for contact terminals in many forms of automatic electric devices. Its behavior when tested on certain magnetos was satisfactory, but experiments performed on a high-grade aeroplane-engine magneto gave negative results. It is not suitable for use with hot concentrated nitric acid nor for electrolytic anodes, but for all other chemical purposes it is entirely satisfactory if the proper composition is chosen and if properly manufactured. Certain of the alloys have given good service in dentistry when used for pins and baked into porcelain teeth and as thin foil and heavy sheet for other types of construction. Rhotanium is said to be superior to pure platinum for use in jewelry; it is harder, stronger and takes a better finish. It does not tarnish, is noncorrodible, has practically the color of platinum, and can be worked as readily. Jewelry made with it passes the common jewelers' and platinum buyers' tests.—U. S. Commerce Reports.

Sir Francis Fox told the Royal Geographical Society, of Great Britain, that one of the difficulties in planning the actual route of the Channel tunnel was to keep the tunnel well within the thickness of the gray chalk. Because of this the tunnel would not be quite a "bee line." The maximum depth of water over the tunnel would be from 160 to 180 feet, and the roof of chalk over the structure had been fixed at a minimum of 100 feet. A dip in the level of the rails would form a water lock, so that a mile of the tunnel could, in case of emergency, be filled with water. The mechanism for doing this would be controlled from Dover Castle, and the entrance and exit of both tunnels would be under the gunfire of the Dover forts. By means of the tunnel, it was stated trains would run direct from London to Paris in less than six hours, and it would be possible to go from London to Constantinople, Petrograd, and by the Serbian express to the Far East.

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# LETTERS ON PRACTICAL SUBJECTS

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# DETERMINATION OF BLANK DIAMETER FOR DRAWN METAL SHELL

In some shops, the determination of the diameter of the blank for a shell of given diameter and depth is a matter of

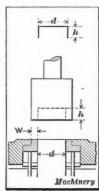


Fig. 1. Shell and Blank-holder

guess or "cut and try," although there are tables that give this information. However, all the tables that the writer has seen have been made by calculating the blank diameters for various sized shells by the formula  $D = \sqrt{d^3 + 4dh}$ , in which D is the diameter of a blank for a shell having a diameter d and a height h. It is obvious that the area of the blank must be equal to the area of a circle having a diameter d and the lateral area of the shell. Then, as the area of the circle with a diameter d is  $\frac{\pi d^2}{d}$ , the lateral

with a diameter d is  $\frac{\pi d^2}{4}$ , the lateral area is  $\pi dh$ , and the blank area is  $\frac{\pi D^2}{4}$ ;

$$rac{\pi D^2}{4} = rac{\pi d^2}{4} + \pi dh, D^2 = rac{4}{\pi} \left( rac{\pi d^2}{4} + \pi dh \right), D = \sqrt{d^2 + 4dh}.$$

But this formula does not take into consideration the "draw," or stretch, of the metal that takes place during the stamping operation. This draw is in proportion to the depth of the shell and is different for different metals. To determine the blank diameter for a zinc shell of known depth and diameter, made in one drawing operation, the chart shown in Fig. 2 will be found accurate. This chart is made with each division representing 1/64 inch. The abscissas represent the depth  $\hbar$  of the shell, Fig. 1, and the ordinates, the width W of the blankholder. For example, suppose that it is desired to find the blank diameter of a shell 2 inches in diameter and 13/16 inch deep. Now 13/16 inch is 52/64, so following the vertical line from 52 to the curve and reading the horizontal line that it intersects at that point, the width W of the blank-holder is

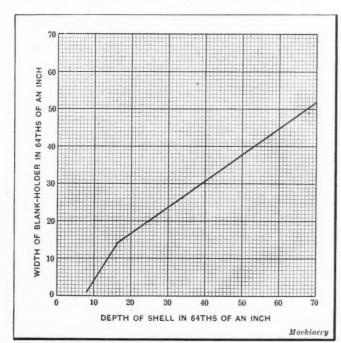


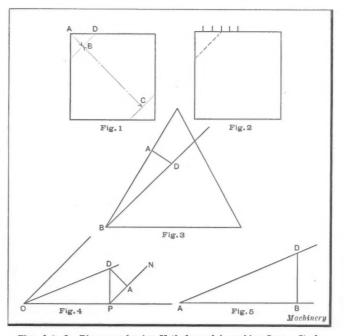
Fig. 2. Chart for determining Blank Diameter of Zinc Shell

found to be 39/64 inch.  $39/64 \times 2 = 17/32$ , which, added to the diameter 2 inches, gives a blank diameter of 37/32 inches. Wheeling, W. Va. H. S. Brady

### MAKING SQUARE STOCK OCTAGONAL

In the machine shop, if a piece of square stock is to be made octagonal, it is necessary to know either the depth of cut AB, Fig. 1, or the thickness BC of the collars between the straddlemills. To the carpenter, however, the problem presents itself in a different light. He cares for neither of these measurements, but needs AD, so that he can scribe a line to guide his saw and plane.

The methods employed to obtain this dimension are interesting. Some of the men with whom the writer has conversed



Figs. 1 to 5. Diagrams showing Methods used in making Square Stock Octagonal

say that they take AD equal to one-third the side of the square, and "don't cut quite to the line." This is undeniably an easy scheme, but about as accurate as the proverbial "blacksmith's hairbreadth," the actual value of AD being not side  $\times$  1/3, but side  $\times$  0.2929 +. Others adopt the plan, shown in Fig. 2, of dividing half the side of the square into fifths and taking the third division from the corner as the starting point for scribing the line. This is not so inaccurate a method as the first, 0.3 being, probably, near enough to 0.2929 + for woodworking purposes, except in the more exacting branches of work.

Another plan is to lay out an equilateral triangle, as in Fig. 3, then with the miter square subtract 45 degrees from it. The length of the side of the square is then laid off at BA, and the perpendicular AD erected, its length being taken for AD in Fig. 1. This, also, is only an approximation, giving side  $\times$  0.2588 +. Some workmen, however, follow a method that is theoretically exact, as it gives the true value: AD =side  $\times$  tan 22 deg., 30 min.,  $\times$  sin 45 degrees. Laying out an angle of 45 degrees with his miter square, the workman bisects it with dividers and straightedge, as in Fig. 4. Then making OP equal to the side of the square, he erects the perpendicular PD, which equals side  $\times$  tan 22 deg., 30 min., and

drawing NP at 45 degrees to PD, he draws the perpendicular AD, which he takes for AD in Fig. 1.

Various other methods of obtaining AD by construction are in use, but none, so far as the writer is aware, is as quick as the approximate schemes here given, nor as accurate as that given in Fig. 4. Obviously, the 22-degree, 30-minute angle can be used in the solution of two problems allied to this; for if, in Fig. 5, AD is made equal to the diameter of a circular piece, BD will be the side of the included regular octagon. Conversely, if BD is made equal to the side of the octagon desired, AD will be the diameter of the circumscribing circle.

New London, N. H.

GUY H. GARDNER

# BLANKING AND FOLDING PUNCHES AND DIES

The shell shown at A, Fig. 1, is made, in two operations, from 16-gage hot-rolled steel. At B, it is shown seated in position, and as it is surrounded by metal, it will not open if an unequal strain should develop. This shell is utilized as a spring seat and retainer; but it has a wider scope of usefulness by reason of its low cost of production. Under ordi-

Fig. 1. Blank and Shell formed from it

nary conditions, a shell of these dimensions drawn from a round blank will take five press operations; or, on basis of 8000 pieces a day, 40,000 operations are required, against 16,-000 operations by the folding method. In addition, five separate dies and punches are required, besides the

expense of repairs and extra help. Furthermore, uniform and unstrained walls cannot be guaranteed when dies and punches must often be polished to eliminate the excessive friction caused by the constant rubbing of metal and dies.

The shell A, Fig. 1, is made on an inclined press in one blanking and one folding, or drawing, operation. The blanking is done with the compound punch and die shown in Fig. 2. The advantage of operating this die in an inclined press is that the blanks will drop clear of the die, by gravity, and will be transferred to a receptacle by a chute fastened to the stripper at J. The blank C, Fig. 1, which is made of scrap,

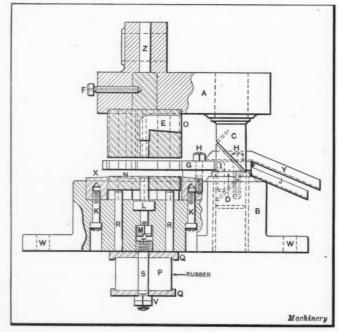


Fig. 2. Blanking Punch and Die

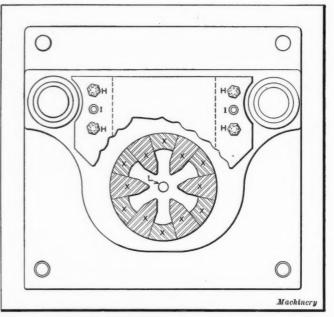


Fig. 3. Top View of Blanking Die

must be carefully developed in size and shape to meet the necessary requirements in dimensions and have all seams tight, as well as to have a uniform and concentric flange, as shown at D, which is a view of the bottom of the shell. This view shows that the hole has opened 1/32 inch in drawing, which is always taken into consideration in developing work of this nature.

Fig. 2 shows the compound blanking and perforating die, which is of the pillar type; this is easily set up, adjusted, and

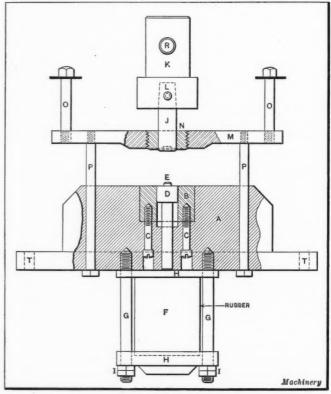


Fig. 4. Folding Punch and Die

put into operation. A is the cast-iron punch-shoe, made to fit the press ram; B is the die-shoe, also made of cast iron. These are held in alignment by guide pins C and bushings D, which are made of tool steel and are hardened and ground. The guide pins C are provided with oil channels to facilitate lubrication; the lubricant used consists of white lead and oil. The punch E is made of hardened tool steel and is held in position by a set-screw F. The hole E is provided to remove the punch E, when it becomes necessary. Punch E has a clearance hole at E0 and when operating in an inclined press dis-

angle by adjust-

ing screw D.

This screw

works in pivots,

one of which is

screwed into the

fixture and can

rotate to suit the

various angles

required. The

other pivot is

screwed into the

tailstock in the

same way, and

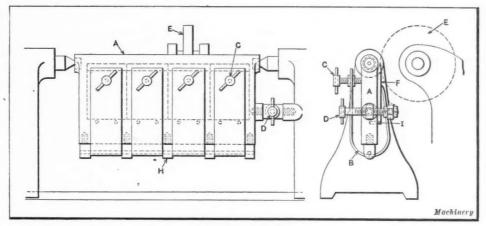
is not threaded

in the hole. The

adjusting screw

charges the slugs over the stripper G, which allows them to slide through a chute Y to the scrap receptacle. The stripper Gis held in position by screws Hand dowel-pins I.

The die X is made, in sections, of tool steel and is hardened. It is securely held in the die-shoe B by



Knife Grinding Fixture

reason of the sections being properly fitted and by screws K. Fig. 3 shows a top view of the die, which consists of twelve sections X; it also shows the clearance under the stripper to allow the blank to leave the die and enter the chute J, Fig. 2. The perforating punch L is seated in the bottom of the die and is held in position by nut M. The ejecting pad N receives its motion from a rubber buffer P, the force being transmitted through plates Q and pins R. The rubber buffer is held in position by a bolt S screwed into the die-shoe at T and tension nuts V. Holes W are provided for bolting the die to the press, making it unnecessary to use a bolster plate.

Fig. 4 shows the folding, or drawing, punch and die. The die-shoe A is made of cast iron and has a seating bushing B, held in position by screws C. Bushing B is made unusually long to increase its life; after the face is ground when the edge becomes worn, a washer is placed under the bushing to raise it to the proper height. This bushing is tapered 0.003 inch to allow the shell to be ejected more easily by the knockout pin D. Pin D has a gage pin E on its face to gage and center the blank previous to drawing it. The knockout pin receives the proper tension from a rubber buffer F, which is secured by bolts G, plate H, and adjusting nuts I.

The drawing punch J is made of carbon steel and is counterbored to clear the gage pin E. It is held in a machine-steel punch-holder K and secured by a tapered pin L. The stripper plate M is machine steel and has a hardened bushing N in the center to flatten the flange of the shell when the punch descends. This bushing also releases the shell from the punch when the latter returns to high center. The adjustment of the stripper M is made by bolts O and P. A pin R secures the punch to the ram and prevents it from pulling out under ordinary conditions. Bolt holes T are provided for securing the die to the bed of the press.

Highland Park, Mich.

ERNEST A. WALTERS

# KNIFE GRINDING FIXTURE

When their edges are to be ground, knives, bayonets or other thin stock may be set up on the centers of a Brown & Sharpe grinding machine or some similar type of grinder. The grinding fixture here shown consists of a cast-iron body A, to which spring-steel plates B are attached by pivots H. These plates are U-shaped and clamp the work F to the cast-iron body A, the tension being adjusted by screws C. The centers are provided with two hardened bushings, which engage the centers of the grinder. The fixture can be set at any desired

has two collars, one on each side of the pivot. Stops I support the work while it is being ground by wheel E, which can be adjusted backward and forward. This fixture has proved to be very rapid and efficient.

Mount Vernon, N. Y.

S W POTTS

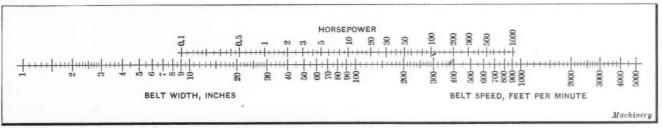
#### COATING CASTINGS WITH CHALK

Common white chalk is used extensively as a coating on castings that are to be laid out. Although its application may seem to be extremely simple, some men cannot get the chalk to stay on even if they rub a whole lump into dust and blow it off. The first time over, the chalk sticks fairly well, but the coating is not heavy enough for lines drawn upon it to be easily distinguished; after that the pulverizing begins. Rubbing in this pulverized chalk with the fingers will give a good white face, and one that will stand scribing. When a vigorous rubbing will not make the chalk stay, the old schoolboy trick of wetting it will help. Momentarily, the dampened surface looks too gray or black, but blowing on it drys it to its normal white. If a machined cast-iron surface is to be laid out, chalk should only be used when permission has been obtained, as the chalked section is sure to rust-not badly, but enough for it always to be visible unless a cut is taken over it. Middletown, N. Y. DONALD A. HAMPSON

### CHART FOR POWER TRANSMITTED BY LEATHER BELTS

The accompanying chart may be used to determine the width of a single leather belt necessary to transmit any ordinary amount of power, the horsepower that will be transmitted by a single belt running at a given speed, or the speed at which a belt must run in order to transmit a given power. For example, to determine the power that will be transmitted by a single belt 7 inches wide running at a speed of 5000 feet per minute, locate the points 7 and 5000 in the lower graduated line and then find the point midway between them. This point will be found at 44 horsepower on the upper graduated line. The dividing may be done with a rule, or a pair of dividers, or by folding a piece of paper.

Should it be necessary to transmit 44 horsepower by means of a belt traveling at a speed of 5000 feet per minute, the width of single belt required may be found by measuring the distance between 44 horsepower and 5000 and then measuring an equal distance to the left of the 44-horsepower point. In

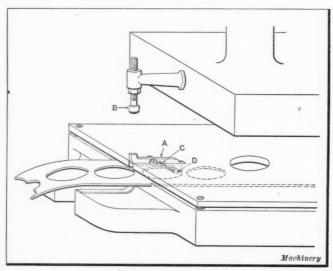


this case, it will be found that a 7-inch belt is sufficient. In a similar way, the belt speed can be determined where the belt width and horsepower are known. This chart is based on the well-known rule of thumb: A single leather belt, one inch wide, running at a speed of 800 feet per minute will transmit one horsepower.

N. G. Near

# AUTOMATIC STOP FOR BLANKING DIES

Probably one of the most valuable attachments used in connection with blanking, shearing and perforating dies, where stock is fed in by hand, is the automatic stop, and yet it is astonishing how little is known of its application. When the stock is fed in a strip or from a reel, this simple contrivance is more efficient than any kind of automatic feed and is far less expensive. The writer has observed many instances where the automatic stop could have been applied with a great saving of time. In one case the production of mica and hard rubber disks was increased from 11,000 to 100,000 a day by its use, while a shop blanking 8000 sheet-steel gear blanks increased its daily output to 58,000. The stop is an essential feature on dies made by high-class diemakers and is extensively used by firms who specialize in punch-press products, but there is no reason why firms who use the punch press as auxiliary equipment should not adopt its use wherever possible.



Automatic Stop for Blanking Dies

The illustration shows the application of this stop to a simple blanking die. Trigger A is shown locating the stock for the next blank, one of the perforations in the stock serving as a shoulder for this trigger at point D. When the ram descends, stud B trips the trigger A, lifting its point Duntil it clears the stock. When the point clears the top of the flat stock, the spring C pulls the trigger forward; and when the stock is fed farther, the spring pulls the trigger down into the next perforation, which again forms the shoulder for the point. One end of spring C is fastened to trigger A and the other to the bottom of the stripper plate. There is a slot in the trigger for the fulcrum pin, which allows the double motion, forward and down. This entire operation is repeated at each stroke, so that the press may be run at full speed and the stock fed through without having to trip the press each time. The trigger is shown mounted on two lugs on top of the stripper plate, but it may be set in the die-block beside the stock, reaching in over the stock. While only a simple case is described here, the application of the automatic stop will not at any time be found complicated. -

Cincinnati, Ohio

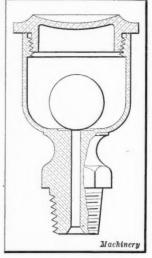
JOSEPH AHLERS, JR.

# IMPROVED FORM OF OIL-CUP

On a number of small machines an ordinary brass oil-cup with a top that is screwed on is used. Waste soaked in oil or boiled in vaseline before soaking is then put in it. If the spindle revolves very rapidly a vacuum is formed in the cup, causing a thread of the waste to be drawn into the bearing.

On most of the smaller grinders and buffing lathes, the bearings are of babbitt, and so are quickly cut enough to allow dirt to gather and in time to wear the spindle, thus spoiling the efficiency of the entire machine.

This trouble is eliminated in the oil-cup shown in the accompanying illustration. A basin about the diameter of the ball used is milled in the brass cup. Then the steady, positive vibration of a grinding or a buffing machine causes the ball to rock on the oil-hole, thus allowing the oil to drop, as in a sight-feed oiler. The ball also shuts off the supply of oil when the machine is not running. The fact that more oil can be put in at a



Improved Form of Oil-cup

time means that the machine will run longer without the trouble of oiling and an operator can readily tell if oil is needed by removing the cap. The steel ball used should be six times the diameter of the hole in the oil-cup.

New Britain, Conn.

JOHN J. MCGAULEY

#### REDUCING GLARE OF ELECTRIC BULB

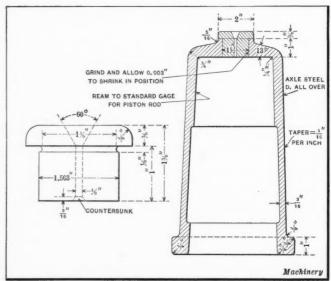
Coating an electric-light bulb with Prussian blue reduces the glare and gives a light that does not tire the eyes. The pigment should be rubbed lengthwise on the bulb, but not on the bottom, of course.

Milwaukee, Wis.

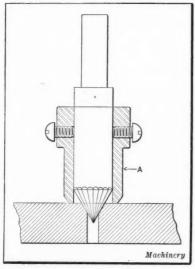
FRED FRUHNER

#### CENTERING SLEEVE FOR PISTON-ROD

The device shown in the accompanying illustration was designed principally for use on piston-rods that have to be trued up in a lathe or grinding machine, but the centers of which are so battered that they will not run anywhere nearly true. So much material must be cut or ground off a piston-rod in this condition that the rod soon gets down to the limit size, and instead of having a long and useful life it is wasted. For use under these conditions, a sleeve is made to fit the end of the piston-rod. In one end of this a small, hardened, tool-steel plug is shrunk. This plug has a 1/8-inch hole and is countersunk 60 degrees to suit the lathe center. At the other end, the sleeve is made a little larger in section, so that it can be knocked off the piston-rod with a soft hammer, when the rod has been turned or ground, without being injured. This sleeve can be modified, of course, to suit other tapered or straight pieces with poor centers. M. K.



Sleeve for truing up Piston-rods with Damaged Centers



Countersink with Sleeve attached for obtaining Accurate Depths

### COUNTERSINK SLEEVE

The sleeve here shown enables the user to obtain accurate depths in countersinking; where a large quantity of work is to be machined to the same depth, it saves time and produces satisfactory results. The sleeve A is made to fit the countersink and may be adjusted to suit the piece being worked on. The tool is fed down until the sleeve touches the surface of the work, so that all the pieces are countersunk to the same

depth. It is difficult to countersink all the pieces alike without employing some method of this kind, especially if some of the pieces are thicker than others, but this is successfully accomplished with the tool described.

Ambridge, Pa.

AUGUST J. LEJEUNE

#### FALSE GRAPHIC REPRESENTATION

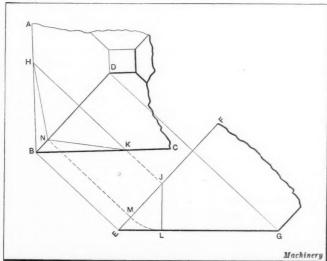
I find Babson's "Graphic Representations of Volumes and Weights" to be misleading. For eight times the quantity, he shows a bottle, bag, or barrel eight times as high and wide; whereas it should be only twice the linear dimensions, because  $8=2\times2\times2$ . This method was carried to the height of ridiculousness in the war statistics of the National Security League and American Defense Society, where armies were represented by soldiers of height in proportion to number. Nothing is so simple and convincing as ordinary heavy straight lines to scale.

New York City

ROBERT GRIMSHAW

# FINDING TRUE ANGLE OF VALLEY PLATES FOR STEEL HOPPERS

The article in the May number of Machinery, "Laying Out a Hopper Miter Joint," brings to mind a method the writer has used to find the true angle of valley plates used on steel hoppers. It is a graphic method and may be used for any size or shape of hopper. Let ABCD represent the plan of the hopper, while EFG is the elevation; BD is the intersection line of the sides. Draw HK perpendicular to BD; line HK is the edge of an imaginary plane passed perpendicular to the intersection line and is shown in the elevation by a line JL drawn



Graphic Method of finding True Angle of Valley Plates for Steel Hoppers

perpendicular to EG. Revolve JL about the point J to the position JM and project the point M back to the plan to N. Then HNK is the true angle of intersection of the two sides of the hopper, since it is the trace on a perpendicular plane of the two sides after the plane is revolved into the plane of the drawing.

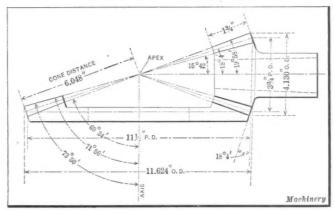
St. Joseph, Mo.

L. M. HAMLET

#### STUB-TOOTH BEVEL GEARING

Stub-tooth bevel gears are now being used extensively by some automobile manufacturers instead of the standard-tooth bevel gears. By using a 20-degree pressure angle and shortening the height of the gear tooth, a stronger gear is obtained, which requires no under-cutting but which has better rolling contact. This type of tooth is therefore recommended for machinery requiring gearing that will withstand severe stresses. The method of calculating the parts of this gear is best shown by an example.

Let it be required to make a pair of stub-tooth bevel gears of 4/5 diametral pitch, with 46 teeth in the gear, 15 teeth in the pinion, and a 20-degree pressure angle. As the tangent of the pitch angle of the pinion is  $15 \div 46 = 0.32609$ , the angle is 18 degrees, 4 minutes. The pitch angle of the gear is then 90 degrees — 18 degrees, 4 minutes = 71 degrees, 56 minutes.



Stub-tooth Bevel Gears of Forty-six and Fifteen Teeth

The pitch diameter of the pinion is  $15 \div 4 = 3.75$  inches, and of the gear,  $46 \div 4 = 11.5$  inches. The addendum of both the gear and the pinion is 0.2 inch. The cone distance is one-half the pitch diameter of the gear divided by the sine of the pitch angle of the gear, or  $11.5 \div 2 \div 0.9507 = 6.048$  inches. Then, dividing the addendum, 0.2 inch, by the cone distance, 6.048 inches, gives the tangent of the increment angle for both the gear and the pinion; or,  $0.2 \div 6.048 = 0.033068$ . This angle is therefore 1 degree, 54 minutes. The face angle of the gear is 71 degrees, 56 minutes  $\div 1$  degree, 54 minutes = 73 degrees, 50 minutes; and the face angle of the pinion is 18 degrees, 4 minutes  $\div 1$  degree, 54 minutes = 19 degrees, 58 minutes.

The dedendum for both the gear and the pinion is 0.25 inch. The tangent of the dedendum angle or the angle of decrement for both gears is therefore  $0.25 \div 6.048 = 0.04133$ ; which is the tangent of 2 degrees, 22 minutes. The cutting angle of the gear is then 71 degrees, 56 minutes - 2 degrees, 22 minutes = 69 degrees, 34 minutes; and of the pinion, 18 degrees, 4 min-- 2 degrees, 22 minutes = 15 degrees, 42 minutes. The diameter increment of the gear is the product of twice the addendum and the cosine of the pitch angle, or 2 imes 0.2 imes0.31012 = 0.124 inch. Adding this to the pitch diameter of the gear gives the outside diameter of the gear, or 11.5 inches + 0.124 inch = 11.624 inches. The diameter increment of the pinion is the product of twice the addendum and the cosine of the pitch angle, or  $2 \times 0.2 \times 0.9507 = 0.38$ . Adding this to the pitch diameter of the pinion gives the outside diameter, or 3.75 inches + 0.38 inch = 4.13 inches. As the addendum is 0.2 inch and the dedendum is 0.25 inch, the total depth of the gear tooth is 0.45 inch. The thickness of the tooth is 0.3926 inch.

Brooklyn, N. Y.

EDWARD J. RANTSCH



Fig. 1. Piece formed by Die shown in Fig. 2

# DIE FOR PRODUCING SMALL STEEL PIECES IN ONE OPERATION

Fig. 1 shows a small piece made from 1/32-inch steel, and Fig. 2 shows the die for producing it in one operation. Similar dies can be used for work of this kind, where great accuracy is not required, where the metal is light, and where the bending point is reduced, so

that it is not necessary for the forming punch to bottom the piece against the die to form the bend. As the part is pushed through the die out of the way, the operation is much faster than it would be if the part were left on the die to be slid or knocked off.

Fig. 2 shows the plan of the die without the stripper and the front view of the punch and die. The hole is pierced at A and the piece formed, cut off, and dropped through at B. D and E are the cutting edges and F the forming edge, which is 3/16 inch higher than the cutting edges. The end of stop C is the same size and shape as the cutting-off punch, so that the end of the strip, after being cut, centers against it. The stripper G is 1/4 inch thick and extends 3/8 inch above the die, leaving 3/16 inch under it, over the forming edge. The cutting-off and

bend is completed before the piece is cut off. The forming edge is under-cut so that the piece is free to drop away from the punch and will not follow it back.

Plymouth, Mich.

W. B. GREENLEAF

### A SIMPLE JIG

The toolmaker in the jobbing shop meets many difficulties; sometimes he is called upon to be a designer, without making elaborate details. The other day it was necessary to make three brass plates containing 280 steel pins, 3/32 inch in diameter, 1/2 inch apart. For one plate the holes for the pins were laid out by the aid of a milling machine, as accuracy was essential. But this method was too slow and not accurate enough. So four rows of holes were laid out on a piece of steel 3/16 by 6 by 3 inches, which was used as a jig.

As the brass plates were milled up square, it was easy to clamp the jig for the first four rows of holes. Then, after these holes were drilled, the jig was unclamped and moved along on the plate, being located by pins that passed through the jig into two of the holes drilled in the brass plate. This method was continued until all the holes were drilled. The plate laid out by the milling machine was not nearly so true as those laid out by means of the jig; this may be due to the fact that when milling machines are used much the screws

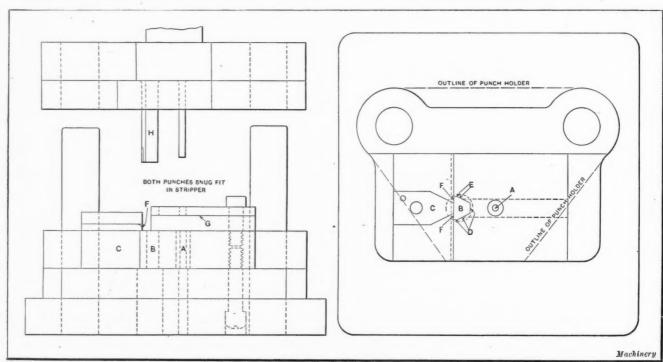


Fig. 2. Die for forming Small Steel Piece shown in Fig. 1

forming punch H is made the full size of the hole, except at the two corners where clearance is allowed for the two prongs. This leaves a space between the prongs for it to slide against the forming edge, to back up the cut. The guide pins are of one-inch drill rod; they are not hardened and are left with the original finish. They are a drive fit in the shoe and a nice sliding fit in the punch-holder, and have no bushings. This construction will outlast two or three dies and has been used for the last five years.

In operation, the strip is fed directly against the stop C; this gives a blank without prongs or hole. The second blank also lacks the hole, but after this blank a complete piece is produced at each stroke. If this material is bought in coils, the loss of two pieces at the beginning of each coil does not amount to anything. The press may be run continuously to the end of the coil, for the stop is positive and cannot be run over and the part drops through without scrap. As the punches rise after the cut, they carry the strip against the stripper, so that it is pushed forward on that level, with the prongs at the end resting on the forming edge. On the downward stroke, the punch bends the prongs while the blank is still part of the strip, which gives the prongs the necessary support, for the

wear and the graduated collars are not absolutely accurate.

New Haven, Conn.

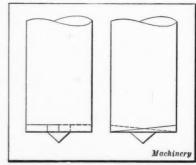
ERIC LEE

### HEAVY-DUTY PUNCH

If a heavy-duty punch is ground off as illustrated, it will take less power to operate, start more easily, and shear a smoother hole than it will if ground as shown in the April number of MACHINERY.

I have used punches ground as illustrated up to two inches in diameter on material two inches thick, and have found that if the bevel is not greater than 3/32 inch in two inches, the punches stand up to the work and give better service.

C. G. WILLIAMS Miles City, Mont.



Heavy-duty Punch

### TO PREVENT BREAKING VULCANITE-MOUNTED MAGNIFYING GLASSES

A simple and effective method of preventing the breaking of the ferrule of vulcanite-mounted magnifying glasses consists of placing several rubber bands, about ¼-inch wide, around the ferrule at the glass end, allowing the rubber to project slightly beyond the ferrule. When dropped, the glass end, which is the heavier, will almost always strike the floor first, and if not protected, the vulcanite, being very thin at this end, will chip off and allow the glass to fall out. These bands act as a cushion and protect the vulcanite.

Providence, R. I.

R. C. SCHOLZ

# SAFETY ATTACHMENT FOR LADDERS

Several accidents occurred in the plant in which the writer is employed to the men who inspected, repaired, and oiled the lineshafting, before it was noticed that these were due chiefly

to the fact that the ladders slipped when the men leaned too far to one side to reach a bearing, etc. Therefore, to prevent the ladder slipping along the shaft on which it was resting, rubber strips were tacked along both sides of the ladder, as indicated by the heavy lines in the accompanying illustration. This device worked out very satisfactorily, and no further accidents have been due to this source. Although not shown, the base of the ladder was also equipped with iron claws to prevent slippage at that point.

Philadelphia, Pa.

W. A. LAILER

# HARDENING KINK

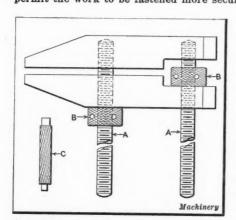
Toolmakers and diemakers often experience difficulty from dies expanding during hardening. If, when a die is put in the furnace, it is placed top face down on a firebrick slab, it will get more heat than if placed bottom face down, which is the usual method. The hole will then contract, instead of expanding, and will allow about 0.002 inch for stoning. When too much metal has been filed from the hole in the die, there is more chance of the templet fitting if the die is hardened this way.

Long Island City, N. Y.

E. KERN

# TOOLMAKER'S CLAMP

The clamp shown in the accompanying illustration is one of the most useful to be found. As the screws A are headless and pass through only one side, it is possible to get to the bottom working surface. The nuts B permit the work to be fastened more securely than the screws

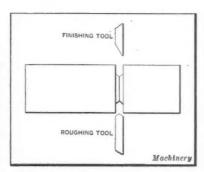


Handy Parallel Clamp for Toolmakers and Diemakers

in the ordinary form of clamp; the nuts are tightened by means of the pin C. This clamp is made of coldrolled steel and is casehardened: the nuts are made of carbon steel and are drawn to a dark brown, and the screws are made of steel (Stubs gage) and tempered in oil. AUGUST J. LEJEUNE Ambridge, Pa.

CUTTING-OFF TOOLS

The accompanying illustration shows two cutting-off tools mounted on one cross-slide. With a roughing tool shaped as shown, greater speed and better work is insured, and a minimum of power is required. This tool is self-clearing on the sides



Roughing and Finishing Cutting-off Tools

and guides straight, an important feature when cutting off thin disks of large diameter. When the roughing tool has been fed to a certain point, it is backed off and the finishing tool on the opposite side is brought up to finish the cut. The small amount of work done by the finishing tool makes it

possible for this tool to be ground at an extreme angle, thereby making a clean cut.

Oak Park, Ill.

P. Bertles

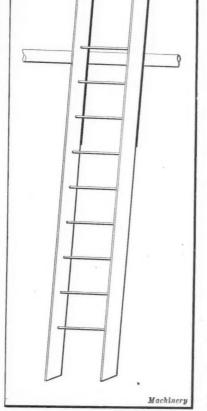
# GRINDING EDGE TOOLS ON EMERY WHEEL

The article entitled "Wheel Dressing" in the June number of Machinery recalls an incident that shows what the average woodworker thinks of the emery wheel for grinding edge tools. The writer was assisting the boss patternmaker to make a large pattern, which was being turned in the lathe, when it became necessary to grind the wood-turning chisel. This was made from a flat file 5/16 by 11/2 inch, and considerable stock had to be removed to put the chisel in good working condition. As the shop grindstone was worn down pretty close to the hub, the writer began to grind the chisel on the emery wheel, but was soon stopped by the boss, who called him down for committing such an unmechanical act.

In that particular shop the grinding of an edge tool on an emery wheel might be considered unmechanical, but the writer did it long before he worked there and has doffe it ever since, and his edge tools are in good condition and in use every day. A great many first-class mechanics in the wood-working lines have an idea that the emery wheel has a bad effect on edge tools. Perhaps experiences have shown this to be

true, but if you inquire from these men, "Do you keep the wheel in good cutting condition?" their answer is in a great many instances, "I never bother about that; an emery wheel requires no attention."

Wood-turning tools become dull very quickly; they are made from heavy stock, and grinding, even on a good grindstone, is slow and tedious. In a great many shops, the grindstone is located in a dark corner some distance from the wood-turning lathes, and during the process of turning a great many patterns, several trips to the stone must be made. The writer grinds his turning tools on an emery wheel, which he has mounted on a wooden faceplate that fits on either end of the lathe spindle. When turning between centers or on a faceplate at the front end of the lathe, the emery wheel is mounted at the back end of the spindle, and when turning at the back end of the spindle, the emery wheel is placed at the front. For the small lathe, a small wheel is mounted on a wooden center made like the regular lathe center and fitted to the hole in the spindle. By this plan, the turning tools are easily and quickly ground without leaving the lathe. All inside-ground gouges are ground on the small wheel, as it is but a moment's



Ladder with Rubber Strips to prevent Slipping

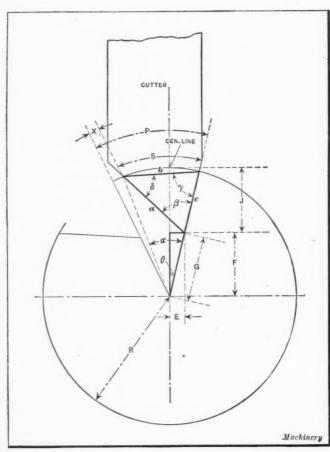


Diagram for finding Set-over, Depth, etc., of Cutter

work, with the aid of the dresser, to form the wheel to the curve of the gouge. The wheels and the dresser are part of the writer's turning-tool kit; they are his own property and he keeps them in good cutting condition. A clean wheel will do good and fast work; a dirty, glazed, neglected wheel will not grind burrs off rough castings, to say nothing of edge tools.

Kenosha, Wis.

M. E. Duggan

# SETTING AN ANGULAR CUTTER FOR MILLING SPIRALS

The writer recently had a number of spiral end-mills to flute, and not being able to find a suitable formula for obtaining the necessary set-over, full depth, etc., used the solution given herewith. The outside diameter, number of teeth, and width of land are the dimensions furnished. In this solution it is assumed that the vertex of the cutter angles is a point, N= number of teeth; X= land; R= radius. The cutter  $2R\pi$ 

angles were 53 and 12 degrees. Arc 
$$P=\frac{2R\pi}{N}$$
; arc  $S=P-X$ ; 360 degrees — 180 degrees —  $\alpha$ 

$$\alpha = \frac{\frac{360 \text{ degrees}}{2}}{\frac{2R\pi}{8}}; \ \gamma = \frac{\frac{180 \text{ degrees} - \alpha}{2}}{2}; \ \beta = 65 \text{ degrees}; \ \delta = 180$$

degrees — 
$$(\gamma + \beta)$$
;  $b = 2R \times \sin \frac{\alpha}{-}$ ;  $c = \frac{b \times \sin \delta}{\sin \beta}$ ;  $G = R - c$ ;  $\theta = 12$  degrees;  $E = G \times \sin \theta = \text{set-over}$ ;  $F = G \times \cos \theta$ ;  $J = R - F = \text{full depth}$ .

# LIGHTING STAIRCASES

Denver, Colo.

Recently, the writer called attention, in a certain factory, to the necessity of having electric lights at the foot of each staircase. Light at the top of the flight casts a shadow on each step and makes the stairs dangerous. He also found a swinging door opening outward at the foot of one of the stairs, tending to block the corner on the turning. Such a door should not be used as a fire

exit, unless it can be locked back when open, and it is a poor arrangement in any case.

New York City

ROBERT GRIMSHAW

# DOUBLE KEYWAY MILLING FIXTURE

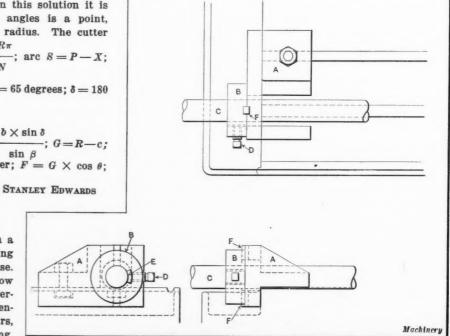
The accompanying illustration shows an indexing fixture that was designed for milling opposite keyways for movable saws in long saw arbors on wood-working machinery. The keyways are cut in opposite sides in order to balance the shafts, as they run at high speed. The fixture consists of a cast-iron bracket A and a steel collar B which is fastened to the shaft C to be milled, by a set-screw D that bears on a shoe E. The bracket A extends down over the end of the platen of the milling machine and is held in place by a bolt in the T-slot next to that in which the work is laid. The collar B thus forms a stop, bearing against the bracket and the end of the platen to resist the action of the milling cutter. The collar is slotted to receive two keys F, which are fastened in slots in the body A of the fixture: the slots in the collar are made central with the hole. No key is used to locate the fixture in relation to the T-slots, as this would entail locating the key an exact distance from the indexing keys, and this would be affected by any variation in the chamfer on the edges of the T-slot where the work is located.

In operation, the work and fixture are put on the milling-machine table, and the holding-down bolt is tightened slightly by hand; the hole for this bolt is 1/16 inch larger than the bolt. Collar B is then set up solidly on the shaft in the proper position lengthwise, and the shaft is strapped down over the T-slot with U-straps in the customary manner. The holding-down bolt for the fixture is now tightened, as the work has located it in the correct position. When the slot has been milled, the U-straps are loosened, the shaft is drawn back until collar B clears keys F (without loosening the collar), the shaft is given a half turn, and the collar is slipped over the keys again. The straps are then tightened and the second slot is milled.

This fixture has done very satisfactory work, indexing the slots perfectly without the necessity of putting the shafts on index centers, which in most cases would be impossible owing to the length of the shafts handled. The accuracy of the fixture is dependent wholly on the accuracy with which the slot in collar B is centered; this can easily be done very accurately. The fixture is so proportioned as to handle shafts from 1 7/16 to 2 3/16 inches in diameter, a collar being used for each size of shaft that is milled.

Orange, Mass.

W. R. STULTS



Indexing Fixture for milling Double Keyways in Shafts

# HOW AND WHY

QUESTIONS ON PRACTICAL SUBJECTS OF GENERAL INTEREST

## HOBS AND MULTI-CUTTERS

A. L. K.—We have had a difference of opinion over the meaning of the term "hob." What is the correct definition?

A.—The term hob, when applied to a tool for cutting threads or gear teeth, means a cutter having teeth in a helical path like a tap. The term hob is sometimes erroneously applied to multi-cutters used in thread milling machines for cutting threads. These cutters do not have the teeth in a helix, but in parallel circumferential rows.

# MARKING COUNTERSINK ANGLES ON DRAWINGS

H. G. F.—We have had a lengthy discussion on the proper method of marking the angle of countersinks on a drawing. I made a drawing which indicated three holes for screws with countersink heads, and marked them "25/64 drill, 76 degrees countersink." When the pieces were made and delivered, it was found that the included angle of the countersink was 104 degrees, that is, 180 degrees minus 76 degrees. Will you kindly tell us what is regarded as the proper method of marking countersink angles?

A.—The angle of countersink is always the included angle and there is no practice warranting anyone using the supplement angle instead. The angles of twist drills, countersinks, and similar tools, are always expressed as the included angle or half the included angle.

# WHY DIDN'T IT EXPLODE?

W. S. R.—A small can of evaporated milk—not the thickened condensed milk, but the 50 per cent reduction kind—was left in a pot of water boiling furiously for twenty minutes after it came to a boil from 96 degrees F. The can was absolutely tight and there was no apparent escape of steam. Early in the boiling the can ends bulged, indicating internal pressure, but that was all. Why didn't it explode?

A.—The probability is that the ends bulged sufficiently to crack the soldering at some point and make a minute opening through which sufficient steam escaped to prevent explosion. However, there is another side to the matter, and that is the slowness of heat transfer under certain conditions. It may be that even after having been in boiling water for twenty minutes, the whole mass of milk had not yet reached boiling temperature. The question is submitted to the readers.

## GRINDING TAPER PLUGS IN BRASS VALVES

F. E. R.—What is an approved method of grinding in the taper plugs of brass plug cocks? I have had trouble in making a tight job, using fine ground glass and flour emery as abrasives.

A.—The grinding in of brass taper plugs in valve bodies is a job requiring considerable care and skill to insure water-tightness. Emery should never be used, as it tends to cut circumferential grooves, and the abrasive action continues after the valve is put in use, due to minute particles of emery that are left embedded in the soft brass. Valve manufacturers use fine burnt foundry sand mixed with machine oil to form a paste abrasive for grinding plug valves. Hard soap is rubbed on the plug at short intervals to furnish the necessary lubrication. The action when grinding in a plug valve should be an oscillating motion, and the plug should be pulled out of the valve body frequently to distribute the abrasive evenly and to prevent cutting. The fine burnt sand and hard soap give good results; when the grinding is finished, the surface may be easily cleaned and no cutting will take place afterward.

## CASTING LAMP BASES AND COFFIN HANDLES WITHOUT CORES

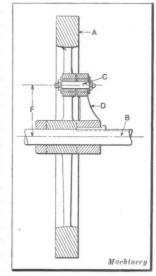
H. T. S.—Will you tell me how fancy lamp bases, coffin handles and other articles requiring a high finish are cast hollow without using cores?

-Fancy lamp bases are cast in iron molds by pouring in a comparatively small amount of alloy having a low melting point and turning the mold about while a thin shelf of the metal hardens. When the desired thickness has hardened, the workman tilts the mold so that the molten metal runs out, leaving a thin shell of metal in the mold, which is then removed. Essentially the same process is employed in casting coffin handles. The mold is provided with a gooseneck into which the britannia metal is poured. The mold is allowed to stand for a few seconds until the metal hardens and then turned over and the molten metal poured out, leaving the center hollow. The workman can make a thick or thin shell by simply varying the time that the metal is allowed to stand in the mold. Considerable skill is required to make a shell of uniform thickness, especially thin shells. The chief art in this trade is in securing uniform thickness of the shell and using the minimum of metal.

#### RESISTANCE OF SHEAR PIN

P. G. P.—We have fitted a flywheel with the safety device shown in the illustration. A one-inch square steel pin C is held between steel bushings, one bushing being held in the flywheel arm and the other in a spider D keyed to the shaft B. The flywheel A is free to revolve around the shaft, in case an overload should shear pin C. We have assumed that it would require 60,000 pounds to shear a steel pin one inch square and also that the pin would be severed when sheared about one-third its thickness. The question is, does the distance F affect the resistance of the shear pin? It seems to me that it must remain the same wherever placed.

A .- The position of the shear pin positively affects its effective shearing resistance. If it is located at the hub, its resistance to the action of the flywheel will be much less effective than if it is located in the rim. If the shear pin is located 20 inches from the shaft center, its effective resistance to check the flywheel will be twice that if placed only 10 inches from the center. The principle is exactly the same as found in a pair of shears. If a thick wire is to be sheared, you place it as near the pivot or hinge of the shears as possible in order to get the most effective leverage. The farther the wire is placed from the pivot, the harder it is to force the jaws through it. The wire cuts no harder, however, in one



Flywheel loosely mounted on Shaft and driven by Shear-pin

position than in the other, but the effective leverage is lessened as the wire is moved away from the pivot.

#### MELTING COPPER IN AN IRON CUPOLA

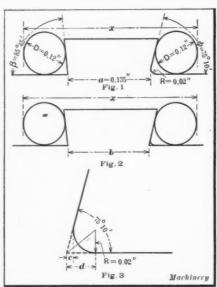
E. P. F. & N. Co.—We have a small brass furnace and an iron cupola in our foundry and have to make three bronze castings weighing one ton each. We understand that the copper can be melted in the iron cupola and the tin, zinc and lead required for making brass or bronze mixtures may be melted in the brass furnace and heated in the cupola as the copper runs from the iron cupola. Will you please advise?

A.—Large quantities of copper for making bronze castings may be melted in an iron cupola by using a reduced tuyere area and a blast pressure of 8 to 10 ounces. The tin and other metals used for making the bronze should be melted in an ordinary crucible brass furnace and poured into a large ladle into which the copper is tapped from the cupola. Care

should be exercised in melting the copper to use a fuel having a low sulphur content. After tapping the cupola, the melted copper should be covered with lump charcoal to prevent oxidation. Heavy brass castings may also be made by melting in an iron cupola. The practice of Dibert, Bancroft & Ross Co., Ltd., of New Orleans, Pa., in melting brass in the cupola, is to charge with 90 per cent heavy red brass and 10 per cent pure copper. A very light blast is used while melting. The losses from oxidation in the foregoing mixture vary according to the quality of brass with which the cupola is charged, but are rarely more than 5 per cent, affecting mostly the zinc and tin. To secure the proportions desired in the casting, zinc and tin, previously melted in a brass furnace, are added to the ladle after tapping from the cupola. The company has not thought it necessary to use deoxidizers in the ladle. although they are regarded as beneficial in some cases.

### MEASURING DOVETAIL SLIDES

S. C. B.—Please show me how to calculate the distance over the two wires used in measuring the dovetailed angles shown in Fig. 1, the dimensions of which are as given.



Figs. 1 to 3. Diagrams used for finding Distance x

A.-To calculate the distance x, it is first necessary to know the distance b, Fig. 2, between the sharp corners of the angles; therefore, the distance c, Fig. 3, must be found. This distance may be obtained by first finding the distance d from the formula

$$d = R \cot \frac{1}{2}$$
; then  $c = d - R$ . This value of  $c$  must be subtracted from the length  $a$  to give the distance  $b$ . The dis-

tance x is then found by the formula  $x = D + \left( \frac{1}{2}D \times \cot \frac{r}{2} \right)$ 

+ b. Applying these formulas to the pres-

75 deg., 10 min. ent case,  $d = 0.02 \times \cot$ = 0.02598 inch; so 2

c = d - R = 0.02598 - 0.02 = 0.00598 inch, and b = a - c= 0.135 - 0.00598 = 0.12902 inch. Then x = 0.12 + 0.06 $\times$  1.0774 + 0.06  $\times$  1.2993 + 0.12902 = 0.3916 inch.

# MEASURING FORCE OF A HAMMER BLOW

C. C. B .- To test the force of a blow in hammers, we take a round lead plug, one inch in diameter and one inch high, and strike it one blow with the hammer; then we take a duplicate plug, put it in a Riehle testing machine, and press this plug to the thickness of the plug that has been struck. Is the pressure indicated by the machine equal to the force of the blow? Some people say it is, while others take the opposite view; which are right?

A .- The fundamental formula for ascertaining the force of a blow is ft = mv, in which f = force of blow, t = time required to bring body to rest, m = mass of body, and v = velocity of body at instant of striking. It is seldom possible to measure t and it is usually difficult to ascertain v; consequently it is customary to determine the force of a blow, with more or less accuracy, by employing the principle of work. In the case of a pile driver, this method gives fairly satisfactory results, the formula being, theoretically, wh = fs, in which w = weight of falling body, h = height of fall, f = force

of blow = resistance offered by pile, and s = distance pile is driven by blow; the weight w and the force f are in pounds and h and s are in feet. In the present case, the hammer is assisted by an additional force, and if this is known or can be found, it must be added to w. Even then, the result will not be exact, because every body, even lead, has a certain amount of elasticity and will not entirely retain the shape it had at the instant of greatest compression. Solving the foregoing

wh-. If it is assumed that the work done formula for f, f = -

in the testing machine is equal to wh, all that is necessary is to multiply and divide the pressure p recorded by the machine by s (measured in feet), and the result (f = p) will be a fair approximation to the force of the blow struck by the hammer. But this assumption implies that the pressure is uniform from the instant that the plug begins to be compressed until the required thickness is reached, which is by no means the case. It is also probable that a greater force will be required in the machine than the almost instantaneous force exerted by the hammer; however, it is reasonable to assume that your method is not far wrong. J. J.

# CONCERNING THE DIAMETER OF A SHAFT

B. C. L.—In an article showing how to calculate the diameter of a steel shaft, I find the statement: "If the diameter eter of a steel shaft. I find the statement: is less than 13.6 inches, use Formula (1); but if it is greater than 13.6 inches, use Formula (2)." The formulas are as follows, in which d is the diameter, in inches, H is the horse-power transmitted, and N is number of revolutions per min-

ute: 
$$d = 4.7 \sqrt[4]{\frac{H}{N}}$$
 (1), and  $d = 3.3 \sqrt[3]{\frac{H}{N}}$  (2). Why are the

formulas so different, and how is the number 13.6 obtained? A.—When a shaft transmits power, it is subjected to a twisting stress, and the resulting deflection is measured by the socalled "angle of twist." It is not desirable to have this angle

exceed a certain limit, and when it is taken into account, Formula (1) is derived. But when the angle of twist is neglected and only the strength of the shaft is considered. Formula (2) is obtained. It is evident that there must be one diameter for which both formulas will give the same result; to find it, proceed as follows: Placing the right-hand members of the

two equations equal to each other, 
$$4.7 \left(\frac{H}{N}\right)^{\frac{1}{4}} = 3.3 \left(\frac{H}{N}\right)^{\frac{1}{3}}$$

or 
$$4.7 \left(\frac{H}{N}\right)^{\frac{3}{12}} = 3.3 \left(\frac{H}{N}\right)^{\frac{3}{12}}$$
. From the last expression, objectively

tain by division 
$$\left(\frac{H}{N}\right)^{\frac{1}{12}}=\frac{4.7}{3.3}$$
. Raising both members to the 12th power,  $\frac{H}{N}=\left(\frac{4.7}{3.3}\right)^{\frac{12}{2}}=$  69.675, using a five-place

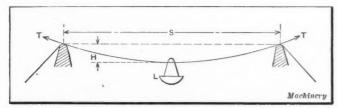
the 12th power, 
$$\frac{H}{N}=\left(\frac{4.7}{3.3}\right)^{12}=$$
 69.675, using a five-place table of logarithms. Substituting this value of  $\frac{H}{}$  in either

of the two formulas, the value of d is found to be 13.579, say 13.6. In practice, that formula should be used which gives the larger value for d. If the diameter is less than 13.6, Formula (1) will give the larger value; but if the diameter is greater than 13.6, Formula (2) will give the larger value. In the case of engine crankshafts, neither formula will give very good results, because the heavy loads induce bending stresses, which must also be considered, the resulting formula being somewhat complicated. J. J.

# STRENGTH OF ROPE FOR A CABLE BRIDGE

W. H. D.—We wish to put a cable bridge across a small stream and would like to know what size steel-wire rope, nineteen wires to the strand, will be necessary. The span is 85 feet, and the sag H must not exceed 5 feet; the greatest weight of the car and contents is 2500 pounds.

A .- As may be supposed, it is not possible to derive a formula that will give exact results; that is, results that will be closer than, at the most, two significant figures. The ten-



Determination of Strength of Rope for a Cable Bridge

sion T in the rope may be found quite accurately by means of the following formula:

$$T = L\left(\frac{8}{4H} + \frac{4HL}{8^2W + 28L}\right) + \frac{8^2W}{8H} + HW$$

in which S = span, in feet;

H = sag, in feet;

L =maximum weight of car and contents, in pounds; W = weight of rope, in pounds, per foot of length.

In order to find a value for T, it is necessary first to determine the value of W. When the values of S and L are comparatively large, as in this case, and steel rope is used, W exerts but a small effect on T; hence, making W = 0, a value for T is found, by means of which the size of the rope can be determined, approximately. In the present case,

$$T = 2500 \times \left(\frac{85}{4 \times 5} + \frac{4 \times 5 \times 2500}{2 \times 85 \times 2500}\right) = 10,900$$
 pounds, ap-

It is necessary to allow a reasonable factor proximately. of safety, the value of which will depend upon how frequently the cable is used and how often the maximum load is carried; it may be as low as 3 or as high as 6. Assuming that it is 4.5, the rope should have a breaking strength of  $10,900 \times 4.5 = 49,050$  pounds, say 25 tons. A cast-steel wire rope 1/8 inch in diameter has a breaking strength of 25 tons and weighs 1.2 pound per foot. Substituting this value for W in the complete formula for T,

$$\begin{split} T = 2500 \times \left(\frac{85}{4 \times 5} + \frac{4 \times 5 \times 2500}{85^2 \times 1.2 + 2 \times 85 \times 2500}\right) + \frac{85^2 \times 1.2}{8 \times 5} \\ + 5 \times 1.2 &= 11{,}135 \text{ pounds. Multiplying by the factor of safety, } 11{,}135 \times 4.5 &= 50{,}107 \text{ pounds, or } 25 \text{ tons, very nearly.} \\ \text{Hence a } \%{-}\text{inch rope will be large enough; but if the cable} \end{split}$$

bridge is to be subjected to heavy usage, it might be well to

# TRIGONOMETRIC FUNCTIONS FOR ANY ANGLE

J. P. C .- I should appreciate a rule that is easily remembered for finding the trigonometric functions for angles greater than 90 degrees, using an ordinary table.

A.—Let x be any angle less than 90 degrees; then any other angle can be expressed as  $n \times 90$  degrees + x, n being an integer. For example, 286 degrees, 42 minutes may be written  $3 \times 90$  degrees + 16 degrees, 42 minutes; 563 degrees, 19 minutes =  $6 \times 90$  degrees + 23 degrees, 19 minutes; and 52 degrees, 24 minutes =  $0 \times 90$  degrees + 52 degrees, 24 minutes. As shown in Fig. 1, angles are assumed to increase by the radius starting from OA and moving counter-clockwise about the circle; hence AOM = x, AON = 90 degrees + x, AOP = $2 \times 90$  degrees + x, and  $AOQ = 3 \times 90$  degrees + x. If the

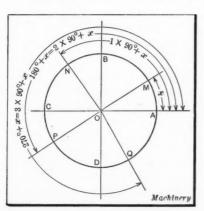


Fig. 1. Angle Diagram

angle is greater than 360 degrees (=  $4 \times 90$ degrees), subtract 4 (or some multiple of 4), so that n will be less than 4, but not negative. For example, the functions of 563 degrees  $= 6 \times 90$ degrees + 23 degrees are exactly the same as for  $2 \times 90$  degrees +23degrees = 203 degrees. Having expressed the angle in the form  $n \times 90$ degrees + x, note whether n is even or odd; if it is even (0, 2,

4, etc.), the numerical values of the functions will be the same as those for x; but if n is odd (1, 3, 5, etc.), the numerical value of the functions will be the same as those for the cofunctions of x. Thus the numerical value of the sine of 203 degrees  $= 2 \times 90$  degrees + 23 degrees is sin 23 degrees; of 296 degrees = 3 × 90 degrees + 26 degrees is cos 26 degrees, cot 163 degrees =  $1 \times 90$  degrees + 73 degrees =  $\tan$ 73 degrees, etc. The sign of the function is determined by noting the quadrant in which the revolving radius stops. As shown in Fig. 2, all the functions are positive for the first quadrant AB. Note that for the upper semicircle ABC, the sine is positive and for the lower semicircle it is negative. For the right-hand semicircle BAD, the cosine is positive; and for the left-hand semicircle, it is negative. In the diagonally opposite quadrants AB and CD, the tangent and cotangent are positive, and in the other two diagonally opposite quadrants BC and DA, they are negative. From this it follows that  $\cos$  685 degrees, 13 minutes, 33 seconds =  $\cos$  7 imes 90 degrees + 55 degrees, 13 minutes, 33 seconds = cos 3 imes 90 degrees + 55 degrees, 13 minutes, 33 seconds = +  $\sin$  55 degrees,

13 minutes, 33 seconds. The name of the function changes from the cosine to the sine because n is odd; the sign is plus because the revolving radius stops between D and A in the fourth quadrant, and the cosine of any angle in this quadrant is +. The sign of the secant is the same as that of the cosine of the same angle, since the secant is the reciprocal of the cosine; for the same

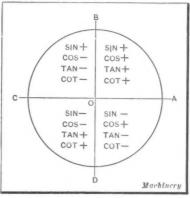


Fig. 2. Signs of Functions in Each Quadrant

reason, the sign of the cosecant is the same as that of the sine of the same angle.

# GANG AND MULTIPLE-SPINDLE DRILLING MACHINES

E. K. H.—What is the distinction between an upright multiple-spindle drilling machine and a gang drilling machine? It is my impression that a machine is classified as a multiple-spindle drilling machine if there are two or more spindles carried by a single frame, and that it is known as a gang drilling machine if there are two or more spindles carried by individual machine frames.

A .- This question was submitted to the principal makers of multiple-spindle and gang drilling machines, but there seems to be no general agreement. F. K. Hendrickson, of the Reed-Prentice Co., Worcester, Mass., writes: "Originally a gang drill meant not only a machine composed of a series of independent frames or columns carrying one or more spindles, but any type of machine wherein there were several spindles. I note that it is your impression that a multiplespindle drill is composed of two or more spindles carried by a single machine frame and that a gang drill is composed of two or more spindles carried by individual frames. If your meaning of the word 'frame' applies to the entire column or unit, the distinction would be quite definite, but if your understanding of the word frame merely suggests the member carrying the spindle, the situation becomes a little more complicated. In referring to the old type of gang drills such as were originally used by the railroads, a main housing with cross-rail was a general construction upon which were mounted several heads, each carrying its own spindle or multiple spindles. This type of machine was generally known as a gang drill. It is my opinion that a multiple-spindle drilling machine is any drilling machine having a single housing, with all the spindles either mounted in a single head or in independent heads and supported by the single housing, while a gang drill is a series of practically independent machines driven from one source of power and mounted either on a single base or independently in a group."

G. E. Randles, vice-president of the Foote-Burt Co., Cleveland. Ohio, states that it is their opinion that any drilling machine having more than one spindle is a multiple drill, and from this the different types should be classified, such as: universally adjustable (which would be the Baush type); fixed center independent feed, the type of drilling machine in which the spindle heads are mounted on a common crossrail and adjustable in a straight line for centers, but provided with an independent feed for each spindle. "The gang type is this same sort of machine, except where the feed is connected up in a gang and the feed on all spindles is engaged and disengaged at one time and from one point. We think this type of machine is more truly the gang drill than the type to which you refer where several individual machines may be set on one base with one common table, such as the Barnes type. We would say that the correct term for a battery of machines of this sort would be fixed by the size of the machine set in a gang, no matter what number may be used. We build practically all types of multiple-spindle drills and class everything of more than one spindle as a multiple drill, but also classify them beyond this as universally adjustable multiple drills, independent-feed multiple drills, gang-type multiple drills, etc."

G. E. Hallenbeck, of Baker Bros., Toledo, Ohio, writes that it is their belief that "multiple-spindle drill" should apply to machines of the Baush, Fox, "Natco" or cluster box type, and that "gang drill" should apply to single-spindle drilling machines connected in a gang.

### TOGGLE FRICTION CLUTCH

H. W. L.—The two clutches shown roughly in Fig. 1 act on the toggle principle. What is the theory pertaining to the friction and forces acting on the bearing surfaces of such clutches? I have been unable to find any data of this kind.

Answered by John S. Myers, Philadelphia, Pa.

To illustrate the principle on which such clutches operate, refer to Fig. 2. Here, a block resting upon a smooth surface is acted upon by a force C. This surface reacts against the block with an equal force C, neglecting the weight of the block. Now force C may be resolved into a component N acting normal to the surfaces and a component F acting parallel to the surfaces. The resistance offered by friction opposing motion in the direction of the arrow is fN, where f= coefficient of friction. If this resistance is greater than the component F, no sliding of the surfaces will result. As F=N tan a, if we do not desire sliding to occur, N tan a must be less than fN, or tan a must be less than the coefficient of friction f.

The same principle applies to the clutch problem, and the forces there acting are indicated by similar letters in Figs. 3, 4 and 5. The function of the spring A, Fig. 1, is simply to keep the friction surfaces in contact, and the forces due to it as well as to centrifugal effect, being small, may be neglected. For example, suppose that it is desired to develop a twisting moment of 6000 inch-pounds with a radius R of 10 inches and a coefficient of friction f=0.08; what are the forces acting? The frictional component must be  $F=6000 \div 10=600$  pounds. Taking tan  $\alpha=0.06$ , allowing 0.02 less than f

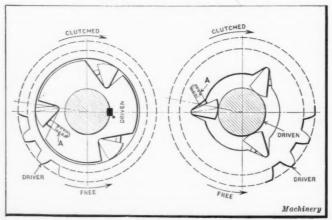
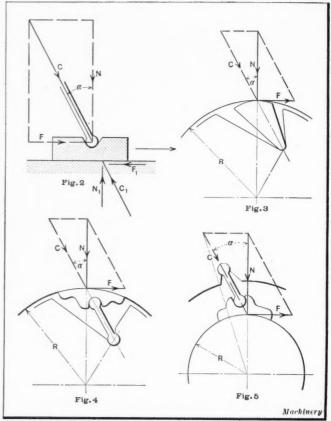


Fig. 1. Toggle Friction Clutches



Figs. 2 to 5. Diagrams showing Principles of Friction Clutches

as security against slipping, the force acting normal to the friction surfaces is  $N=\frac{F}{\tan a}=\frac{600}{0.06}=10{,}000$  pounds, or

 $10,000 \div 3 = 3333$  pounds on each of the three surfaces. The various parts of the clutch would have to be sufficiently strong to withstand these forces. Problems allied to this are discussed in "The Constructor," by Reuleaux, pages 158 to 161. The wearing shoes indicated in Figs. 4 and 5 make no difference in the theory of the device, but increase its useful life by preserving the proper length of the toggle element.

# \* \* \* CONCRETE MIXTURES

In a paper read before the Concrete Institute of Great Britain recently, it was stated that in a 1-2-4 concrete the cement may range from 18 to 24 per cent of the total volume of the mixture. For instance, 130 tons of dry cement is required for a broken-stone aggregate and only 100 tons when gravel is used. But the concrete containing gravel is from 12 to 15 per cent weaker than the one with the broken stone. However. when the quantity of cement per cubic foot of the mixture is the same, gravel concrete is as strong as concrete with a broken-stone aggregate. Washing the aggregate increases the strength of hand-mixed concrete 30 to 40 per cent, and of machine-mixed concrete, from 15 to 20 per cent. As the strength of concrete is governed largely by the percentage of cement that it contains, it has been suggested that specifications, instead of calling for a 1-2-4 mixture, provide that the volume of dry cement used be a specified proportion of the total final volume of the mixture.

A new type of soldering iron consists essentially of two high-resistance heating points, or electrodes, that become incandescent when the current passes through them. As the circuit is closed as soon as the points come into contact with the metal to be heated, the iron is said to become heated to the required degree the moment it touches the work. Besides, the heat is generated at the point of contact and at the spot where the heat is needed when soldering, brazing, or annealing. The iron operates at from six to sixteen volts and the points are made to carry current according to ratings of 150, 250, and 500 watts.

# NEW MACHINERY AND TOOLS

THE COMPLETE MONTHLY RECORD OF NEW AMERICAN METAL-WORKING MACHINERY

# LEEDS & NORTHRUP OPTICAL PYROMETER .

This is an optical pyrometer for determining temperatures by the comparison of luminous hot bodies with a tungsten lamp filament in the pyrometer, which is adjusted by means of a rheostat until the brightness of the lamp corresponds to the brightness of the heated part as seen through the pyrometer. The reading of a milli-ammeter connected to the pyrometer enables the observer to determine the temperature with considerable accuracy, the readings of different observers for temperatures within the hardening range of steel varying not more than six degrees.

For the measurement of temperatures above, say, 1400 degrees F., only two methods have been found practicable for works service. One of these is based on the thermo-couple and the other on the laws of radiation. The latter includes both the radiation pyrometer and the optical pyrometer, which utilizes only that radiant energy visible to the human eye. For many services the inexpensive base-metal couple may be used for accurate measurements up to 2000 degrees F. with satisfaction; the more fragile and expensive platinum couple may be used up to 2800 degrees F., but the thermo-couple, like thermometers in general, must assume the temperature of the hot object by convection, conduction, radiation, or all combined. This fact militates against its use for measuring the temperature of molten brass, iron and other metals, or for measuring temperatures in gas producers and other locations where the thermo-couple would be subjected to rough mechani-- cal treatment or to contamination by vapors and gases, which would rapidly impair its accuracy. In many industries the temperatures are far above the range of thermo-couples.

Measurements by radiation can be carried out at a distance when the laws concerning the temperature of radiating body and intensity of radiation have once been determined, and the radiation receiving and measuring part need not be heated to the temperature of the radiating body, nor even anywhere nearly to that temperature. Pyrometers utilizing radiation are divided into two classes: those which measure as heat energy the total radiation falling upon the receiving part



Fig. 1. Leeds & Northrup Optical Pyrometer

of the instrument, and those known as optical pyrometers, which are based upon the fact that the luminous radiation or light varies in a definite manner as the temperature of the hot body changes.

The greatest success has been attained by separating out one wave length of radiation—usually that which excites the sensation of red—and comparing the intensity of this one-color light with the intensity of the light of the same color emitted by a standard source of light. The eye is very sensitive when comparing the brightness of two surfaces when one is superimposed upon the other, and after having arranged to have light from the hot body and light from the standard of comparison viewed in this relation, they can be made equal, either

by varying the amount of light received from the incandescent object or by varying the intensity of the standard of comparison. The latter method, that is, variation of the intensity of the standard of comparison, is preferred and used by the U. S. Bureau of Standards, also by the Reichsanstalt, of Berlin, where its practical application has been brought to a high degree of perfection by Messrs. Holborn and Kurlbaum. The Leeds & Northrup Co., of Philadelphia, Pa., working under the

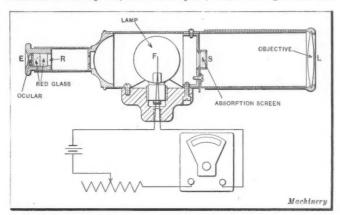


Fig. 2. Optical System and Electrical Circuit of Leeds & Northrup
Pyrometer

fundamental Morse patents, has developed this type of optical pyrometer with a view to realizing a high degree of accuracy and reliability in a simple and portable device. The instrument, which is illustrated in Fig. 1, is suitable for measuring from dull red (about 1100 degrees F.) up to the highest known temperature.

The manner in which the luminous radiation from the hot body is balanced against that from a standardized source will be understood by reference to Fig. 2. By means of the lens L, rays from the hot body are brought to a focus in the plane F, where there is located a tungsten lamp filament. By means of the eye-piece E, the observer views the incandescent filament, which appears to lie upon the image, just as the crosshairs in a surveyor's telescope appear upon the distant object looked at. By means of a rheostat in a case slung about the neck (see Fig. 3), the case also containing a storage battery and a milli-ammeter, the current through the lamp is adjusted until the brightness of the filament is just equal to the brightness of the image produced by the lens; that is, so that the filament blends with the background formed by the hot object. The observer then notes the reading of the milli-ammeter. which may be provided either with a special scale to read in degrees of temperature or the temperature corresponding to the current may be read from a calibration curve supplied with the instrument. The adjustment is made with accuracy, as the eye is keen in distinguishing differences in brightness between superimposed objects.

At high temperatures the light emitted by both the hot body and the filament would become dazzling, and comparison would be difficult. For this reason a red glass is placed in the eye-piece at R, which has the further advantage that light of only one color then reaches the eye and no difficulty is introduced by lack of color identity between the light emitted by the hot body and that emitted by the filament. The intensity of light radiation of any one color increases progressively in a definite manner as the temperature of the radiating body rises, and nothing is therefore lost by eliminating all other light from the comparison. As only brightness, not color, of light is matched, inability to distinguish colors and color-blindness do not interfere with the use of the instrument. In fact, in the range of temperatures used for harden-



Fig. 3. Method of using Optical Pyrometer

ing steel, for example, different observers using this instrument agree in their readings within 6 degrees F.

The brightness of the image of the hot body produced by the lens L is almost absolutely constant, irrespective of the distance from the hot body, although the size of the image varies with the distance. Since it is the brightness of the image and not the total radiation received through the lens that is measured, it is possible to measure the temperature of a small body or of a body at a distance equally as well as that of a large body or of one near at hand. It is not necessary that the hot body should fill the entire field of view of the instrument, as with "total radiation" pyrometers.

In observing bodies at very high temperatures, as 2500 degrees to 10,000 degrees F., the light received through the lens is too blinding for direct observation, even through the red glass of the eye-piece, and the intensity of the image might also become greater than that at which it is practicable to burn the tungsten filament, so that a balance would become impossible. Some method for reducing the intensity of the light must therefore be provided, such as by placing a screen to intercept some of the light. The screen is placed between the lens and the image so that it reduces the light from the hot body, but not that from the filament. With the reducing screen it is possible to make direct observations of the most brilliant light, as the electric arc or the surface of the sun.

It is not feasible to calibrate the instrument at such high temperatures by direct comparison, since they are above all known melting points and the ranges of contact thermometers, but fortunately a relation has been found to exist between temperature and intensity of radiation of any one color or wave length of light. By making use of this relation. known as Wien's law, and reducing the intensity of the image in a known ratio by means of the screen just referred to, it is possible to extend the scale of the instrument to the highest The scale thus obtained has been found to temperature. agree closely with a scale of temperatures established by known facts about the relation between temperature and total radiation. In other words, this form of optical pyrometer gives the same scale of temperature as do total energy pyrometers used with the precautions necessary to secure accuracy and precision in the measurement of total radiation. The screen used for cutting off part of the radiation from very hot bodies can be thrown into or out of the field of view by means of a milled disk projecting through an opening in the tube of the instrument. With the absorbing screen in use, a different milli-ammeter scale or calibration curve is required, but as the range of the instrument without the absorbing screen overlaps many hundred degrees with the range for the absorbing screen, the accuracy of the two scales can always be checked by observing a hot body, the temperature of which lies within this range.

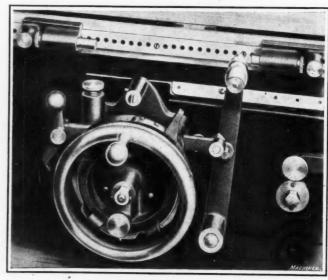
The readings obtained with this instrument are always the same for the same temperature, if the body viewed is surrounded by other objects, such as the walls of a furnace at the same temperature. Also no correction is required in the case of so-called "black bodies," such as incandescent carbon, when viewed in the open. For iron and steel in the solid state, the corrections required for readings taken in the open are also negligible. Objects having a metallic sheen, that is, a surface which reflects light freely, as molten metal or polished platinum, do not give the same readings when viewed in the open as when viewed in the furnace, or as a black body would give with this or any other radiation or optical pyrometer. The readings, however, are always consistent for the same material under the same conditions, and by using suitable reduction factors, can be converted to true temperatures. Furthermore, the readings obtained with this type of instrument when sighted upon a body in the open differ less from those given for the same body at the same temperature enclosed in a furnace, or for a black body at the same temperature, than do the readings of instruments which measure the total radiated energy. In other words, the correction where there is a departure from "black body" conditions is smaller than with the total radiation pyrometer.

The instrument can be calibrated by sighting it upon bodies the temperatures of which are known, either by means of a thermo-couple pyrometer, or by the melting or freezing of various substances. The constancy or reliability depends upon the constancy of the lamp, or its ability always to shine with the same intensity when receiving the same current. This matter has been investigated exhaustively by the U. S. Bureau of Standards and also in the laboratory of the Leeds & Northrup Co., and it has been found that after a tungsten filament is thoroughly aged, that is, burned for some time at a temperature higher than that to which it will be subjected in service, no sensible variation thereafter occurs. The instrument is so designed that one lamp can quickly be replaced by another, and by keeping two lamps, their correctness can always be insured by checking one against the other.

The instrument itself is handy and portable, weighing only a few ounces, and can be sighted as easily as an opera glass. The case, containing the battery, rheostat, and milli-ammeter, is slung about the neck, and weighs about ten pounds.

# CROSS-FEED MECHANISM FOR OTT GRINDER

The Ott Grinder Co. of Indianapolis, Ind., has brought out a new design of universal grinding machine. The most notable feature of this machine is the automatic cross-feed mechanism,



Automatic Cross-feed Mechanism applied to No. 2 Universal Grinder built by the Ott Grinder Co.

which is shown by the accompanying detail illustration. In order to obtain simplicity and ease of adjustment, this mechanism has been equipped with a single rocker arm, a spring plunger and a stop-screw. When the table reaches the end of its stroke, the cross-feed rocker arm is swung down to its lowest position by a hardened pin on the reverse lever. As the table reverses its motion, the rocker arm is forced to move upward by a compressed spring. This upward movement continues until it is arrested by an adjustable stop-screw.

The pawl attached to the left-hand end of the rocker arm engages the cross-feed ratchet wheel, thus feeding the wheel slide. The feeding movement may be varied from 0.00025 to 0.003 inch. With this mechanism the grinding wheel is fed inward by the positive action of the reverse lever as it engages the rocker arm, whereas the spring previously referred to is simply relied upon to move the rocker arm and pawl back an amount depending upon the feed adjustment. The feeding movement may be disengaged by swinging over the feed pawl or by screwing down the adjusting stop. The feed may be disengaged automatically, a positive stop being provided for hand feeding.

#### METALWOOD STRAIGHTENING PRESS

The Metalwood Mfg. Co., Leib and Wight Sts., Detroit, Mich., is now manufacturing a straightening press in 20- and 35-ton sizes, and in three styles, including a motor drive, a belt drive from a lineshaft, and an accumulator drive. The particular press shown is equipped with a motor. The hydraulic pump for operating the press forms an integral part of the design and is of the two-plunger type. This pump is mounted upon the base, which forms a tank for the liquid. The pump body is of bronze, and the plungers are of tool steel, hardened and ground. The pump bearings are of phosphor-bronze. The ram of the press is returned by a heavy spring arranged for differential pull and with an adjustable tension. The ram nose has a sliding chrome-nickel steel resistance block with two steps for crank work, so as to reduce the stroke of the press whenever practicable and increase the operating speed.

The table is made of semi-steel and is provided with renewable steel strips upon which the centers are mounted and which take the thrust of the ram when pressure is applied to the part being straightened. The table is finished on the top and sides so that indicators can be used for testing the work. The centers are of the yielding type and are adjustable for length. The thrust is taken by tapered steel wedges placed under the work on the steel tracks. A single lever and a quick-operating valve serve to control the speed of the

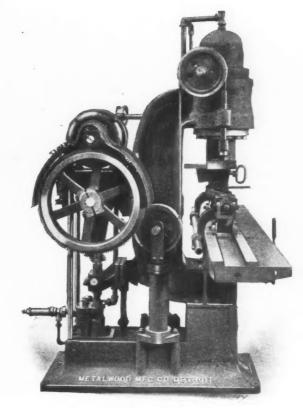


Fig. 2. Side View of Straightening Press

press ram, the pressure applied, and the return movement. All parts of the press subjected to heavy stresses are of alloy steel castings or forgings, and all piping under hydraulic pressure is of seamless steel tubing. The press is equipped with a gage reading in pounds per square inch and tons on the ram or applied to the work.

#### WESTINGHOUSE OVEN HEATER

An electrical oven heater designed especially for use in enameling or japanning ovens is illustrated herewith. This heater may also be applied for a variety of work where ovens are employed for a baking or drying process. The heating element consists of a ribbon wound on a number of fire-clay bushings assembled on two steel tie-rods, between two pressed steel end-plates. The ends of the ribbon are secured to dropforged steel terminals, clamped to the steel tie-rods, which therefore become the terminals for the heaters. The tie-rods are insulated where they pass through the end frames, and the ends are threaded for bolting onto the connectors. Special

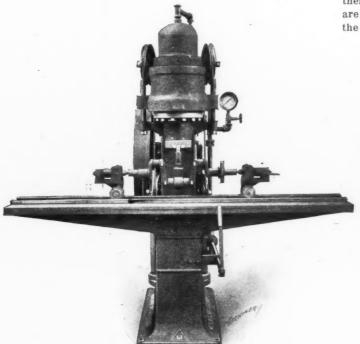
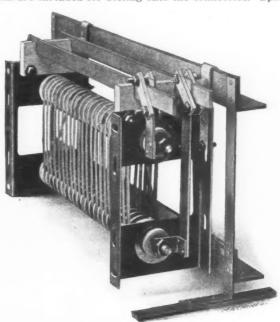


Fig. 1. Front View of Metalwood Straightening Press



Westinghouse Type C Oven Heater

connectors are furnished to meet requirements. Cold-rolled steel bus bars are recommended, and may be mounted directly above the heater on insulators bolted directly to the end-frames. Connectors are secured to bus bars by steel clamps.

Hooks are used for hanging the heaters from the usual supporting steel work, which may be flat iron, angle iron, channel iron or pipe work. The hooks are bolted to the flanged endplates of the heaters. Protecting screens may be attached di-

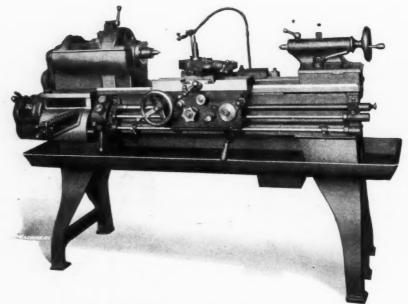


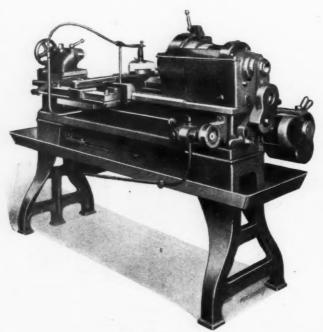
Fig. 1. Davis "Close-coupled" Tool-room Lathe

rectly to the flanged end-plates without any other means of support. Heaters may be mounted either on the side walls or on the floor, and in any position.

These heaters are normally rated at 2.5 kilowatts at 120 volts. Any number of them may be installed in an oven, and connected to any power circuit, whether single-phase or polyphase and 110-220 or 440 volts. On 220-volt service, two heaters are connected in series, and on 440-volt service, four heaters are connected in series. Where three-phase power circuits are used, the heaters are connected three-phase, with the phases balanced. This heater (Type C) is made by the Westinghouse Electric & Mfg. Co., East Pittsburg, Pa.

#### DAVIS TOOL-ROOM LATHE

The "close-coupled" tool-room lathe now being manufactured by the Davis Machine Tool Co., Inc., Rochester, N. Y., has been designed to meet modern requirements as to accuracy, convenience, power and simplicity of construction. Front and rear views of this machine are shown in Figs. 1 and 2, and a sectional view of the headstock in Fig. 3. One of the important features of this lathe is the method of mounting the "back-gears," which are placed under the headstock at the front end of the spindle. The small cone gear that is usually located at the end of the cone next to the small step is placed



kig. 2. Rear View of Davis Lathe

next to the large end of the cone. The backgears are carried in a voke which swings from a bearing at the back of the headstock. These gears are engaged with the cone gears by a cam operated from the front of the lathe by the small handle seen in Fig. 1 at the right of the gear-box. With this back-gear arrangement, the long eccentric shaft and quill common to cone-driven lathes, and the torsional strains to which this member is subjected, are eliminated.

The headstock is a heavy one-piece cast-

ing. Gear guards are integral with the headstock and form a cover for the cone pulley. At the top of the gear guard there is a brake for stopping the rotation of the spindle. This feature is of especial value when frequent inspection or gaging is necessary. The crucible steel spindle is mounted in heavy phosphor-bronze boxes, which are lubricated from large oil pockets by means of rings. The front spindle bearing is tapered to compensate for wear. The carriage has a bearing

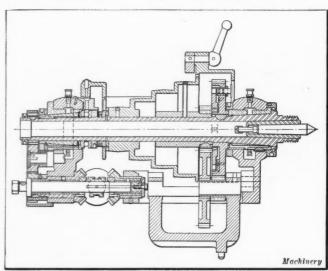


Fig. 3. Headstock of Davis Lathe

of  $19\frac{1}{4}$  inches on the ways and a cross-bridge 6 inches wide. The compound rest is provided with four clamping bolts for holding it rigidly in any position.

The apron is of the double-plate type with two bearing supports for all shafts. A central oil pocket is arranged to lubricate all bearings from one point. The apron has the usual interlocking feature to prevent engaging the feed-nut and halfnut at the same time. The lever seen in Fig. 1 beneath the right-hand end of the apron serves to reverse the movement of the carriage by shifting a sliding clutch interposed between bevel gears located beneath the headstock. The same rod that operates this reverse mechanism carries adjustable collars for stopping the feeding movement of the carriage at any point. This lathe has a screw cutting capacity varying from 11/2 to 80 threads per inch, including 111/2. The regular equipment provides thirty-six different leads or pitches, and this number can be increased by applying change-gears to the quadrant. The maximum error allowed in the lead-screw is 0.001 inch per foot. Thirty-six different feeds are provided, the feeding movement being transmitted through an independent feed-rod. All gears in the quick-change gear-box are made of steel and generated on a gear shaper.

accompanying il-

lustration. The

machine swings

diameters up to

72 inches and

takes work 16

inches high un-

der the saddles.

It is driven by

a twenty-five-

horsepower elec-

tric motor. The

general design

of this machine

that of a stand-

ard boring mill,

but owing to the

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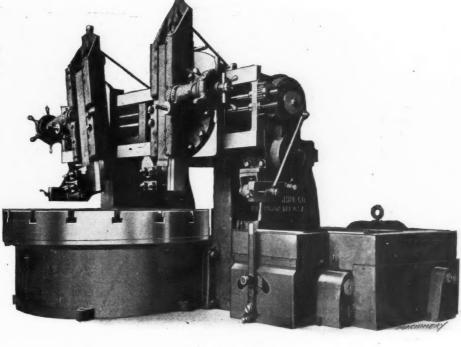
ing gears are of

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To insure correct alignment, an extra foot is placed in the center of the right-hand leg, so that the lathe has a three-point support. The outer ends of the right-hand leg are provided with adjusting bolts which can be screwed down until they just touch the floor, thus overcoming any rocking tendency. The bed of this machine is ribbed transversely with heavy doublewall cross girths. The rear end is low enough to

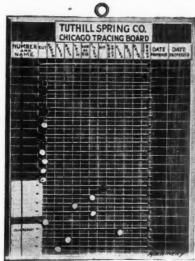


Betts Tire Turning Mill

permit sliding off the tailstock without disengaging the clamping bar or removing bolts. The manufacturers will supply this machine with a motor drive if desired. The motor is mounted

> over the headstock and is geared to the spindle through a train of gears which provide four mechanical changes by sliding clutches. Further speed changes are obtained through the motor, which should have a variation of from 500 to 1500 revolutions per minute. This lathe may be equipped with a taper attachment, draw-in chuck and collets, transposing gears for cutting metric pitches, and a relieving attachment if desired by the pur-

> > chaser.



Board for following Progress of Orders through the Plant

#### TUTHILL SPRING CO.'S TRACING BOARD

The tracing of orders so that delays are noticed, the causes discovered, and deliveries made on schedule time, is a problem common with all manufacturers. Tuthill Spring Co., Kesner Bldg., Chicago, Ill., formerly followed the progress of orders through their plant by a card index system. Every day the exact location of each job was noted on a card, and the superintendent or shipping clerk was kept posted on just what was taking place by referring to the cards.

The tracing board, the upper section of which is shown in the illustration, was devised to facilitate this work. This particular board is used in tracing Chicago orders. Each day the entry clerk, in a much shorter time than it took to make the card records, can bring his tracing board up to date. A glance tells the superintendent, or anyone else interested, the exact status of each job.

#### BETTS TIRE TURNING AND BORING MILL

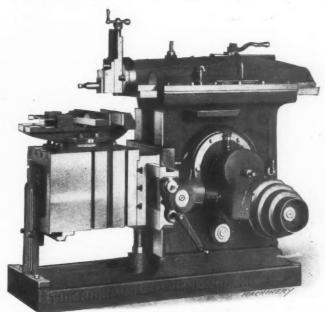
A 66-inch tire turning and boring mill recently built by the Betts Machine Co., Wilmington, Del., is shown in the

ly covered, and provision is made to lubricate them properly; all feed gears, saddles and tool spindles are of steel, and the latter are independently counterbalanced and have rapid hand movement. Separate feed works are provided for each side of the machine, and the feeds can be changed quickly without stopping the machine.

The necessary speed changes are obtained through the field control of the motor in connection with two or three mechanical changes. This style of machine is built in five different sizes, ranging from 66 inches up to 108 inches, and it can be furnished with a movable instead of a fixed cross-rail so that it may be used for general machine shop work as well as for tire work.

#### COLUMBIA 20-INCH CRANK SHAPER

The heavy-duty crank shaper illustrated herewith is a 20inch size built by the Columbia Machine Tool Co., Hamilton, Ohio. The column of this machine is made straight in front in order to permit the head to be set at an angle without interfering with its full travel across the table. The feed mechanism of this machine is designed along somewhat different lines from usual; it is carried in a housing which covers and protects the gears, and is an adaptation of the well-known



Columbia 20-inch Heavy-duty Crank Shaper

ratchet type. Feed changes may be made quickly, and a safety stop is provided, as well as means of controlling and indicating the direction of the feed. There are eight feed changes in all.

The position of the ram and the length of the stroke can readily be adjusted from the front of the machine. The ram is held in place by clamping gibs on top of the column, and an angular gib at one side of the ram provides adjustment for wear. The tool-head has a micrometer adjustment and is graduated for angular adjustment. The machine is proyided with back-gears, which, in connection with the four-step driving cone pulley, give eight speed changes in geometrical pro-

gression. The table is of box form and long enough to accommodate work up to the full rated capacity. In addition to the regular T-slots, a V-groove is formed in one side of the table for holding round stock. The vise regularly furnished is of the double-screw type and has a graduated swiveling base.

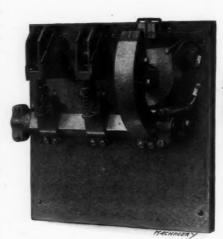


Fig. 3. Magnetic Contactor Panel



Fig. 4. Gage Type Pressure Regulator

### WESTINGHOUSE AUTOMATIC STARTERS FOR INDUCTION MOTORS

Several automatic starters for motor-driven machinery, (manufactured by the Westinghouse Electric & Mfg. Co., East Pittsburg, Pa.), are shown in Figs. 1 to 4 inclusive. These automatic starters are for use with single-phase or polyphase squirrel-cage and wound-rotor induction motors, where it is desired to start the motor from a remote point or where automatic acceleration is required to guard against improper starting by unskilled operators. They are simple, reliable, and rugged in construction, consisting of a magnetic contactor panel and a master switch, which may be either a pushbutton, a float switch, a pressure regulator, or similar device for closing the control circuit, depending upon the service. The vital element is the magnetic contactor. The contactors used on these starters have been employed successfully in steel mill, cement plant, and mine installations, where the requirements are extremely severe. The contactors are opened by strong spring action assisted by gravity. The destructive action of the arc is reduced to a minimum by strong blow-out coils and arcing horns.

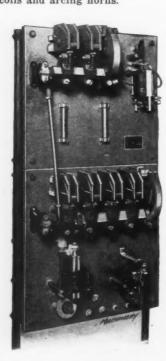


Fig. 1. Automatic Starter



Fig. 2. Westinghouse Highvoltage Starter

The operation of the starters is very simple. When starting motors driving lineshafting, woodworking, and machine tools, and similar apparatus, it is only necessary to press a button, and close a small knife or snap switch. The starter then automatically makes the proper connections to limit the starting current to a suitable value and to vary the time required for acceleration according to the load on the motor, thus preventing damage to the machinery by too slow or too rapid acceleration, and saving time by bringing the motor to full speed at the most rapid permissible rate. When used for pump or compressor service in connection with a float switch or pressure gage, the action of the starters is entirely automatic, the motors being started when the pressure or liquid level of the tank control falls to a predetermined point, and stopped when the desired maximum pressure or level is reached, or vice versa.

The automatic starters for squirrel-cage motors are most frequently employed for starting motors operating centrifugal pumps, air compressors, fans, blowers, metal-working and wood-working machines, and other apparatus requiring starting torque less than full load torque. This type of starter, however, owing to the wide application of squirrel-cage motors for industrial service, can be applied economically for starting service in nearly every industry.

Squirrel-cage motors of five horsepower and smaller are usually connected direct to the line. Large squirrel-cage motors are first impressed with low voltage from auto transformers or connected to the line through resistance so that in either case the starting current is reduced. When the speed of the motor has reached such a point that the starting current has decreased sufficiently the motor is then automatically connected to the line.

The automatic starters for wound-rotor motors are particularly adaptable for starting motors driving plunger pumps, positive pressure blowers, air compressors, long lineshafts, and loads having heavy inertia. The severe starting conditions encountered in this class of service require from 100 to 200 per cent full load torque in starting, making automatic starting a very desirable feature.

When an automatic starter is used in connection with a wound-rotor motor, the line switch is first closed, with the maximum resistance in the rotor circuit. When the speed falls to a predetermined value, a relay closes a magnetic contactor which cuts out a part of the resistance in the rotor circuit. Each contactor operates in a similar manner, cutting out its portion of the resistance at the proper time until all the resistance is short-circuited by the last contactor.

The power on any circuit may fail suddenly, and it is important that some protection be afforded both operator and motor against an unforeseen return of power. This protection may be provided for motors operating pumps, compressors, etc., by a low-voltage release to disconnect the motor from the line when the voltage is low or the power fails entirely. Then as soon as the power returns, the motor will automatically start up again. In many applications, however, such as for motors operating machine tools or wood-

working machines, low-voltage protection is required. Motors so protected are disconnected from the line when the power fails and will not start when the power comes on again until the operator presses a button or manipulates a similar device; hence, there is no danger from the unexpected starting of a machine.

The advantages resulting from the use of automatic starters for induction motors comprise absolute protection to both operator and machinery, proper starting at the most rapid permissible rate, economy in operation and maintenance, convenience of remote control, and automatic operation.

#### FOX ARBOR PRESS

The Sunderland Machinery & Supply Co., 1006-1010 Douglas St., Omaha, Neb., has placed on the market an arbor press known as the Fox "high-speed" No. 4, that is designed for rapid operation and adjustment. The press is equipped with a special type of mechanism for elevating and lowering the



Fox No. 4 Arbor Press

table easily and rapidly. The table is counterbalanced by a weight at the rear of the press so that it can easily be raised or lowered. It is elevated by grasping the handle at the left-hand side and simply lifting it, and is held in position by the rack and pawl shown beneath it. In order to lower the table the pawl is first disengaged from the rack by a lever provided for that purpose, and the table is then pushed down to the required position. The press ram is operated by a counterweighted ratchet lever, as the illustration shows. The frame and table are of cast iron, and the rack, pinion, pawl and ratchet are

made of a special alloy steel properly heat-treated. This press will take diameters up to 19 inches, and the capacity over the table is 30 inches. The ram has a movement of  $17\,1/7$  inches and the leverage is 60 to 1. The weight of the press is 1100 pounds.

#### SKELTON TAPER REAMER

The taper reamer shown in Fig. 1 is designed for reaming taper holes and has a flat, high-speed steel blade and a low-carbon steel holder. The edge A, Fig. 2, is ground to a circular form, and between this edge and the heel B there is a flat surface. The heel is backed off or relieved sufficiently to allow for the maximum cut and still prevent "hogging in," the depth of cut being positively controlled by the clearance or amount ground away at B. The curved flutes C, adjacent to each cutting edge, provide rake so that the reamer cuts the metal instead of scraping it. The method of holding the blade allows



Fig. 1. Skelton Taper Reamer

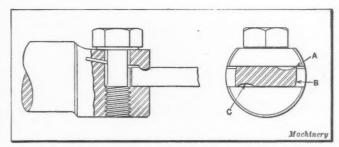
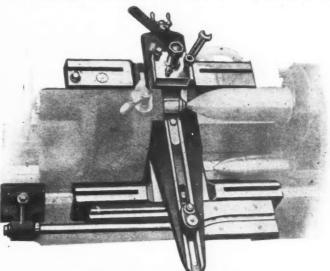


Fig. 2. Connection between Blade and Holder of Skelton Reamer

for lining up the reamer with the spindle in case the turret hole is out of alignment. As Fig. 2 shows, the end of the holder is split and it has a circular tongue which engages a circular groove extending across the end of the reamer blade. The tongue is offset slightly with reference to the groove in the blade so that the blade is forced back into the bottom of the slot, thus aligning it with the holder. The clamping screw is of nickel steel, heat-treated and so arranged that the pressure comes in front of the holder. This reamer has been placed on the market by Charles E. Skelton, 107 N. Franklin St., Syracuse, N. Y.

### SHELL FORMING ATTACHMENT FOR CINCINNATI LATHES

An attachment for use when turning shells is shown in the accompanying detailed view as applied to one of a number of 18-inch lathes built by the Cincinnati Lathe & Tool Co., 3207-3211 North St., Oakley, Cincinnati, Ohio. A shell made of 50-point carbon steel, having a 12-inch radius, was finished to the required size and form with an attachment of this type in 16 minutes, 48 seconds. The actual cutting speeds varied



Shell Forming Attachment applied to Cincinnati Lathe

from 69 to 204 feet per minute, owing to the curvature of the shell, and a feed of 1/32 inch was used. The attachment illustrated is equipped with a cam for forming 6-inch shells.

#### ARMSTRONG-BLUM METAL-CUTTING BAND SAW

A universal metal-cutting band saw, which is the product of the Armstrong-Blum Mfg. Co., 343 N. Francisco Ave., Chicago, Ill., is shown in a vertical position in Fig. 1, and in Fig. 2 with the saw blade tilted to an angle of 45 degrees for cutting an 18-inch beam. The saw may be inclined to a 45-degree angle, either to the right or left, and its position is indicated by suitable graduations. The saw blade is mounted on two flanged wheels supported by a rigid frame, which is pivoted to a frame or cage under the table. This cage is equipped with four hardened roller bearings that travel in planed dirt-proof races. The automatic feeding movement may be engaged or disengaged by means of a small lever at the front of the machine.

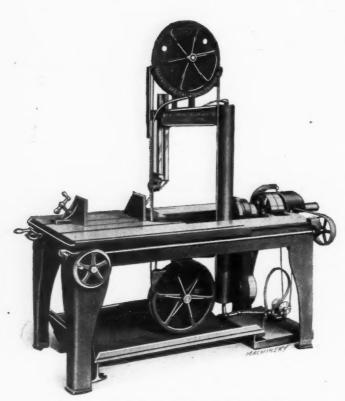


Fig. 1. Armstrong-Blum No. 8 Metal-cutting Band Saw

The required pressure is imparted to the saw blade by a bronze worm-gear having cork inserts, two friction disks, a spring and an adjusting nut. Lubrication is supplied to the saw blade at the cutting point by a submerged centrifugal pump, the lubricant passing directly through the teeth at the point of delivery. The saw blade guide rollers have double ball bearings and felt dirt-proof rings. The machine may be stopped at any required depth of cut by a knock-off dog or trip. The saw table is 32 inches wide, 5 feet long, and has four T-slots. The two inner slots are machined and notched to receive the vise jaws, which may be placed wherever needed or be removed entirely. The drip-pan is telescopic and designed to catch the lubricant when the saw blade is inclined 45 degrees either way from the vertical. The speed of the saw

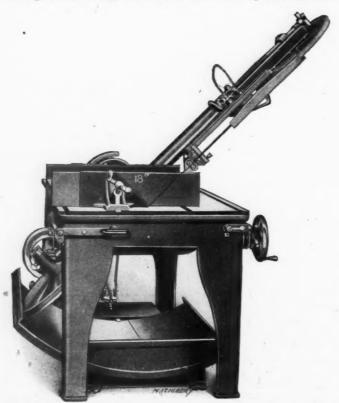


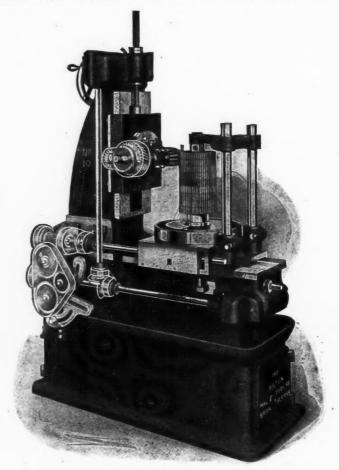
Fig. 2. Metal-cutting Band Saw set at Angle of 45 Degrees for cutting 18-inch Beam

may be increased about 90 per cent by means of double cone pulleys. This machine has a throat capacity of 18 by 20 inches. The saw blade is 14 feet, 8 inches long, 5% inch wide, and 0.032 inch thick. Guards are provided wherever necessary.

### BILTON UNIVERSAL GEAR-HOBBING MACHINE

A universal gear-hobbing machine recently added to the gear-cutting equipment of the Bilton Machine Tool Co., Bridgeport, Conn., has a rated capacity for gears of 10 inches outside diameter, 10 diametral pitch and 10 inches width of face. The work-table of this machine (see accompanying illustration) is driven through a steel worm and a bronze worm-wheel 11½ inches in diameter. The worm is automatically lubricated and is fitted with a ball thrust bearing. Automatic stops are provided for the vertical and horizontal feeding movements, and the horizontal feed shaft has a micrometer dial. The differential gears and the feeding and indexing gears, which are on the rear end of the machine, all have teeth of 14 diametral pitch, so that they are interchangeable, and the total number is reduced to a minimum.

The vertical slide is made extra long and has flat ways with large bearing surfaces. The hob spindle head carried by this slide may be set at any desired angle for cutting right- or left-



Bilton No. 10 Universal Gear-hobbing Machine

hand spirals. The hob spindle is driven through helical gears, and it may be adjusted lengthwise to relocate the hob if it should become dull in one place, without disturbing the adjustment of the spindle bearings. The work-table has a central hole 1% inch in diameter, so that teeth can be hobbed on the ends of shafts up to 1% inch diameter and 24 inches long. The table has deep oil-grooves with a drain running to the base of the machine where the oil reservoir is located. This reservoir is removable so that it can be cleaned. The hob speeds vary from 50 to 250 revolutions per minute and the range of hob feeds per revolution of the work is from 0.010 to 0.125 inch. The machine is driven through a three-step cone pulley designed for a 2½-inch belt. The net weight of the machine is 1100 pounds.

#### UNITED STATES ELECTRICAL GRINDER

The United States Electrical Tool Co., 6th Ave. and Mt. Hope St., Cincinnati, Ohio, is now building a combination wet and dry grinding machine that is electrically driven. This grinder is built in two sizes, with motors of three and five horsepower capacity. The machine equipped with a three-horsepower motor is arranged to carry two grinding wheels 12 inches in diameter by 2 inches face width, and the five-horsepower machine carries two grinding wheels 18 inches in diameter by 3 inches face width. These grinders are equipped with either direct-current motors for 110-, 220- or 550-volt circuits or alternating-current motors for 220-, 440- or 550-volt circuits of 25 or 60 cycle and two or three phase.

The bearings used in these machines are of the self-aligning ball bearing type, and the motors are built by the Westinghouse Electric & Mfg. Co. The grinding machine equipped with a three-horsepower motor weighs 575 pounds, and the



United States Electrical Grinder

machine equipped with a five-horsepower motor weighs 700 pounds. The speed of the grinding machine driven by a three-horsepower motor is 1800 revolutions per minute, and the machine driven by a five-horsepower motor runs at 1120 revolutions per minute.

#### NEW MACHINERY AND TOOLS NOTES

Plug Gages: Simplex Tool Co., Woonsocket, R. I. A standard line of hardened tool steel pluge gages varying by 1/32 inch from  $\frac{1}{8}$  to 1 inch in diameter.

Cutter Grinder: Elmer Sacrey, 1001 Diamond St., Philadelphia, Pa. A grinder for sharpening milling cutters up to 9 inches in diameter. The machine is equipped with a diamond wheel-truing device.

Pneumatic Hammer: H. Edsil Barr, Erie, Pa. This hammer strikes a maximum of 200 blows a minute and has a capacity for stock up to 2 inches square. The hammer is arranged to permit continuous striking.

Engine Lathe: Richard H. Kiddle, Kinsman, Ohio. Fourteen-inch engine lathe of cone pulley type, with beds varying from 4 to 10 feet in length. The swing over the carriage is 8% inches, and the weight, 1200 pounds.

Grinding and Polishing Stand: Lamb Knitting Machine Co., Chicopee Falls, Mass. A ball bearing grinding, polishing, and buffing machine. The head is separate from the base so that the machine may be used either as a bench or pedestal type.

Grinding and Buffing Stand: U. S. Electrical Mfg. Co., Los Angeles, Cal. This is a self-contained, motor-driven tool equipped with ball bearings that are sealed against dirt and grit. The machine may be supplied for bench mounting or with a pedestal.

Hydro-pneumatic Press: Metalwood Mfg. Co., Leib and Wight Sts., Detroit, Mich. A press for subjecting high-explosive and shrapnel shells to internal pressure. Presses of this type are built in various sizes with pressures ranging from 2000 to 21,000 pounds per square inch.

Bender for Ship Frames: Watson-Stillman Co., 192 Fulton St., New York City. Hydraulically-operated bender designed for bending heavy steel ship frames, deck beams, etc. The machine is mounted upon broad rollers so that it can be moved along the work when bending long parts to the shape of a templet.

Polishing Machine: Harvard Machine Co., Harvard Square, Cambridge, Mass. Polishing and lapping machine provided either with a No. 2 Morse taper spindle or with spring chucks for accommodating work up to ½ inch in diameter. These machines are intended especially for tool-room use in lapping bushings, plug gages, etc.

Pyromagnetic Indicator: Pyromagnetic Instrument Co., 175 N. Jefferson St., Chicago, Ill. An instrument of the magnetic type for determining the critical point when heating steel parts for hardening. One end of the instrument is energized and is placed in contact with the steel, which is heated until it becomes non-magnetic.

Universal Curveograph: W. G. Classon, Leominster, Mass. An instrument for the use of engineers and draftsmen, adapted for drawing simple, compound, reverse, and irregular curves. The spline or part for guiding the pen or pencil is held by adjustable fingers provided with graduations indicating the radius of curvature.

Automatic Threading Lathes: Automatic Machine Co., Bridgeport, Conn. These lathes operate on the same general principle as those formerly manufactured, but differ in some of the details. They are adapted for single or multiple thread cutting on either right- or left-hand screw threads. Forged tools or circular form cutters may be used.

Two-spindle Milling Machine: Newton Machine Tool Works, Inc., 23rd and Vine Sts., Philadelphia, Pa. A machine of the type having a horizontal planer type table equipped with two spindles, one being vertical and the other horizontal. The maximum height under the vertical spindle is 36 inches, and the width between the uprights, 42 inches.

Vertical Bending Rolls: Southwark Foundry & Machine Co., Philadelphia, Pa. A large bending roll for boiler plates having rolls which are vertical instead of horizontal. Two of the three rolls in the set are 22 inches in diameter, and the third roll is 30 inches in diameter. The driving motor and mechanism is located in a pit beneath the floor.

Cold Saw: Newton Machine Tool Works, Inc., 23rd and Vine Sts., Philadelphia, Pa. A cold metal-cutting saw for handling heavy structural steel sections. The machine is equipped with a 56-inch saw blade, but this may be increased to 62 inches in diameter if necessary. With the smaller blade the machine will handle rounds up to 16% inches, squares up to 15½ inches, and oblong sections up to 17 by 58 inches.

Power Shear: Buffalo Forge Co., Buffalo, N. Y. A line of power cut-off shearing machines. These shears are mounted on wheels to make them portable, and individual electric motor drive makes the entire machine self-contained. Four sizes of shears are built, the largest of which has a capacity for cutting flat bars up to  $1\frac{1}{8}$  by 5 inches, round stock up to  $1\frac{3}{4}$  inch in diameter, square stock up to  $1\frac{1}{2}$  inch, and angles up to 5 by 5 by 9/16 inch.

Spline Milling Attachment: Standard Engineering Works, Pawtucket, R. I. An attachment of the vertical type for use on hand and weight-fed milling machines. It is adapted for milling tang slots, feather keyways, etc. A cam operated by a ratchet gear controls the vertical movement of the cutter, and the spindle returns to an upright position automatically after reaching the proper depth. The horizontal travel is controlled by an automatic trip.

Sandblast Room: American Foundry Equipment Co., 52 Vanderbilt Ave., New York City. A compartment for the protection of the operator when sandblasting. The compartment or room has a circular table which extends beyond the enclosed part at the rear, so that it can be loaded while the work inside the compartment is being operated upon. The sandblast nozzle is inserted through a slit covered with rubber flaps, and the work may be seen through a fine brass screen.

Power Press Guard: G. H. Scott Machine Co., Cleveland, Ohio. This guard is entirely independent of the press treadle. Accidents due to repetition of the press are claimed to be impossible, and it is also stated that interference with the production of the machine is avoided, as well as accidents to the dies and the press. The guard is actuated by a cam and roller, and descends ahead of the ram, but the work is visible at all times and the operator has free use of his hands.

Dynamic Balancing Fixture: N. K. Akimoff, 1013 Harrison Bldg., Philadelphia, Pa. A fixture applied to an engine lathe for testing the dynamic balance of revolving machine parts. One end of the part to be tested is held in the chuck while the other rests on rollers having a yielding support. The position of an adjustable member is changed until an indicator dial shows that the part is in balance. The amount and location of excess metal to be removed by drilling is determined by reference to special tables.

Wire Nail Machines: Sleeper & Hartley, Inc., Worcester, Mass. Distinctive features of these machines consist of the employment of toggle joints actuated from a single crankshaft to provide the working motions, separation of the pointing and heading operations, and reduction in the size and weight of the machines and the floor space which they occupy. In operation, wire is taken from a coil and run through straightening rolls. During a single revolution the wire is fed forward to form the nail blank, the blank is cut off and the incoming end pointed. In the meantime the previously cut-off blank is headed.

### MR. SHIPLEY RETIRES FROM THE LODGE & SHIPLEY MACHINE TOOL CO.

Mr. Murray Shipley has sold his holdings in the Lodge & Shipley Machine Tool Co. of Cincinnati to Mrs. Lodge and her daughters, and given up all connection with that business. Mr. Shipley states that his retirement from the company does not necessarily indicate a permanent retirement from business, but rather a relief from the close attention which he has had to give to details for twenty-five years. Mr. Shipley has been identified with the concern since its establishment by Mr. Lodge and himself in August, 1892, and his activity in the machine tool business has covered a period of great progress and expansion in the industry, of which the Lodge & Shipley Machine Tool Co. has had its full share, starting from a small shop on Culvert St., from which it was moved to its present location, where the plant and business has steadily increased until it is now one of the largest and best known in the world. The new officers of the company are Mrs. M. G. Lodge, president; J. W. Carrel, vice-president and general manager; and L. A. Hall, secretary and treasurer. It is stated that the policy and organization of the company will continue on the same progressive lines as before. J. W. Carrel, the vice-president and general manager, has had many years of training and experience in the manufacture and sale of machine tools, having been connected with several well-known concerns before he became sales manager for the Lodge & Shipley Machine Tool Co. Mr. Carrel is widely known and highly regarded in the industry, and under his management the business will undoubtedly continue moving onward and upward.

#### RELIEVING ATTACHMENT FOR LATHE

The Phoenix Mfg. Co. of Eau Claire, Wis., has equipped one of its engine lathes with a simple attachment for relieving hobs, taps and various forms of milling cutters. It will be seen that this consists of a gear A mounted on the lathe spindle nose, from which power is transmitted to compound gears B, carried on a bracket at the back of the lathe. These compound gears may be changed to suit the cutter that is being relieved. Secured to the last gear of the compound train there is a cam C which has the same number of lobes as there are

flutes in the cutter. A roller mounted at the end of crank D runs in contact with cam C, and is secured to an eccentric shaft E mounted in bearings at the back of the lathe bed.

By disengaging the cross-feed screw in the lathe carriage, the cross-slide is left free and connection is made between it and the eccentric on shaft E by means of a connecting-rod F. It will be apparent that cam O and crank D impart an oscillating movement to eccentric shaft E, from which a corre-

sponding reciprocating movement is imparted to the crossslide on the carriage. In this way the necessary motion is obtained to give the cutter teeth the required relief. Different cams C and combinations of compound gears B are employed according to the type of cutter that is to be relieved. Cam Cmust, of course, have the same number of lobes as there are flutes in the cutter. Springs C hold the cross-slide so that all lost motion in the mechanism is taken up and accurate results are secured.

#### "COLLEGE OF THE MIDNIGHT LAMP"

BY GUY H. GARDNER 1

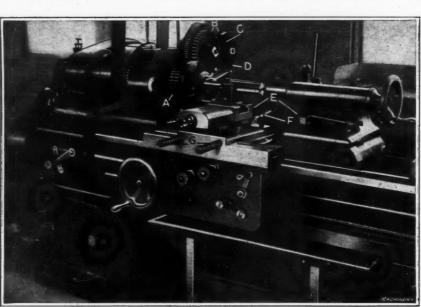
Though not wholly unfamiliar with other institutions of learning, I hold high opinions of the "College of the Midnight Lamp." Just now I have a small yarn to spin in regard to it. Last November a young apprentice wrote asking me to tell him how to find by a lay-out, as he knew no mathematics beyond long division, how far apart to place the tacks to draw an ellipse 8 by 12 inches. I learned subsequently that he wished to make a hole for an 8-inch stovepipe. In the last week of November he began the "midnight" study of plane geometry. In January of this year he began trigonometry. March 24, in response to his request for "something a little harder," I sent him a trigonometric problem which I have put before successive generations of high school and academy boys without finding one who could solve it. It is simple, but depends on the formula for the sine of twice an angle. My apprentice friend sent me the solution by return mail. Rah for the "College of the Midnight Lamp!" He is now working on the mathematics of gearing, and asks me to help him later with navigational astronomy, as he thinks "a man ought to have a hobby unconnected with his daily work."

His father writes that he has never seen so marvelous a transformation of character. No more loafing, no more "movies," just hard work, which is not hard because he loves it. That boy will amount to something. I could tell a dozen tales of men who have subscribed to Machinery to get rid of an importunate solicitor, and have undergone, in consequence, as complete a change of character as this youngster. Billy Sunday "has nothing on" Machinery as an agent of reformation.

#### GRINDING WHEEL BALANCE

Howard W. Dunbar calls attention to the need of perfect grinding wheel balance in *Grits and Grinds*, asserting that probably nine-tenths of all trouble with cylindrical grinding machines is caused by the efforts of the operator to obtain good work by tightening the boxes so as to prevent an out-of-balance wheel causing marks on the work. Out-of-balance

wheels set up vibrations throughout the whole machine, which cause chatter marks in the work; they are more likely to break than wheels in balance; they wear out the spindle boxes rapidly; and are more destructive to diamond truing tools, requiring more frequent dressing. Outof-balance wheels. therefore, are more expensive than wheels in balance because of more rapid wear and their deteriorating effect on grinding machinery.



Lathe Attachment for relieving Milling Cutters, Taps and Hobs

<sup>1</sup>Address: New London, N. H.

#### SPOT-FACING TOOLS

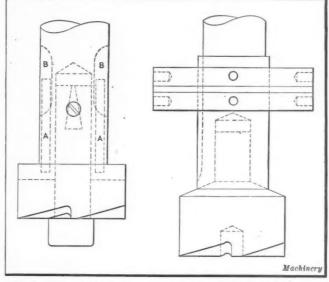
BY F. B. JACOBS 1

Spot-facing tools and counterbores are often spoken of as the same thing, but there is a slight difference between them. As a general thing, a spot-facing tool is used to finish off a surface, although it is sometimes used to counterbore a hole slightly. On the other hand, a counterbore is generally used for counterboring comparatively deep work and sometimes for enlarging a hole that has been drilled, particularly when several holes are so near together that they break into each other. There are many varieties of spot-facing tools, but this article will be confined to some of the more simple forms that have been found efficient in everyday work, especially in the automobile industry.

The simplest form of spot-facing tool is shown in Fig. 4. This consists of a bar of the requisite length having a hole drilled and reamed near the bottom to accommodate the cutter, which is held in place by a set-screw. Owing to the ease with which it is made, this tool is a favorite with those employed on experimental work, who often have occasion to face off several bosses of different sizes. If the tool is of medium size, say with a one-inch shank, it can be made by a machinist

in about one hour. The only feature calling for any degree of accuracy is the angle made by the shank and the bar, which should be 90 degrees. This tool is comparatively short-lived, as it has only one cutting edge, but when only a few holes are to be spot-faced it serves the purpose as well as some of the more elaborate and costly forms.

A more substantial form of spot-facing tool is illustrated in Fig. 5. This consists of a shank to which the cutter, which closely resembles a hollowmill, is fastened by means of a cone-



Tool for spot-facing drilled and reamed in a Jig

point set-screw. The

teeth terminate in a

liberal fillet and the

angle is compara-

tively slight. This

is essential on rapid

production work.

where tools are

worked to the lim-

it to avoid undue

breakage. The pilot

can be protected

from undue wear by

casehardening, if ma-

chine steel is used.

Boiling in evanide for

fifteen minutes will

produce a case deep

enough to withstand

several weeks of con-

stant use. The cut-

ter should be made

of high-speed steel if

the material to be

machined is cast iron

or steel: for brass

and aluminum, how-

Fig. 1. Spot-facing Tool with Interchangeable Cutter

Fig. 2. Convenient Form of Spot-facing Tool for Small Sizes

Fig. 3. Spot-facing Tool in which Cutter is driven by Projections on Shank

Address: 435 Harvard Place, Indianapolis, Ind.

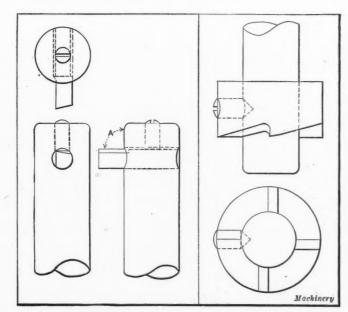


Fig. 4. Simplest Form of Spot-facing Tool

Fig. 5. Rapid-production Spot-facing Tool

ever ordinary tool steel may be used, especially since the war has forced the price of high-speed steel to an almost prohibitive mark. If an accurate face is desired, the hole in the cutter should be finished after hardening by grinding or lapping, and the teeth should be backed off by locating the piece from the hole. If only a fair degree of accuracy is called for, however, the teeth can be backed off with a file before hardening, and in this case no grinding is necessary until the teeth become dull through use.

Occasionally, it is convenient to have spot-facing tools that are interchangeable, as shown in Fig. 1. Here the shank is drilled and reamed to accommodate the pilot, which is held in place by a set-screw, while the cutter is fastened to the shank by another set-screw. By providing several pilots and cutters, quite a variety of work can be taken care of without making complete tools for each hole. The shank can be left soft, but the cutters and pilots should be finished by grinding after hardening. It is not necessary to make the pilots of tool steel, as ordinary machine steel, casehardened by packing in bone dust, gives equally good results. The tool shown in Fig. 2 has a removable pilot, but inasmuch as the shank and cutter are made integral it is an expensive form of construction. For small sizes, however, say one inch in diameter and smaller, this form is often used. In sharpening, the pilot is removed and the tool is located by the shank.

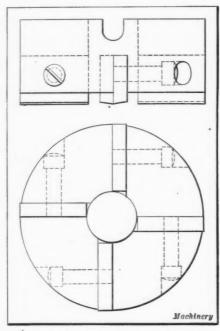


Fig. 8. Spot-facing Tool with Inserted Teeth

A good design is illustrated in Fig. 3. The pilot locates the cutter, being fastened by a set-screw, while the strain of driving is taken by two projections, milled on the end of the shank, which fit a slot in the top of the cutter. This is a practical form of tool if properly made. As the illustration shows, the slot in the top of the cutter terminates in a halfround section: this form is essential, for a sharp corner at this point would be very likely to result in a fracture.

A unique form of spot-facing tool is shown in Fig. 6. The cutter is driven by two pins A that are a driving fit in the shank. Slots B are milled with a Woodruff key cutter for the purpose of driving out the pins when necessary. When the pins shear off, which sometimes happens, all that is necessary is to remove the pieces that have been cut off and drive the pins down slightly; the cutter is then ready for use. With the form shown in Fig. 3, it would be necessary to remill the end of the shank, which would take at least an hour's time, whereas with the pin design the operator can repair the damage in a few minutes. For this reason the pin form of tool is extensively used.

Comparatively large spot-facing tools, from two inches in diameter upward, are often made with inserted teeth as shown in Fig. 8. The cutter-head can be made of machine steel while the cutters can be of either tool or high-speed steel according to the nature of the work. The cutters are held in place by fillister-head screws. As the cutters seat firmly on the bottoms of the slots provided for them, one screw suffices to hold each cutter in place. The wear on the cutter-head is slight, and it should last indefinitely; when the cutters have been ground until they have become useless, they can be replaced at slight cost.

It is often advisable to spot-face surfaces on work that is drilled and reamed in a jig, in which case it is a good plan to dispense with the pilot, guiding the tool by means of a supplementary bushing inserted in the jacket bushing. As shown in Fig. 7, the cutter is held to the shank by means of a coarse-threaded screw machined to fit rather loosely, as the tool is centered by the bevel. The two collars are threaded to the shank and are for the purpose of adjusting the depth of cut as occasion requires; as they bear on the top of the bushing they should be hardened and ground true. A cutter of this kind could, of course, be guided by a pilot, but as spotfacing tools are generally broken by the pilot galling up it is a good plan to eliminate this feature when possible. In order to save the expense of an extra bushing, these tools are sometimes run directly in the jacket bushing, but this is poor economy, as the bushing is soon worn oversize, and the accuracy of the jig is impaired. The tools described are among the simple things that are often lacking, even in many well organized shops, but a little attention to simple tools often leads to efficient results, thus aiding materially in cutting down the cost of production.

In order to prevent the misappropriation of foreign trademarks, the president of Costa Rica has ordered that no trademark that is well known in the country, because of the advertising or the sale of the trademarked articles, shall be registered unless authority to apply for such registration is proved.

#### THE GRINDING WHEEL

The electrochemist speaks of the abrasive wheel and the automobile manufacturer of the emery wheel, but the manufacturer thinks that neither of these words adequately describes his product, and so has adopted the term "grinding wheel." This term is here restricted to those wheels that are composed of two main constituents: the abrasive and the bond, or the substance that holds the particles of abrasive together. The commercial method of classifying grinding wheels is by the kind of bonding material used.

The most important type is the vitrified wheel. The bonding material in this type is composed of various kinds of clay mixed according to definite, secret formulas. Weighed amounts of the abrasive and the bond and a measured amount of water are stirred together in a mixing kettle for a certain length of time and then the mixture is drawn off from the bottom of the kettles into molds and allowed to dry. When dried, the wheels are taken to the shaving department, where they are turned to the approximate dimensions and shape called for by the order.

A kind of vitrified wheel, known as pressed wheel, is made by the pressed process. In this case, only enough water is added to the bonding clays to make the particles stick together to a slight degree. The abrasive and bond are mixed in kneading machines and are then placed in an iron mold and subjected to pressure by powerful hydraulic presses. The pressure applied depends on the grade of hardness desired. These wheels do not need shaving. The next operation is the heat-treatment, in which the wheels are subjected to a heat that will properly vitrify and mature the bond; the highest temperature reached is about the melting point of steel. The length of time required for heating, the length of time during which the wheel is subject to high heat, and the cooling period must be carefully controlled.

In silicate wheels, the bonding material is a commercial grade of silicate of soda, commonly known as water-glass, to which certain chemicals are added to make the bond water-proof. A weighed amount of the grain and a measured amount of the bonding material are placed in long cylinders, which are slowly revolved, end for end, until a uniform mixture is obtained. The mixed mass is placed in an iron mold of the approximate dimensions called for by the order and rammed into place by hand or air hammers. The wheel is then baked.

The name elastic wheel is derived from the fact that the bonding material has quite a degree of elasticity. The bond is of organic nature, the most satisfactory material being shellac, to which certain chemicals are added to facilitate hardening in the baking and also to make the wheel waterproof. Weighed amounts of the grain and the bond are thoroughly mixed and then dumped into large shallow pans and allowed to cool, thus becoming brittle. This brittle cake of abrasive and bond is broken into small pieces and then put through rolls that break the mass into the individual grain. The rolls do not fit close enough, however, to reduce the size of the grain, the idea simply being to produce a mass composed of loose grains, each of which has a coating of shellac. The material is then placed in an iron mold the approximate shape of the wheel, heated and then subjected to pressure. The amount of pressure depends on the degree of hardness desired. The mold and mass are again placed in a steam box and heated until the bond becomes permanently hard.

In vulcanized wheels, the bonding material is rubber, and their manufacture is practically like that of any other hard-rubber product. A weighed amount of the very best grade of crude rubber, the right proportion of sulphur, and a weighed amount of grain are thoroughly mixed by numerous passes in a vertical direction. After a uniform mixture is obtained, the mass is passed through a set of rolls that passes the material in a horizontal direction. It is then rolled down to the required thickness, cut to the required diameter, and a hole of the required diameter is cut in the center. The next operation is vulcanizing, which does not differ from the vulcanizing of any other rubber product.

<sup>&</sup>lt;sup>1</sup>Abstract of a paper by R. G. Williams read before the American Electrochemical Society, in Detroit, May, 1917.

The next operation in the making of the wheels is that of truing, or bringing the wheels to the dimensions called for on the order. The wheels are mounted in a three-jaw chuck, revolved, and special tools resembling an emery-wheel dresser are brought up against the side of the wheel. In order to bring the wheels to the desired diameter, they are firmly held on a revolving arbor and the dressing tool passed back and forth across the face, gradually reducing the wheel to the desired size. For fine wheels that must be carefully shaped on the face, a diamond is securely mounted in a fixture and slowly passed across the face of the wheel. Light cuts only are taken so as not to crack and destroy the diamond.

The bushing, as it is termed, consists of lead or a babbitt. The wheel is allowed to rest on its side in a three-jaw chuck and is carefully centered; then a steel arbor from 0.002 to 0.005 inch larger than the desired hole in the wheel is placed in the center hole in the chuck and the lead poured around the arbor. When the lead has solidified, the wheel is removed from the chuck and the arbor is carefully driven out with a soft hammer. The bushing is then trimmed, so that it is not quite flush with the sides of the wheel; this is to provide clearance so that when the wheel is mounted on the machine there will be no possibility of stress being concentrated at the hole of the wheel.

In the next operation, the speed test, the wheel is revolved at a speed higher than that recommended for its operation, in order that the manufacturer may know that his product goes out with a sufficient factor of safety. The testing speed for wheels is 9000 surface feet per minute, except for those of organic bonds, when the test speed is higher. Since wheels are recommended to operate at about 5000 surface feet per minute, this gives a factor of safety, based on the squares of these speeds, of between 3 and 4. A careful record of every test is kept; and before these records are filed, the men that keep them are required to appear before a justice of the peace and swear that their statements are true.

#### Grinding Characteristics of Various Abrasives

Probably the most important physical property of an abrasive is hardness. Other properties, such as toughness and ability to resist shock, are also important, but knowledge of the art of grinding has not advanced sufficiently for us to state definitely the relative importance of the different physical characteristics; that is, we cannot state on which of the properties the grinding action of the abrasive most depends. It is known that the artificial abrasives are harder than corundum but not so hard as diamond. It is hard to determine differences in the hardness of artificial abrasives, although it is known that carbide-of-silicon abrasives are harder than aluminous abrasives

When a grinding wheel containing a certain abrasive satisfactorily grinds very tough material, it is said to possess considerable toughness. Actual experience has shown that when materials of low tensile strength, such as cast iron, brass, bronze, etc., are ground, carbide of silicon, which is hard but relatively weak, is more efficient than aluminous abrasives. On the other hand, when grinding materials of high tensile strength, ranging all the way from medium carbon to the high-speed steels, aluminous abrasives give better satisfaction.

#### Precision Grinding Machines

The word "precision" is used to designate a type of grinding machine, because these machines must be capable of producing work of great accuracy. The art of precision grinding has advanced rapidly during the past few years and the demand of the automobile manufacturer should receive credit for producing most of the advance. Only a few years ago anyone advocating the accurate grinding of shafts five or six inches long without table or wheel traverse would have been condemned as too visionary; this step in the art has long since been passed. It is now possible to grind more than one diameter at one time with one wheel; this is an outgrowth of the use of very wide wheels taking extreme cuts without any traverse of the table or the wheel.

A machine using a very wide wheel, say ten or twelve inches, must be very rigid as well as capable of producing re-

fined work. Imagine the forces present when a wheel weighing 150 or 200 pounds revolves on a spindle, in plain bearings, at 1000 to 1200 revolutions per minute. This spindle must be kept in perfect alignment so that the face of the grinding wheel will produce an absolutely straight cylinder, and there must be ample weight in the base of the machine and in the wheel-slide to absorb all vibration caused by the revolving mass. Another factor that must be borne in mind is the resistance offered when the wheel is brought in contact with the work, as small particles of a very hard material are removed at an extremely rapid rate. The spindle bearings must be so adjusted that the boxes will be quite hot when the machine is in operation; in fact, a temperature of about 140 degrees F. is desirable.

Limits of 0.0005 inch on the work being ground are very common; those of 0.00025 inch are quite common; and in some cases less than 0.00025 inch is demanded. When the work is reduced 0.00025 inch, the massive slide carrying the wheelspindle and the grinding wheel moves forward only one-half this distance, or 0.000125 inch. If it were possible to split a piece of tissue paper into twelve thicknesses, the thickness of one piece would represent the motion of the wheel-slide when the grinding wheel removes 0.00025 inch from the work, and this accuracy must be maintained not only where very small cuts are taken, but also when the object is to grind off as many cubic inches per minute as possible.

#### CONFERENCE WITH GOV. WHITMAN

A conference between Governor Whitman of New York State and trade press editors and publishers was held in Albany, July 25, at the Executive Mansion. The conference is likely to have bearing on some of the relations of the state executive to the various industries represented. Questions of transportation, food control, marketing, conservation of coal and lumber, relations of manufacturers and labor, the importance of exempting machinists and toolmakers and others vitally necessary to the prosecution of this war with machinery, were discussed at some length. A committee of five editors has been appointed to give Governor Whitman the expert advice they are able to furnish because of personal knowledge and connections that enable them to draw from sources of information which may be of service in the prosecution of war.

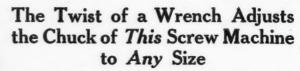
The new color scheme of signal indications, by which white lights will be eliminated altogether, was placed in effect on all lines of the Pennsylvania Railroad east of Pittsburg, June 28. Nearly a year of preparatory work was required to make the change possible. Great difficulty was experienced in obtaining deliveries of materials, owing to the war conditions. The decision to eliminate white from the signal color scheme was reached on account of the increasing use of white lights in buildings, driveways, roads and streets close or adjacent to the railroad's right-of-way. Under the new plan, green will replace white for "clear" or "proceed." "Caution" will be indicated by yellow. Red will mean "stop," as heretofore. The glasses in all the semaphore signals and the following devices have been altered to conform to the new plan of color indication: marker lights on the rear of passenger and freight trains; switch lamps and targets; markers for track tanks; "slow" signs; "resume speed" signs; and hand lamps at interlocking and block signal stations.

An elaborate electrical sign has recently been erected by the Rice Leaders of the World Association in a prominent position overlooking upper Broadway in New York City. The firms in the machinery and tool field whose products are advertised by flashes on this sign are the Billings & Spencer Co., Hartford, Conn.; the Nicholson File Co., Providence, R. I.; and the L. S. Starrett Co., Athol, Mass. The names and products of the various firms that are members of the Rice Leaders of the World Association are flashed upon the sign in rapid succession. The upper part of the sign is composed of the elaborate coat-of-arms or emblem of the Association in colors.



# "BROWN&SHARPE

For Steady, Fast,



Not only does this feature of B & S Nos. 4 and 6 Wire Feed Screw Machines make a material saving on the first cost, but saves time as well as dollars throughout their years of efficient service because no time is lost in adjusting special chucks or in searching for collets.

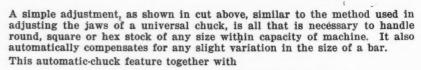
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#### Three-lever Centralized Control

practically eliminates all lost motions.

After tools are set chuck is opened and stock advanced by the slight throw of a handy lever. The return of this lever to its original position closes and locks the chuck.

A second lever, also on the headstock, is employed for starting, stopping and changing speeds while the simple movement of a third lever, close by, changes feed of turret slide in conjunction with a lever just behind the pilot wheel of turret slide which is manipulated with the right hand in connection with the handling of pilot wheel to bring tools up to cut.

Other reasons why your bar work should be handled on these machines—reasons that spell economy and increased production—are explained in detail in our Catalog 21-G. Your request will bring a copy.

# Brown & Sharpe Mfg. Co.,

HANDINESS-An Attribute of Every B & S Product

EQUIPPED"

Quality Production

#### An Increase in Production and Quality With a Corresponding Decrease in the Scrap Heap

naturally follows the use of Brown & Sharpe Tools. The confidence that encourages competence is inspired by the use of these handy, accurate tools and is soon reflected in the high degree of efficiency their use promotes.

Numbering over a thousand different varieties, they

# Cover Thoroughly Every Precision - Tool Requirement

and represent a development covering over half a century.

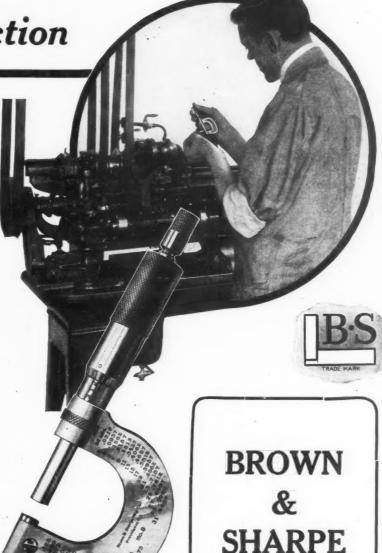
Practically every variety of measuring tool is used in our own shops in the manufacture of our extensive line of machinery, and our small-tool designers have worked with the advantage of first-hand information as to the needs of the man in the shop.

Every care is taken that the highest quality of workmanship be maintained, resulting in a line of machinists' tools that is worldknown for its uniform quality. Not only the kits of your toolmakers and machinists but

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#### LESSONS FROM BRITISH EXPERIENCE

In 1915, the British Minister of Munitions appointed a committee to consider and advise on questions of industrial fatigue, hours of labor, and other matters affecting the personal health and physical efficiency of workers in munition factories and workshops. This committee, after making a careful investigation, has made the following suggestions and recommendations with the purpose of securing maximum output over a period of months, or even years, and at the same time safeguarding the physical efficiency of the workers:

If the maximum output is to be secured and maintained for any length of time, a weekly rest period must be allowed. Except for short periods, continuous work is a mistake and does not increase the output. On economic and social grounds, this weekly rest period is best provided on Sunday. The foremen and the higher management even more certainly require definite periods of rest. They have never spared themselves; they carry a heavy burden of responsibility and cannot be replaced. It is of primary importance, in the interests of the nation, that they should be allowed that rest which is essential to the maintenance of their health.

The objections to overtime, briefly stated, are: It is likely to impose too severe a strain upon the workers, which adversely affects the rate of production and quality of output during the whole period of work as well as during the hours of overtime. It frequently results in a large amount of lost time, which is attributed to the workers becoming exhausted and taking a rest, and also to sickness. It imposes a serious strain upon the management, the executive staff, and foremen, since these persons cannot take days off like the ordinary worker. It is likely to curtail unduly the period of rest and sleep available for those who have to travel long distances to and from work, a matter of special importance in the case of young persons. The fatigue entailed increases the temptation to indulge in the consumption of alcohol.

Admitting that overtime must continue, for adult male workers the average weekly hours (exclusive of meals) should not exceed 65 to 67, including overtime. It may be desirable to differentiate to some extent between different kinds of work and to fix a rather low limit of hours for work requiring close individual attention. Where practicable, the overtime should be concentrated within three or four days in the week, which should preferably not be consecutive. Where overtime is necessary, it is specially important that there should be no Sunday work. The committee feels that the need for overtime among

women and girls is much less pressing than it is for men, and should be abandoned in favor of shifts.

Although work on shifts involves night work, night work is not a good thing in itself because it is uneconomical. Though wages are paid at a higher rate, the rate of output, more particularly during the last two or three hours of a twelve-hour shift, is generally lower. Supervision is frequently unsatisfactory. Conditions of lighting are seldom as good as in the daytime and make fine work more difficult. Workers experience great difficulty in sleeping by day. The unfamiliar meal hour makes it difficult for the workers to consume substantial food, and digestion is likely to be upset.

As a method of speeding up production, the committee recommends the careful regulation of rest periods. It has been found that the operatives, if left to themselves, take rests at irregular and often unsuitable times; hence it is much better for the rest periods to be chosen for them. For instance, a ten-minute period in the middle of the morning and the afternoon, during which the operatives remain at their machines, but have tea or other nutriment brought them by boys or by traveling canteens, has been found a valuable aid to output. Some kinds of work need longer and more frequent rest periods than others; this is determined only by experience.

The committee found that the munition workers, in general, have been allowed to reach a state of reduced efficiency and lowered health, which might have been avoided without reduction of output by attention to the details of daily and weekly rests. The signs of fatigue are even more noticeable in the case of managers and foremen.

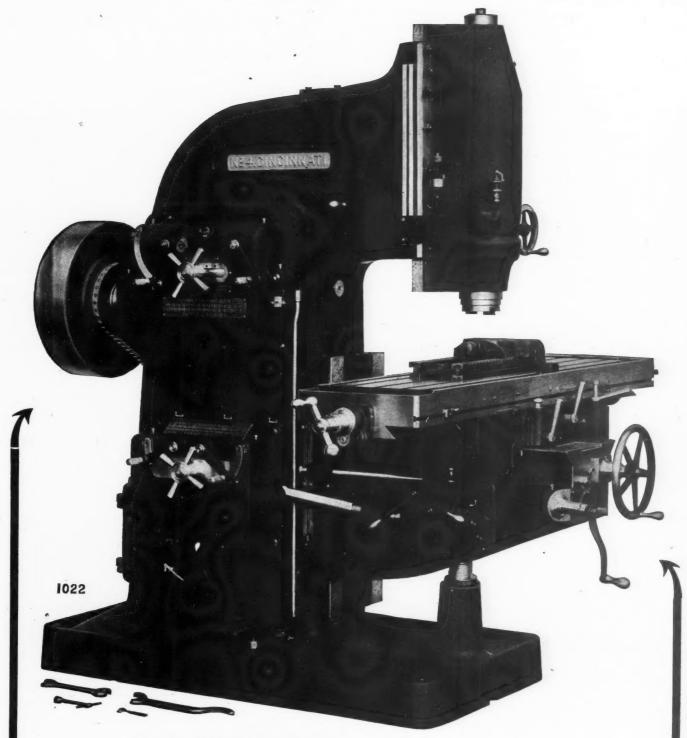
The committee calls attention to the fact that bad lighting affects output unfavorably by making good and rapid work difficult, and also by causing headaches and other effects of eyestrain. The difficulties of supervision are further increased. The essentials of good lighting are: adequacy: a reasonable degree of constancy and uniformity of illumination over the necessary area of work; the placing or shading of lamps so that light does not fall directly on the eye of the operator when engaged at his work or when looking horizontally across the work-room; the placing of lights so as to avoid the casting of extraneous shadows on the work. The committee also calls attention to the need of special measures to prevent undue strain upon the eyesight or to reduce the liability to accidents to a minimum. It suggests that the eyesight of operatives employed on close work be tested and the persons supplied with glasses when necessary; it also suggests guarding the eyes by the use of goggles.



Assembling, erecting and testing Ott No. 1 Universal Grinding Machines

The illustration shows the floor of the Ott Grinder Co. in the Industrial Building, Indianapolis, Ind. The view is of interest, as it gives an idea of the rapid development of one comparatively small manufacturer who started a few months ago to build the line of cylindrical grinding machines acquired by purchase from the Modern Tool Co. of Erie, Pa. The growth of the business reflects the fact that the cylindrical grinding machine is no longer regarded as a refinement for the use of toolmakers only, but is rapidly becoming an indispensable machine tool to many concerns that found no use for it in their machine shops a few years ago. The view shows thirty No. 1 universal grinding machines in the various stages of assembling, erecting and final testing under belt. These are part of fifty machines put through in one lot. The first machine in the front row is being tested for accuracy, a Brown & Sharpe indicator being used for testing the alignment of both wheel-spindle and headstock.

# Cincinnati Verticals



Unusual Spindle Power.
Heat Treated Alloy Steel Hardened Gearing.
Massive Spindle Head Construction.
Handy—Can mill around a rectangle without stopping feed or speed.

These are some reasons why you should use Cincinnati Verticals

THE CINCINNATI MILLING MACHINE CO. CINCINNATI, OHIO, U. S. A.

#### PERSONALS

B. H. Blood has been appointed general manager of the Pratt & Whitney Co., Hartford, Conn., following the resignation of B. M. W. Hanson.

L. A. Larsen was appointed comptroller, effective July 1, at a recent meeting of the board of directors of the American Locomotive Co., New York City.

B. Orum Andresen has joined the engineering staff of Aall & Co., of Tokyo, Japan, the Japanese agents for the American Steel Export Co., Woolworth Bldg., New York City.

Charles H. Purdy, superintendent of the Dalton Machine Co. of New York City, has resigned to engage in the designing and building of special machinery, with offices at 103 E. 125th St., New York City.

H. L. Paulus, R. G. Ferguson, and F. L. Graf, for many years connected with the Baird Machinery Co., of Pittsburg, Pa., have resigned and joined forces with the J. S. Miller Machinery Co., of Pittsburg.

B. M. W. Hanson, general manager of the Pratt & Whitney Co., Hartford, Conn., has resigned, and has been made vice-president and general manager of Colt's Patent Fire Arms Mfg. Co. of Hartford.

Albert P. Weigel, superintendent and general manager of the Superior Machine Tool Co., Kokomo, Ind., has resigned and organized the Weigel Machine Tool Co., Peru, Ind., to

Edgar N. Dollin, organizer and president of the Acme Die-Casting Corporation, Brooklyn, N. Y., has sold his holdings in the company and retired from active management. Mr. Dollin was formerly secretary of the Doehler Die-Casting Co., and president of the Kalak Water Co. He has had a wide business experience as a lawyer and as a manufacturer. His new activities have not been expensed. new activities have not been announced.

R. M. Klein has been appointed sales manager of the International Oxygen Co., with headquarters at the company's main office at 115 Broadway, New York City. Mr. Klein brings to his new position technical training, and experience as an engineer in the United States government employ, as salesman and sales manager of the Diehl Mfg. Co., and as manufacturers' representative handling a number of mechanical lines

R. J. Doty, who for the last three and one-half years has R. J. Doty, who for the last three and one-hair years has been in charge of the steel foundry of the Isaac Johnson Co., Spuyten Duyvil, N. Y., has resigned his position to become associated with the Sivyer Steel Casting Co., Milwaukee, Wis. The company is enlarging its plant and installing an additional three-ton electric furnace to take care of its growing business among the motor truck, tractor, and general machinery manufacturers.

George A. Willard, for many years a manufacturer of lathes in Cincinnati, Ohio, has sold the Willard Machine & Tool Co. to G. Mattman and Thomas L. Bratten. Mr. Mattman was formerly European representative of the Cincinnati Milling Machine Co., and Mr. Bratten held an executive position with the Employers' Liability Corporation, and is well known in the trade. Mr. Willard will retire from business and take a much needed rest at his summer home in Michigan.

F. H. Tackaberry, general agent of the American Steel Export Co., Woolworth Bldg., New York City, sailed July 7 for South America. Mr. Tackaberry will visit the principal South American cities—Rio de Janeiro, Sao Paulo, Buenos Aires, Montevideo, La Plata, Rosario, Valparaiso, Santiago, etc., his object being primarily to collaborate with the company's factorist them with the market conditions in tory agents and acquaint them with the market conditions in the United States for iron and steel and engineering and con-

#### OBITUARIES

H. C. Mather, president of the Moore Oil Co., Cincinnati, Ohio, was drowned June 26 in Lake Superior near Calumet, Mich.

Casimir von Philp died July 5 at Ocean City, N. J., aged sixty-four years. He was born in Sweden, but came to the United States nearly forty years ago. Since 1890, he was connected with the Bethlehem Steel Co., at Bethlehem, Pa., for a considerable period as chief engineer and recently as manager of the machinery department. As an engineer, his career was marked by unusual ability and originality. His inventions included improvements in rolling mills and special features of heavy forging equipment produced at the Bethlehem works. He was a member of the American Society of Mechanical Engineers, the American Society of Swedish Engineers, and the Engineers' Club of New York. He was also recently appointed a member of the John Ericsson Memorial Commission. considerable period as chief engineer and recently as manager

#### COMING EVENTS

August 30—Monthly meeting of the Rochester So-ety of Technical Draftsmen, in Rooms 131-137, thley Block, 328 Main St., E., Rochester, N. Y. I. Angevine, Jr., secretary, 857 Genesee St.,

August 30-September 1—Ninth annual convention of the American Railway Tool Foreman's Association, Chicago, Ill.; Sherman Hotel, headquarters. C. N. Thulin, secretary-treasurer, 935 Peoples Gas Bldg., Chicago, Ill.

September 10-15—Annual convention of the National Safety Council, New York City; Hotel Astor, headquarters. Marcus A. Dow, president, Grand Central Station, New York City.

September 10-15—Exposition of safety appliances at the Grand Central Palace, New York City, under the auspices of the American Museum of Safety, 18 W. 24th St., New York City. Arthur H. Young, director.

September 25-28—Twenty-second meeting of the American Foundrymen's Association, Boston, Mass.; Copley-Plaza Hotel, headquarters. The registration booth will be in the Mechanics' Bldg., where the exhibition of foundry and machine shop equipment and supplies will be held. A. O. Backert, secretary-treasurer, 12th and Chestnut Sts., Cleveland, Ohio.

September 27-29—Informal congress and reunion of American and Canadian engineers and architects of Norwegian birth or descent in Chicago at Chicago Norske Klub, 2346 N. Kedzie Blvd., Logan Square Chicago, Ill.

#### SOCIETIES, SCHOOLS AND COLLEGES

Brown University, Providence, R. I. Circular on ie new course in engineering containing illustra-ons of the laboratory equipment and statement if the requirements for the degree of bachelor of of the he requirements f ice in engineering

Polytechnic Institute of Brooklyn, Brooklyn, N. Y. Pamphlet outlining the evening courses offered by the institute in engineering, chemistry, physics, mathematics, drawing, history, economics and languages. The season 1917-1918 begins October 1 and continues until the courses are completed.

Y. M. C. A. Industrial Department, 124 E. 28th t., New York City. Pamphlet outlining the or-

ganized industrial extension work undertaken by the City Association Among Industrial Workers for the benefit of workers in factories and shops throughout the country. The work comprises edu-cational, social, physical, religious and general activities.

activities.

Electric Power Club at its annual meeting held in Washington, D. C., June 11-12, elected C. L. Collens, of the Reliance Electric & Engineering Co., president; F. S. Hunting, of the Fort Wayne Works of the General Electric Co., vice-president; and C. H. Roth, of Roth Bros. & Co., secretary-treasurer, a resolution tendering to the government the use of the manufacturing plants of the members and offering the services of the committees was passed.

#### NEW BOOKS AND PAMPHLETS

Constitution of the United Nations of the Earth. By Edgar D. Brinkerhoff. 22 pages, 6 by 9 inches. Published by the Pamphlet Publishing Co., Fall River, Mass.

This remarkable document is virtually a para-phrase of the Constitution of the United States adapted for the united nations of the earth as visioned by the author.

visioned by the author.

Oxy.acetylene Welding Practice. By Robert J. Kehl.

105 pages, 5½ by 8½ inches; 111 illustrations.
Published by the American Technical Society,
Chicago, Ill. Price, \$1.

The work is a practical presentation of the processes of welding, cutting and lead burning, with special attention to welding practice for steel, cast iron, aluminum, copper and brass. It is illustrated with many examples showing how to handle the torch and to prepare work for welding. Examples of automobile repair are included, thus making the work of special interest to owners of garages and others concerned with motor car repairs.

How to Make High-pressure Transformers. By F. E. Austin. 46 pages, 4½ by 7½ inches; 21 illustrations. Second edition. Published by Prof. F. E. Austin, Box 441, Hanover, N. H. Price, 65 cents.

Price, 65 cents.

The first edition of this book was published in 1914. It is essentially a work on experimental electrical engineering written with regard to the well-known fact that to learn things we must do things. The student is instructed in the theory of high-pressure transformer design by designing and making a transformer. The work is both practical and technical, but not too highly technical to place it beyond the comprehension of men having a good high school education. It contains data

that should be of use to engineers who wish to brush up on the principles of electrical engineering. Machine Drawing. By Ralph W. Hills. 22 pages, 6 by 9 inches; 119 illustrations. Published by the McGraw-Hill Book Co., New York City.

Some desired and some d

9 inches; 274 illustrations. Fublished by an Nostrand Co., New York City. Price, \$3 net.

This work is, we believe, the first special treatise on valves, valve gears and valve setting published which may be recommended to railway mechanics as a practical guide for locomotive valve setting and a treatise on the common and uncommon types of valve gears. It explains the construction and action of the plain slide valve, the piston valve, and the valve gears used to operate them, as applied to locomotives, and is based on notes used in schools for apprentices on the Pennsylvania Railroad. The authors state in the preface that the book had been prepared to meet the general desire among railroad shop men to acquaint themselves with the valves and valve gears applied to modern locomotives, and to master the principles of valve motion as a preparation to valve setting. Valve motion and valve setting have always appeared to many shop men as more or less of a mystery, and it is the aim of the work to enable those interested to acquire first-hand knowledge. The subject matter is given in seven chapters, the contents of which are as follows: Locomotive Valves and Valve Gear; Stephenson Valve Gear; Walschaerts Valve Gear; Baker Locomotive Valve Gear—Joy Valve Gear—Southern Locomotive Valve, Valve Gear, and Reverse Gear—Gooch Stationary Link—Allen Valve Gear—Effects of Altering the Valve and Its Events; Locomotive Valve Setting; Steam Engine

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Indicator and the Indicator Diagram. The illustra-tions and directions for valve setting leave little to the imagination, the steps pursued by the practical valve setter in securing the data required for ad-justment of the eccentrics and eccentric rods being clearly and specifically described. The book is one that we heartily recommend to all railway students and others interested in locomotive valve motion.

#### NEW CATALOGUES AND CIRCULARS

Warner Hammer Co., Cromwell, Conn. Price list Warner hammers and edge tools.

Metalwood Mfg. Co., Detroit, Mich. Bulletin of the Metalwood inverted type adjustable for Bulletin B-44 No. 121.

press, No. 121.

Metalwood Mfg Co., Detroit, Mich. Circular B-53 of the Metalwood No. 79 hydro-mechanical banding press for banding shells from 3 to 5 inches.

Standard Alloys Co., Pittsburg, Pa. Pamphlet entitled "Uranium in Steel," presenting comparative tests of uranium and other high-speed steels.

Day & Zimmermann, Inc., Philadelphia, Pa., has issued a bulletin showing typical industrial plants throughout the country constructed by this company.

Link-Belt Co., Chicago, Ill. Book 258 entitled "The Ideal Drive for Textile Machinery," illustrating Link-Belt silent chain installations in textile

Cummings Ship Instrument Works, Boston, Mass. Bulletin descriptive of the Gary-Cummings torsion meter for determining the horsepower transmitted by shafts.

Hisey-Wolf Machine Co., Cincinnati, Ohio, Bulle-tin 1403, describing "Hisey" portable electric surface grinders, made for use with either direct or alter-nating current.

Oakley Chemical Co., 26 Thames St., New York ity. Information sheet 857 on munitions manu-neture, illustrating uses of "Oakite" cleaning and

Stanley Belting Corporation, 32-40 S. Clinton St., Chicago, Ill. Circular of Stanley woven cotton belting, made in single, double and triple thicknesses and in all widths up to forty-two inches.

nesses and in all widths up to torty-two unenes.

Peter A. Frasse & Co., Inc., 417 Canal St., New
York City. July stock list giving sizes in stock
ready for immediate shipment of Frasse electric
tool steel, drill rods, steel shafting and strip steel.

Messer Mfg. Co., 117-121 N. 7th St., Philadelphia, Pa. Catalogue of Messer portable oxyacetylene apparatus for welding and cutting; regulating valves, welding blow-pipes and acetylene
generators.

Nagle Corliss Engine Works, Erie, Pa. Bulletin 27, illustrating and describing Nagle-Corliss Class A-E and B-E steam- and power-driven air compressors with capacities from 3 to 8000 cubic feet of free air per minute.

Sunderland Machinery & Supply Co., 1006-1010 Douglas St., Omaha, Neb. Circular of the Fox arbor press No. 4, having capacity for work 19 inches diameter. The movement of the ram is 17½ inches and the leverage 60 to 1.

Sprague Electric Works of General Electric Co 527-531 W. 34th St., New York City. Bulleti 48923 of Type W, one- to six-ton electric hoist giving specifications, dimensions, and weights, an showing a few uses of standard Type W hoists.

Whitman & Barnes Mfg. Co., Akron, Ohio. Catalogue 90, 158 pages, 4% by 7% inches, containing tables of dimensions and prices for twist drills, reamers, drop-forgings, drop-forged and screw wrenches, spring cotters, and flat spring and riveted keys.

General Electric Co., Schenectady, N. Y. Bulle tin 42014 entitled "Headlights and Turbo-generator for Steam Locomotives," describing a turbo-genera tor set, designed to meet the rigid requirements o locomotive headlight service, and giving diagram showing the assembly.

Detroit Twist Drill Co., Detroit, Mich. Catalogue 18, 251 pages, 5 by 7½ inches, containing tables of dimensions and prices for twist drills, reamers, counterbores, milling cutters, end-mills, etc. Special sections are given for millimeter sizes of twist drills and reamers.

Buffalo Forge Co., Buffalo, N. Y. Catalogue 256 f Buffalo exhaust fans for the removal of shavings, awdust, smoke, fumes, etc., containing also engieering data and extracts from state laws regarding the provision of exhaust fans in manufacturing dants as required by law.

plants as required by law.

Manufacturers Equipment Co., 169-179 N. Jefferson St., Chicago, Ill. Circular illustrating "M. C. E." three-jaw air-operated chucks, which are furnished in two styles—semi-universal and full universal. The chucks are made in five sizes, ranging from 8 to 18 inches diameter, inclusive.

Manufacturers Equipment Co., 169-179 N. Jefferson St., Chicago, Ill. Catalogue of labor-saving devices, including two-jaw air chucks, hinge collet chucks, milling machine chucks, air cylinders, air valves, air vises, bath cock millers, self-opening dieheads, forming tools and collapsible taps.

Chicago Pneumatic Tool Co., 1000 Fisher Bldg.,

Chicago Pneumatic Tool Co., 1060 Fisher Bldg.. Chicago, Ill. Bulletin 34-Y treating of gas- and gasoline-driven air compressors. The "Simplate" flat disk air inlet and discharge valves with which these compressors are equipped enable high com-pressor speeds and efficiencies to be obtained.

Oakley Chemical Co., 26 Thames St., New York ity. Information Sheet 860 on "Oakite" for leaning metal parts preparatory to plating.

Photomicrographs of oil emulsified by "Oakite" and oil saponified by caustic, are reproduced to show their fundamental difference of action in cleaning etal surfaces

metal surfaces.

Hammel Oil Burning Equipment Co., Inc., 409
Pine St., Providence, R. I. Catalogue of the Hammel oil burning apparatus, showing applications to steam and water-tube boilers of horizontal and vertical types; oil pump sets; oil burner governors; and oil firing valves. A list of users of the Hammel burners and furnaces is included.

B. D. Nuttall Co., Pittsburg, Pa. Circular of the Nuttall one-piece expansion joint for pipe lines, which is offered as a leak-proof device requiring no packing and eliminating loops and U-bends from pipe lines. The Nuttall expansion joint is of the accordion type, the corrugations being machined from a solid blank, and not molded or bent to shape.

shape.

Bilton Machine Tool Co., Bridgeport, Conn.
letins 203 to 221, illustrating and describing a
matic gear milling machines, automatic manu
turing milling machines, drill presses built
single-spindle and gang types, automatic camdrill presses, horizontal milling machines, roblow riveting machines, automatic worm mil
machines, and universal gear hobbing machines.

machines, and universal gear-hobbing machines.

Chesnutt Mfg. Co., 1301-1303 Independence Ave.,
Kansas City, Mo. Booklet descriptive of the
"Eleveyor," an elevating truck equipped with service swivel casters, which is so designed as to
enable it to meet a wide range of work under difficult conditions. The "Eleveyor" elevates the
load and then conveys it wherever desired. The
book contains reproductions of letters of recommendation from various users of the "Eleveyor."

Check the Westing Truck Co. "Elitaburg Pa.

mendation from various users of the "Eleveyor."

Stroh Steel-Hardening Process Co., Pittsburg, Pa.
Catalogue descriptive of the Stroh Process, which
is a method for casting the finest alloy steel together with ordinary soft steel in one solid piece.
The resultant casting has a wear-proof alloy steel
stratum on the wearing surfaces, while the body
is composed of any desired steel and is in no way
affected. Illustrations of gears, car wheels, and
many large castings made by this process are
shown.

shown.

Henry Disston & Sons, Inc., Philadelphia, Pa., has inaugurated a monthly house organ for its employes, the first issue of which was published in July. The title of the publication is "Disston Bits," which has a double significance, "bits" being another name for the teeth of inserted-tooth saws, one of the company's products. The announced purpose of the publication is the stimulation and crystallization of good-will and fellowship among the employes, and it is the editorial matter be the work of the employes themselves. The new publication, "Disston Bits" will not in any way conflict with the "Disston Crucible," the trade organ of the company, which has been issued for several years, as the objects and purposes of the two publications are dissimilar.

#### TRADE NOTES

Cooper Hewitt Electric Co., manufacturer of merury vapor lamps, has moved its Philadelphia ofice from 124 S. 8th St. to the Drexel Bldg.

E. R. Senn & Co., manufacturers of "Belt-ol,"
scientific oil for treating leather belts, have renoved their offices to more spacious quarters at
2 Vanderbilt Ave., New York City.

J. N. Lapointe Machine Co. of Massachusetts,
Iudson, Mass., has been organized for machine
uilding, and a one-story cement factory building
0 by 300 feet is being erected. Ralph Lapointe is
eneral manager.

Crosman Stamping Co., Ypsilanti, Mich., is a

Crosman Stamping Co., Ypsilanti, Mich., is a concern recently incorporated to do general stamping and die work. George J. Crosman is president and treasurer; A. E. Sanford, vice-president; and Lewis H. McLouth, secretary.

Bickett Machine & Mfg. Co., Cincinnati, Ohio, manufacturer of horizontal and vertical milling machines, has added a large office and engineering department to its plant, which occupies the entire second floor of the main building. The lower floor is now required for manufacturing alone.

Phoenix Mfg. Co., Eau Claire, Wis., has moved to Cleveland office from 1430 W. Sixth St. to 913-5 Engineers Bldg., in order to obtain larger quarers, which are required to care for the increase f business. W. L. Harrison is the eastern representations. entative in charge

Chesapeake Iron Works, P. O. Box 1123, Baltimore, Md., and Westport, Md., are building overhead electric traveling cranes of three-motor direct-current type, having from 5 to 25 tons capacity. The company also builds five-motor double-trolley cranes of any span, having capacity up to 50 tons.

Carlton Machine Tool Co., Cincinnati, Ohio, has moved to 2994 Spring Grove Ave., where a new factory having about three times the floor space of the old shop has been erected. The new shop is equipped with machinery and appliances that will facilitate the production of the line of radial drilling machines made by this company.

Columbia Machine Tool Co., Hamilton, Ohio, which recently acquired the business of the Ceramic Machinery Co., will manufacture machine tools, making a specialty of shaping machines. A plant, 66 by 190 feet, of brick and steel, is being erected, and will be in operation at an early date. E. S. Rich, formerly with the Hamilton Machine Tool Co., is secretary.

Joseph F. Wangler Boiler & Sheet Iron Works

Co., St. Louis, Mo., has moved its general offices from 1547 N. 9th St., to 911-912 Federal Reserve Bank Bldg., 415 Pine St. The company was established in St. Louis more than fifty years ago to manufacture steam boilers, tanks, and all kinds of boiler plate and sheet iron work. Joseph A. Wangler, who has been with the company for more than twenty-five years, is president.

La Salle Machine & Tool Co., La Salle, Ill., has taken out a life insurance policy for each of its employes in the group plan, the amounts of which are equal to the yearly wages, limited to a minimum of \$300 and a maximum of \$2000. It is straight life insurance, and the entire cost is paid by the company. Employes participate in the benefits of the plan when they have been in the employ of the company for six months.

Scott-Spencer Automatic Tool Co., Madison Road

ploy of the company for six months.

Scott-Spencer Automatic Tool Co., Madison Road and N. & W. R. R., Cincinnati, Ohio, was lately organized to manufacture tools and equipment for automatic screw machines, specializing on this work exclusively. Thomas J. Scott, president, and L. B. Spencer, secretary and treasurer, are practical screw machine operators and are thus equipped by experience to design, make, and test equipment for automatic screw machines to suit various needs.

for automatic screw machines to suit various needs. Davis-Bournonville Co., Jersey City, N. J., opened a welding institute August 1, for the purpose of giving competent instruction in the oxy-acetylene art. The institute will be in charge of Henry Cave, technical director. The class will be held at the Jersey City factory of the company, and a charge will be made to cover the cost of oxygen, acetylene, metals and other supplies consumed. Employers using the oxy-acetylene apparatus can arrange to give a limited number of employes this course in welding and cutting.

give a limited number of employes this course in welding and cutting.

Electrical Industrial Co., Drammen, Norway, has consolidated with two other concerns in Norway—the Holm-Hansen Electrical Co., Sandefjord, and the Fridtjov Andersens Telepointage, Christiana. The association will continue to manufacture all articles in the electrical line, and will hereafter conduct its business under the name of the National Industrial Co., with main office at Sandefjord, and branch offices at Drammen and Christiania. The association is represented in New York City by Hans 'Karlsrud, manager of the Drammen branch, 309 Broadway.

J. T. Slocomb Co., Providence, R. I., manufacturer of machinists' tools, is building an addition of two stories to the main building 60 by 100 feet, making the building four stories in height. Another addition in the rear of the main building was erected last winter and has been in use for the past three months. The main office, stock-room and shipping rooms, will be located on the fourth floor and automatic elevator service will be provided. The additions made in the past year and a half provide facilities that more than double the production.

General Electric Co., Schenectady, N. Y., has recreted a building at the Schenectady plant af-

Volu

in the past year and a half provide facilities that more than double the production.

General Electric Co., Schenectady, N. Y., has erected a building at the Schenectady plant affording approximately 20,000 square feet floor space, which will be devoted exclusively to the manufacture of industrial heating devices. Continuous operation and the most productive grouping of machines have been obtained by the use of individual motor drive, direct-current motors being employed which range up to twenty-five horse-power. Many of the machines were developed especially to meet the unique requirements for machining, assembling and testing heating devices.

Acme Die-Casting Corporation, 5 Bush Terminal Bldg., Brooklyn, N. Y., has issued a statement to the effect that the suit recently brought against it by the Doehler Die-Casting Co. for infringement of patent No. 1,156,093 is limited strictly to the use of certain alloys of aluminum die-cast by a certain process. It does not cover aluminum zinc, aluminum manganese, or aluminum alloys containing 8 per cent or less of copper or more than 20 per cent of copper. The suit does not in any way affect the product and present business of the corporation, as it-covers a process not now in use.

Cincinnati Grinder Co. Cincinnati, Ohio, manu-

in use.

Cincinnati Grinder Co Cincinnati, Ohio, manufacturer of plain, cylindrical, universal, and internal grinding machines, is building a modern plant on Colerain Ave., In the heart of the West End manufacturing district. The new plant will afford 35,000 square feet of floor space and will be modern in its equipment and appointments. The building is of brick and steel construction with sawtooth roof, and will have a two-story front. The offices will be on the second floor, which is 40 by 96 feet. The rapid growth of the concern has made larger and better facilities for manufacturing imperative. Provision has been made for further extending the plant as the need for more room is felt.

extending the plant as the need for more room is felt.

Willard Machine & Tool Co., Cincinnati, Ohio, manufacturer of the Willard 13-inch tool-room lathe, has been sold to G. Mattman and Thomas L. Bratten. The firm name has been changed to Willard Machine Tool Co. Mr. Mattman is well known in the machine tool trade, having been for several years the European representative of the Cincinnati Milling Machine Co. He came to the United States from France in 1904 and worked in the shop for four years, learning the American way of building machinery. He has had wide experience both in the production and selling end. Mr. Bratten, although never identified with the machine tool industry, is also well known to the trade in and about Cincinnati, having held an executive position with the Employers' Liability Corporation, Ltd. For the present, the company will continue to manufacture the Willard 13-inch lathe, which will be somewhat improved, but the intention is to add other machine tools to the line in the near future.



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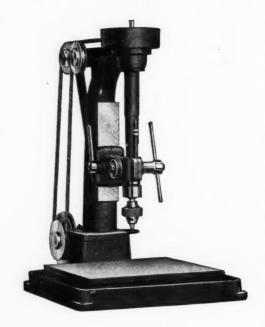
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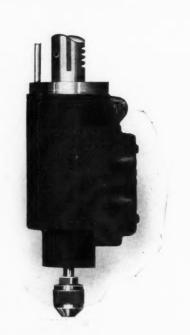
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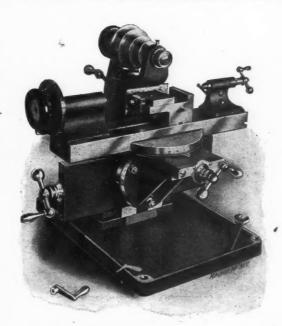
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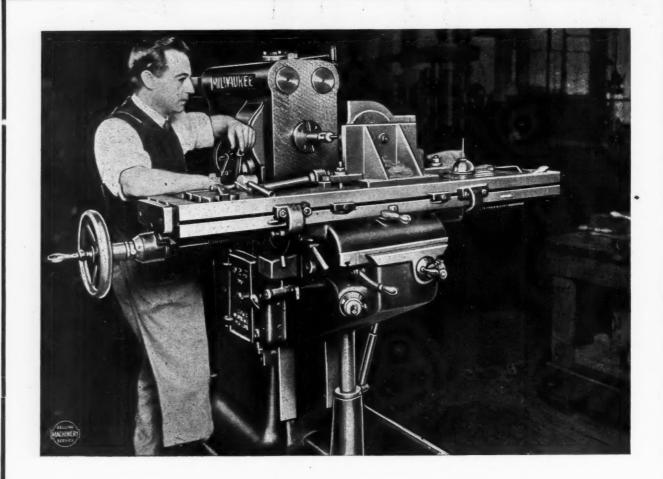
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# Milwaukee Milling Machines for the finest of Machine and Tool Work

The illustration shows a Milwaukee Milling Machine in the modern factory of the Hartford Special Machine Co. This company has quite a number of Milwaukee Milling Machines which were installed about a year and a half ago when the new shop was built on the outskirts of Hartford.

The Hartford Special Machine Co. does special machine and tool work and the Milwaukee Milling Machines are called upon to do the difficult work.

These machines have performed all kinds of milling work since they have been in operation. They have done work requiring extreme rigidity and have met every requirement. They have done work requiring extreme alignment and accuracy and have proven themselves equal to every demand.

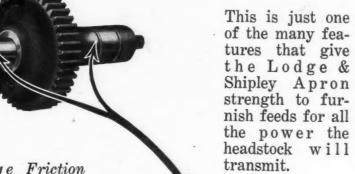
Milwaukee Milling Machines embody many features of design and construction. The double overarm—flanged spindle, reverse for which is self contained in the machine—solid top, box section knee—automatic flooded lubrication—cutter lubricating system an integral part of the machine—all combining for increased production, quality of output, low upkeep and ease of operation.

Catalogue No. 20 sent on request.

KEARNEY & TRECKER CO., MILWAUKEE, WIS. U.S.A.

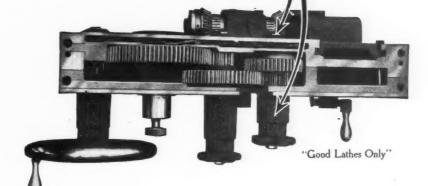
# Double Wall Support

For Every Apron Stud



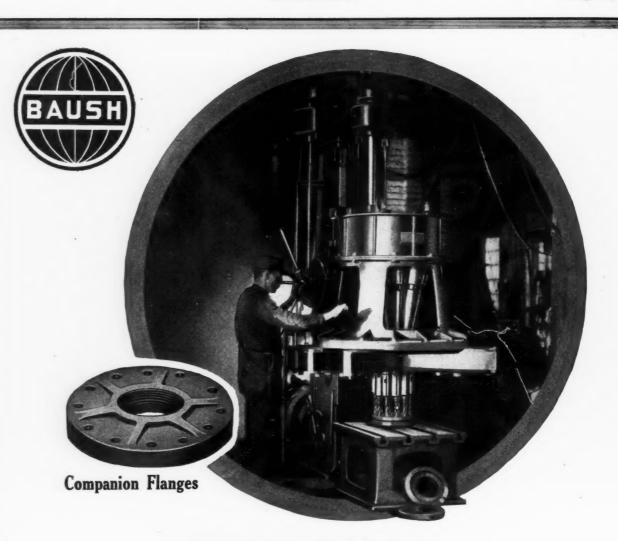
Large Friction Surfaces, Man Size Star Knobs to handle them with, a positive lockout to prevent throwing the half nuts and frictions in at the same time make it easy to operate.

Write for Bulletin M-129



Lodge & Shipley Machine Tool Co.

CINCINNATI, OHIO, U.S.A.



# BAUSH DRILLS

#### ALL HOLES AT ONE SETTING

The machine pictured is BAUSH No. 4 Heavy Duty Multiple in operation at the Chapman-Valve Mfg. Co.'s plant, Indian Orchard, Mass.

Machine has capacity up to  $20\,$   $^3$ 4-in.,  $16\,$ 1-in. or  $12\,$ 1 $^4$ -in. high-speed drills, and it gets all there is out of those drills. As for feeds, up to .020-in. per revolution is obtainable and the No. 4 machine is guaranteed to stand it.

For drilling FLANGED PIPES, FLANGED FITTINGS, NOZZLES, SEPARATORS, EXPANSION JOINTS, UNIONS, LINED FLANGES, BONNETS, YOKES, etc., there's a BAUSH Multiple.

Have you consulted with our Engineering Department?

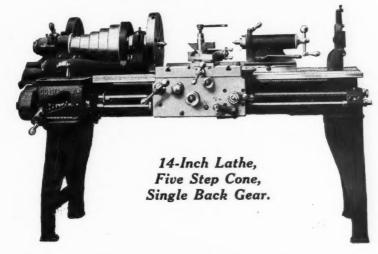
### BAUSH MACHINE TOOL CO., Springfield, Mass.

Detroit Office, Dime Savings Bank Building

Manning, Maxwell & Moore, Inc., 119 West 40th Street, New York City. Fenwick Freres & Co., France, Holland, Belgium, Switzerland, Italy, Spain, Portugal. Alfred Herbert, Ltd., Coventry, England, for Great Britain, Ireland, India, Burma, Ceylon, British South Africa, Japan, Manchuria, Corea, Formosa.



# For Easy Manipulation and Smooth Turning— A Bradford



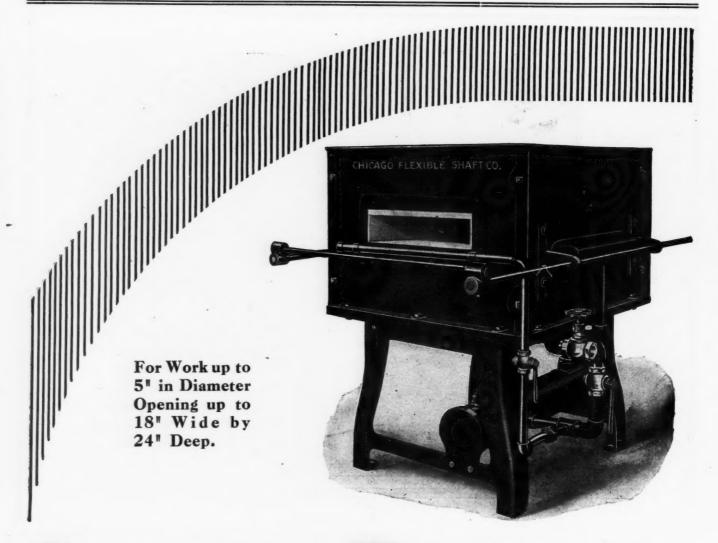
At the Hanscom Cutter Works, Hyde Park, Mass., they turn out counterbores and small cutters—good ones, too—by the bushel. In this hustling plant a 14-inch "Bradford" Lathe is among the busiest machines. With back gears out and belt running on the second (smallest) step, this machine peels the stock off small counterbores at a remarkable rate—and in spite of the high speed there's not the slightest "whip" or vibration. compact, and well-balanced design permits the high speeds that mean fast production on such work. There are a wealth of good features in Bradford Lathes—fully outlined in our catalogue.

Send for a copy.

# **Bradford Machine Tool Company**

CINCINNATI, OHIO, U.S.A.

AGENTS: Swind Machinery Co., Philadelphia. Taylor Machinery Co., Boston, Mass. Stocker-Rumley-Wachs Co., Chicago, Ill. Somers, Fitler & Todd Co., Pittsburgh, Pa. The E. A. Kinsey Co., Cincinnati, O., and Indianapolis, Ind. The Mine & Smelter Supply Co., Denver, Colorado. Pacific Tool & Supply Co., San Francisco, Cal.



# Stewart Furnaces

### A Good Drop Hammer Forge is a Necessity

Steel has to be properly heated to make a good forging. Stewart Forging Furnaces bring work to forging heat slowly and evenly; every piece is so uniformly heated from core to edges that it flows freely under the hammer. Their use is an advantage in every other way, too, for they take up little space in comparison to their capacity, burn gas or oil, need no flue or chimney connection and are free from every objectionable feature of coal or coke fires.

Stewart Furnaces have won their place in thousands of shops by their practicality, economy both of first cost and operation and their excellent performance. Buying a Stewart is really buying guaranteed satisfaction—and at a very moderate price.

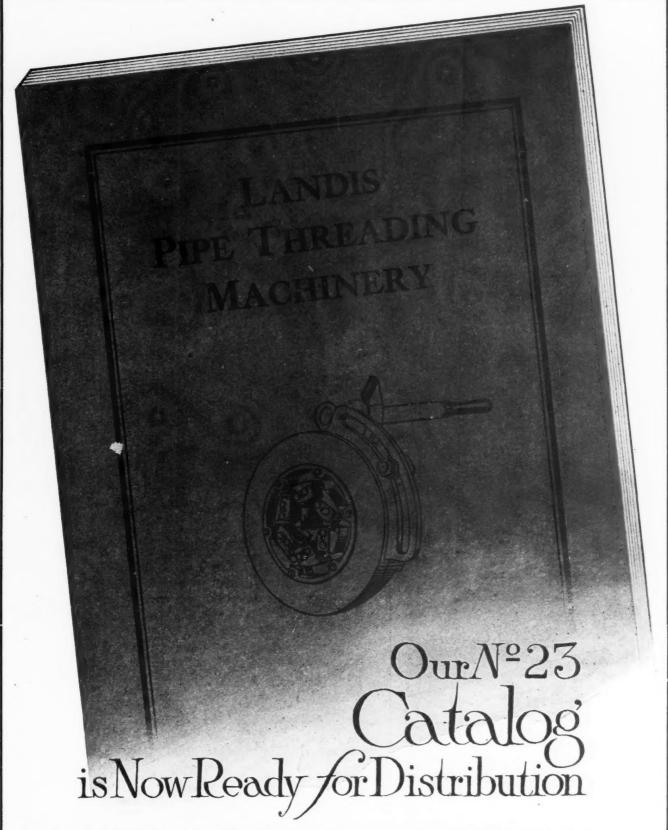
Catalogue?

# CHICAGO FLEXIBLE SHAFT COMPANY

**CHICAGO** 

149 W. La Salle Street

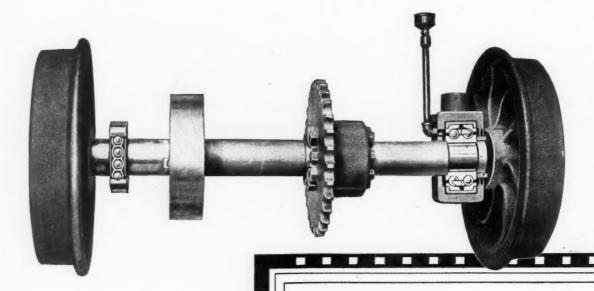
ILLINOIS



It lists the Landis "Pipe Threading Line"—Pipe and Nipple Threading Machines, Pipe Threading and Cutting Machines, also the Landis Chaser Grinder. Well illustrated with diagrams and detailed descriptions to show the advantages of Landis Chaser and Die Head design, construction, etc.

If you have not already received a copy your name is not on our lists. You should write us at once—a post card will do.

LANDIS MACHINE COMPANY, Inc. WAYNESBORO PENNSYLVANIA, U. S. A.





### BETTER **LOCOMOTIVES**

Use New Departure Ball Bearings

Mr. Whitcomb, General Manager of the G. D. Whitcomb Company, says:

"We are using New Departure Ball Bearings in our mine locomotive for two principal reasons; to reduce internal friction; to secure longer life of the bearings. Ball bearings will require a minimum amount of oil and attention while the plain bronze bearings unless kept well oiled, will soon get to cutting. We have very good results with these bearings."

We need add nothing more—except to offer the suggestion that the service of your own machines might be improved in the same way by the use of New Departure Ball Bearings.

Technical Literature and Free Engineering Service Upon Request.

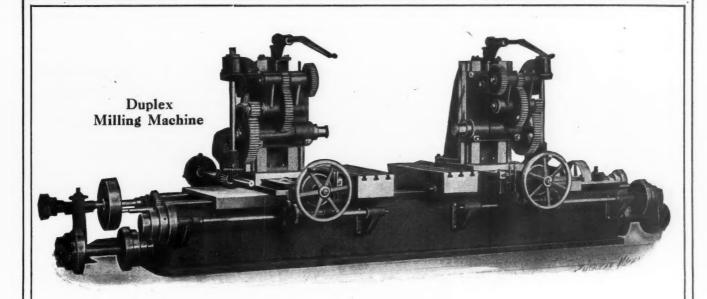
THE NEW DEPARTURE MFG. COMPANY

Conrad Patent Licensee Ford Bldg., Detroit Bristol, Conn.

Distributors in Trade Centers throughout the United States.

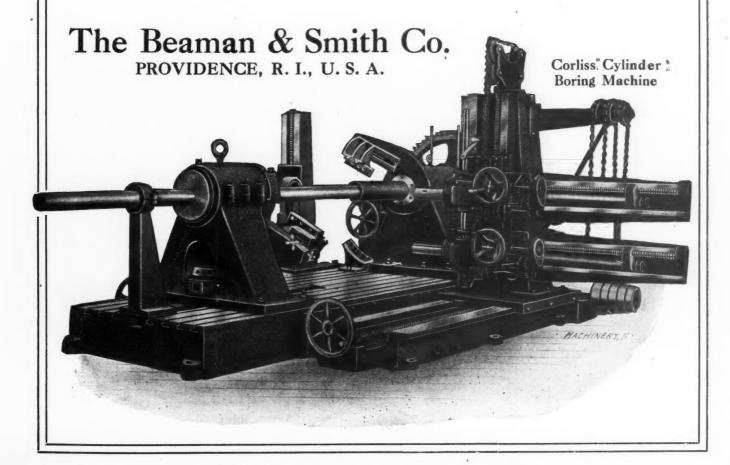
Sole British Agents: Brown Bros., Ltd., London & Manchester.
Continental Europe: Jacob Holst, Copenhagen, Denmark.

NEW DEPARTURE BALL BEARINGS



### If You Want Higher Production Consult Beaman & Smith

We design and build machines for accuracy, speed, ease of operation, and to give long, efficient service—machines capable of putting through several parts at one setting or performing several operations simultaneously. Consulting us involves no obligation. If you cannot use the machines we build to advantage we will say so frankly.



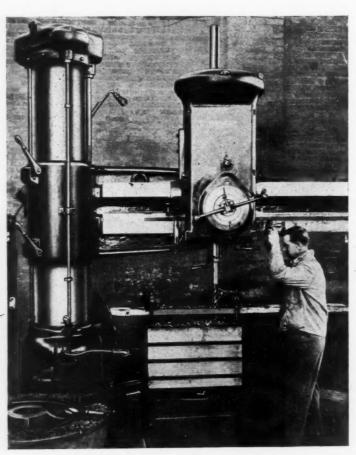


DRILLING RATE

# 600-1½" Holes thru 2" Steel per hour!!

1½" Drill, 500 R.P.M., .040" Feed-35 Point Steel 2" Thick 6 seconds per hole.

# THIS SURELY IS



Whitman & Barnes "Hercules" Drill used

This is nothing exceptional, however, for the new 6' "American" Triple Purpose Radial. Its excellent combination of power, spindle speeds, feeds and simplicity gives this new radial productive possibilities that simply cannot be overlooked by radial drill users.

THE AMERICAN

CINCINNATI,

LATHES

**PLANERS** 

ick



DRILLING RATE

160-1%"Holes thru 4½"Steel perhour!!

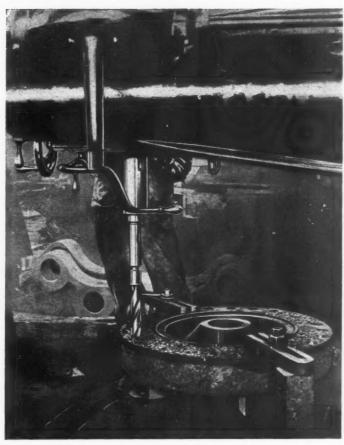
1%"Drill, 308 R.P.M., 040"Feed-35 Point Steel 4½"Thick 22 seconds per hole.

# DRILLING EFFICIENCY

These illustrations show two of the six "American" 6' Triple Purpose Radials in one of this country's large steel plants, where the above records were made during a test. Each of these machines is driven by an 18 H.P. motor. If you are confronted by any drilling problems, let us try to help you. If increased production is your aim, let us tell you about this new "American" drilling wonder.

# TOOL WORKS CO.

U. S. A.

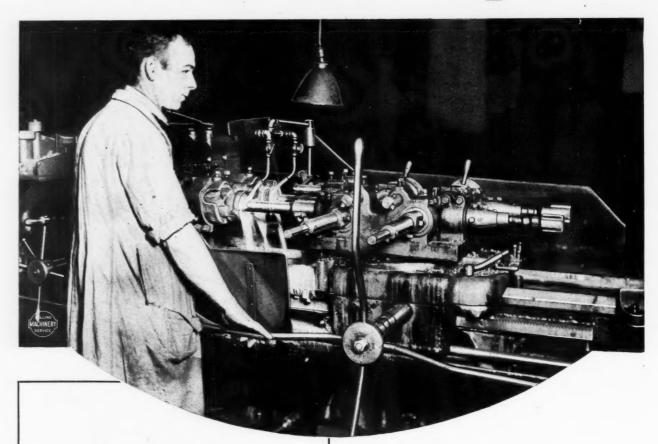


Whitman & Barnes "Hercules" Drill used

**SHAPERS** 

RADIALS

# The Double Spindle



Production
Figures Mean
Nothing Unless
the Conditions
are All Stated

Here are the figures. Fifty-four complete pieces per nine-hour day, average time according to the company's records. Seventy-two completed pieces per nine-hour day is an actual record.

Here are the conditions. The two brake carriers are first chucked. At the first position of the turret the three diameters are rough bored and the lugs on the outside are rough turned. Second position of the turret the 2.249" diameter is finish bored and the lugs on the outside are finish turned. Third po-

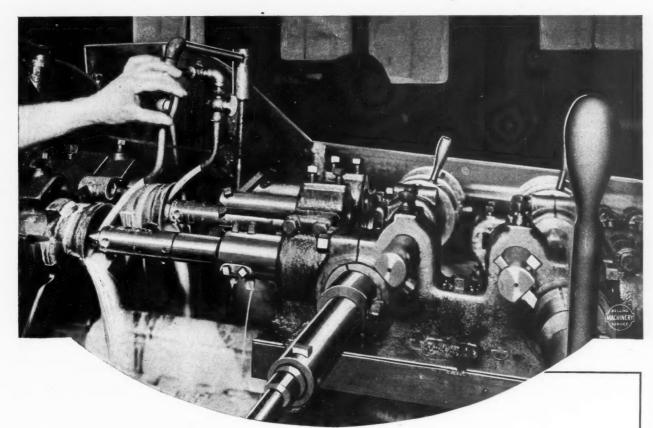
sition of the turret, finish bore 3.9375" hole, the 4 9/32" hole and ream the 2.249" hole, including facing the end and chamfering. At the fourth position of the turret, the 4 3/8" hole is tapped.

SPRINGFIELD, VERMONT U. S. A.

JONES & LAMSON

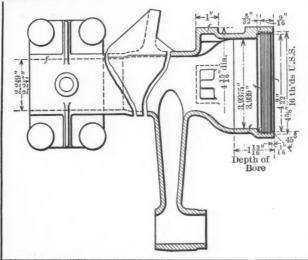
AGENTS:-FRANCE, SPAIN, BELGIUM: F. Auberty & Co., 91 Rue de Maubeuge, Paris.

# Flat Turret Lathe



The time has been given and the conditions have been stated. Draw your own conclusion! If there is any other machine on which this can be done faster and better than the Jones & Lamson Double Spindle Flat Turret Lathe—we would like to hear about it.

This illustration was secured through the courtesy of the H. H. Franklin Manufacturing Co., Syracuse, N. Y., where there are fourteen double spindle flat turret lathes in use. With that number in service the Franklin people realize their full possibilities; but output in this plant is no greater than may be secured anywhere with these machines on similar work.



Why not get thoroughly posted on the possibilities of the Flat Turret Lathe? Single and Double Spindle—each for a particular purpose.

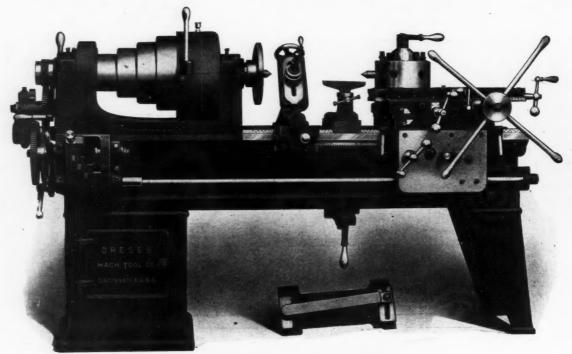
## **MACHINE COMPANY**

109 QUEEN VICTORIA ST. LONDON, E. C.

HOLLAND: Spliethoff, Beeuwkes & Co., Rotterdam.

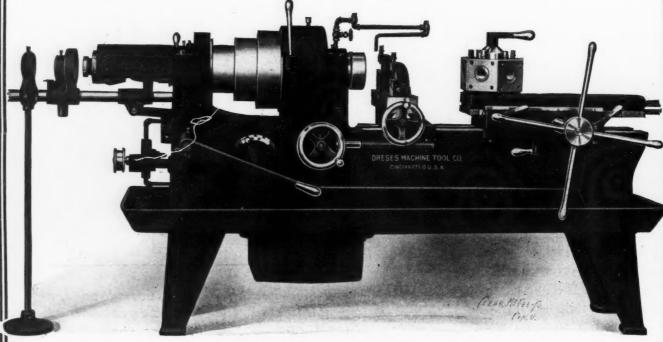
# **DESIGN** and **QUALITY**

Distinguish our complete line of



14", 16", 18" and 20" UNIVERSAL MONITORS

# SCREW and TURRET MACHINERY



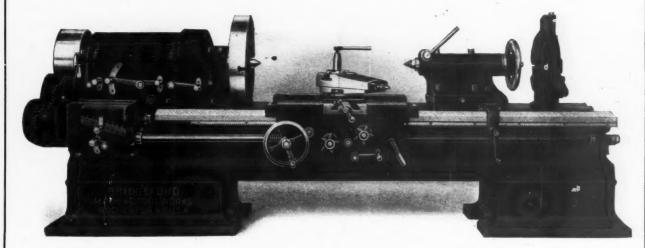
1", 11/2" and 21/4" SCREW MACHINES

### DRESES MACHINE TOOL CO., Cincinnati, Ohio

REPRESENTATIVES: The Fairbanks Co., New York, Boston, Philadelphia and Buffalo; Carey Machinery & Supply Co., Baltimore; E. I. Essley Machinery Co., Chicago; Badger-Packard Machinery Co., Milwaukee; William C. Johnson & Sons Machinery Co., St. Louis; The Chas A. Strelinger Co., Detroit; Canadian Fairbanks-Morse Co., Montreal and Toronto; Selson Engineering Co., London; Stussi & Zweifel, Milan, Italy Morse Louis; Chicago; Co., Louis; Chicago; Chicago; Chicago; Chicago; Co., Louis; Chicago; Chicago

## Bridgeford Lathes

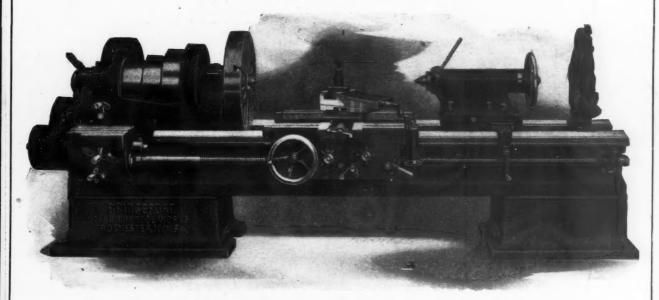
26" Cone and Geared Head Types



HERE is not a better lathe than the "Bridgeford" for handling heavy duty turning. Big shafts, heavy rolls, massive pinion blanks—work that tries the staying qualities of a lathe to the utmost—are the jobs that make up the daily work of these machines. Tremendous pulling power, backed by staunch construction and unusual convenience, make them speedy and efficient on really difficult work—the triumph of two decades of specialization in heavy lathe design.

Two models, 26" size, are shown. The Cone Drive Bridgeford is an accurate, speedy machine—a splendid all-round lathe. The Geared Head model is a wonder for heavy manufacturing, with a pulling power of 9,000 pounds.

Let us tell you more about these lathes.



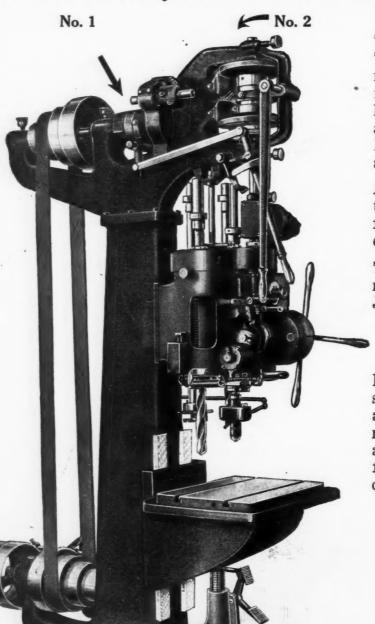
SPECIALISTS IN LATHE CONSTRUCTION FOR MORE THAN 20 YEARS

Bridgeford Machine Tool Works ROCHESTER, N.Y.

151 Winton Road

#### THE JOHNSON FRICTION CLUTCH

Used on the Semi-Automatic Turret Machines Recently Put on the Market by the Turner Machine Co., Danbury, Conn.



Courtesy of The Turner Machine Co., Danbury, Conn., U. S. A The back gears on the New Turner Turret Machine, which may be thrown out of engagement like the back gears of a lathe when not in use, are operated by a No. 5 Double Johnson Friction Clutch as shown by arrow No. 1.

Another Double Johnson Friction Clutch No. 5 operates the forward and reverse of the spindles as shown by arrow No. 2.

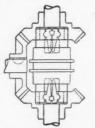
The latest and most up-to-date machines are equipped with Johnson Friction Clutches.

#### Why?

Because the "Johnson" is the smallest and most compact clutch and because it is more easily made to meet modern conditions and because it is the most powerful clutch of its size. It's the clutch with a reputation.



Double Clutch Exterior



Double Clutch in Nest of Gears

Write for Catalogue "A" and booklet "Clutches as Applied in Machine Building."

CANADA—Williams & Wilson, 320 St. James St., Montreal. The Canadian Fairbanks-Morse Co., Ltd., Toronto. ENGLAND—The Efandem Co., Ltd., 159 Gt. Portland St., London, W., Sole Agents for British Isles. AUSTRALIA—George Wills & Co., Brisbane, Queensland.

#### The Simplified Selective Speed Headstock

This is the simplest form of Selective Speed Headstock. The entire range of back geared speeds is obtainable while running and under cut.

The powerful double friction back gears are capable of transmitting loads greater than the full capacity of the wide high speed driving belt, and the change from high to low ratio can be made instantly by simply shifting the back gear lever.

> The belt is shifted rapidly over the cone by a single turn of an

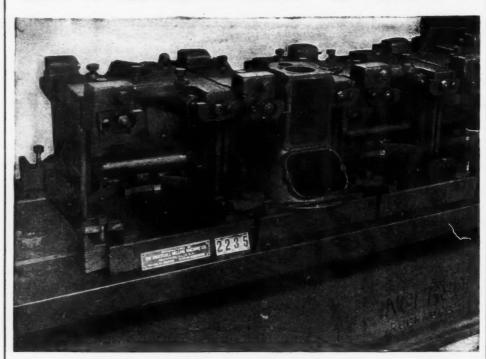
No other type of Headstock, regardless of its manufacture. provides this convenienceatequal investment, and under no condition can equal its low upkeep cost and general reliability.

The R. K. LeBlond Machine Tool Co. CINCINNATI OHIO, U.S.A.

Agents in Principal Cities



#### INGERSOLL



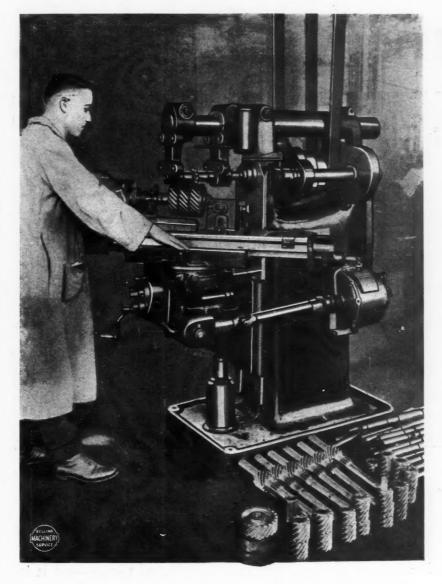
#### INGERSOLL HEAVY MILLING FIXTURES

are one of the most important features of Ingersoll Milling Equipment. Our experience has covered a long period of years; our designing and erecting are done by special departments devoted exclusively to fixture work. Our estimates and preliminary engineering work are absolutely without obligation to you, but our equipment is positively guaranteed.

THE INGERSOLL MILLING MACHINE COMPANY, Rockford, III.



FIXTURES



#### KEMPSMIT

#### Rigidity Scores Again

45° Spiral Gears

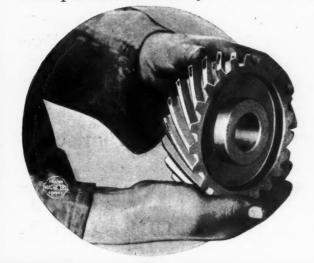
Take a look at these gears, at the relative positions of work and cutter, the angle at which the table travels to bring three blanks under the tool at each cut. Then consider the accuracy required in gears for machine tool use. It's a job that calls for rigidity, all the rigidity that can be put into a machine.

The Kempsmith Milling Machine is built on lines which fit it for just this kind of work. It is rigid in the most absolute sense of the word, with ample power to match its great strength.

It's a simple machine to operate, a rapid producer even on exacting work. Awkward positions, or hard-to-get-at surfaces are no bar to Kempsmith efficiency. Just what Kempsmith milling can do towards

boosting production and lowering costs, we want to show you—the sooner the better.

Write us.





MILWAUKEE, U.S.A

#### Cincinnati Planers



#### An Economical Way to Machine Gas Engine Connecting Rods

We've just received from our printer a new booklet that is sure to interest every planer user or owner.

It shows 28 typical planer jobs in as many different shops—gives somesidelights on the way the "other fellow" does it.

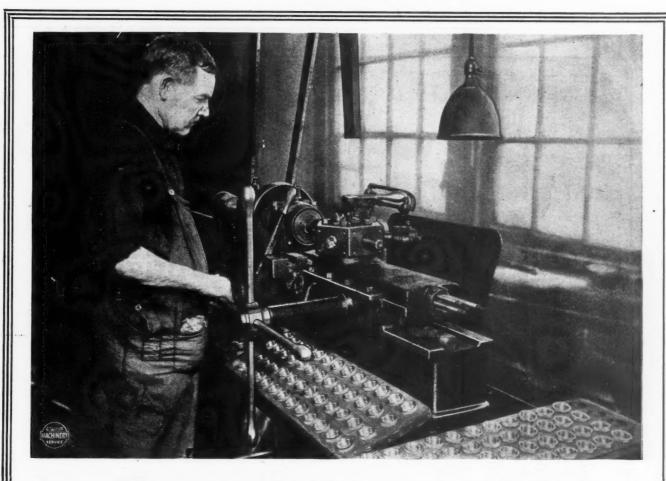
Better send for a copy.

This looks like a modern, efficiently conducted plant—and it is. Look at the way they plane those gas engine connecting rods! Cincinnati Planers, of course—and their full efficiency is utilized. On the 42" Cincinnati Planer of the widened type twenty connecting rods are clamped. These steel castings travel under the cutting tools at a speed of 40 feet per minute against a cut ½" deep and a traverse feed of 3/32" per stroke. Finish is good, output high, labor cost per piece very low—the usual "Cincinnati" combination.

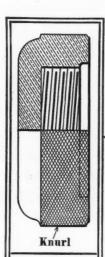
It takes a good planer—a planer like the Cincinnati—to handle work like that in quantities and maintain close and uniform accuracy. Staunch design, ample power, quick reverse, aluminum pulleys, wide, well supported vees, and easily handled operating parts are a few of the features that make

Planer Efficiency—Efficiency Planers

CINCINNATI PLANER COMPANY
CINCINNATI - OHIO, U. S. A.



#### One Minute! Nothing, or a Lifetime!



Let us tell you more about the good features that make the Cincinnati-Acme Screw Machine a different lathe of this type. In some forms of animal life a minute is an entire lifetime; in others it is nothing. It all depends upon what is done with, or in, the minute.

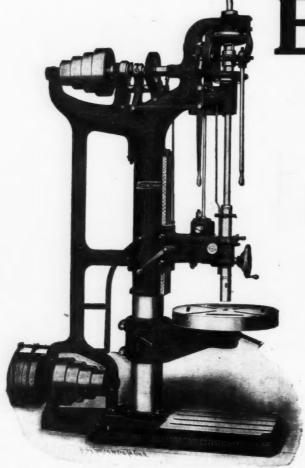
One minute is sufficient time in which to complete the second operation on this brass cap—turn, face and knurl—the work being held on a thread arbor.

The machine that makes such good use of a minute is a Cincinnati-Acme Screw Machine—and this is *average* time, output is 60 per hour, all day long.

This machine has been used by the Westinghouse Air Spring Co., New Haven, Conn., for a few months only; but this has been long enough to demonstrate its efficiency and economy over a wide range of work. And there are hundreds of concerns who have demonstrated the same things.

#### THE ACME MACHINE TOOL COMPANY

CINCINNATI, OHIO, U.S.A.



#### **Built for**

## The Cincinnati Upright Drilling Machine

This Heavy Pattern Drill was designed for special purposes and its construction is vastly superior to the average. Study a few of its good points and you'll readily see why fine service comes so easy to the Cincinnati.

The frame is composed of a deep, well ribbed base, large accurately ground column, well shaped gearguarded yoke, strong brace and conveniently located belt shifter. This built-in distinctiveness insures most profitable service and characterizes every part of the machine.

There are six positive, instantly available, feed changes, eight spindle speeds and a tapping attachment which acts through friction clutches and is operative at all speeds without shock or noise. This attachment possesses unusual gripping power, is adjustable, and may be disengaged when not in use. In addition to reducing tap breakage to a minimum it offers a convenient means for starting and stopping the spindle when changing tools.

Many other features contribute their share toward fine service—adjustable table, counterbalanced head, automatic trip, elevating mechanism, bronze bushed bearings, etc.

For a complete description get our circular U-4A. Copy on request.

THE CINCINNATI BICKFORD TOOL

U-534

### Fine Service



The features incorporated into this drill for insuring fine, accurate work cannot be improved upon. In the arm, for instance, no other radial offers such a narrow guideway for head or has such great depth between outer edges for preventing side or end rocking. The elevating screw cannot be set in motion by accident or remain in motion after the arm has reached its limit of movement. The depth gauge insures exact drilling depth, safety stop trips feed at right instant, while the strength and rigidity of construction further aid in preserving accurate alignments and close limits.

COMPANY, Oakley, Cincinnati, Ohio

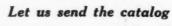
R-534



#### The GIANT Keyseater and a "Heap Big"

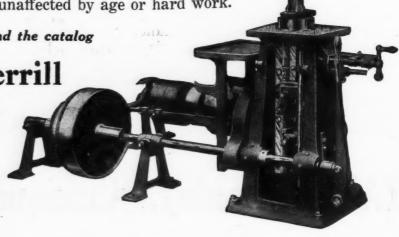
This "CIANT" is an important part of a busy contract manufacturer's gear making equipment. It cuts the keyways. In this 48" spur gear it cuts a 11/4" keyseat in less than 20 minutes, including setting up and removing work. It puts smaller work through in proportionately quicker time. The "CIANT" Keyseater gets its speed from an exclusive feature—holding work by the bore alone. No blocks, fixtures or holding devices are required. There is no waste time or effort; no need to face hubs to get a true surface from which to work.

"CIANT" Keyseaters are built in sizes to meet all requirements—to cut any shape, size or length keyway, accurately and rapidly. They are simple, rigid, dependable machines unaffected by age or hard work.



#### Mitts & Merrill

843 Water Street SAGINAW MICH.



## "MORSE" DRILS



Will help you keep your production up to the mark you have set. Many times they will enable you to set a new and a higher mark. They have the accuracy to do good work and the stamina to continue doing it. With a reasonable amount of care they will turn out almost unreasonable results but to do this

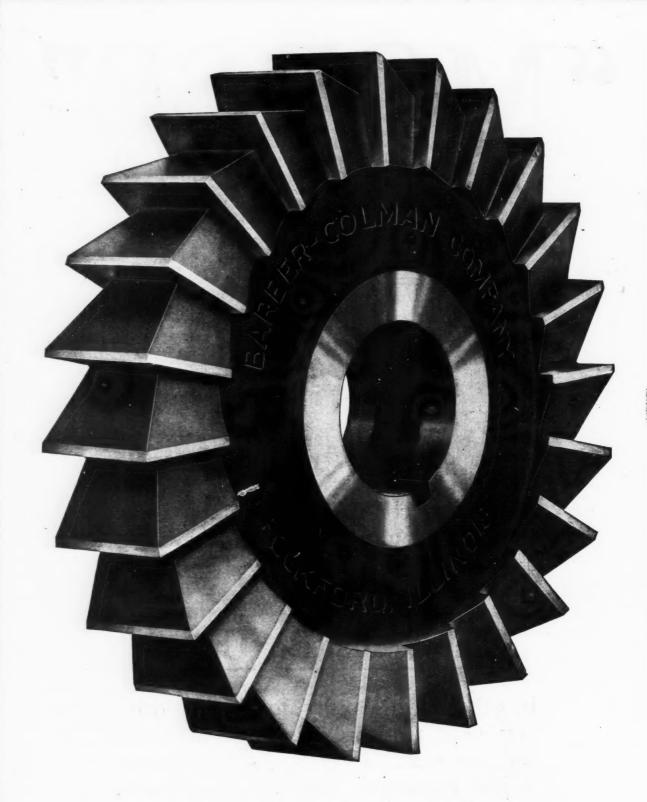
#### They Must Be There.

In other words, order to-day the drills you need to-morrow and the next day and the next. Even a slight overstock is less expensive than idle machinery, and when you want a drill these days you want it.

Catalog on Request.

#### MORSE TWIST DRILL & MACHINE CO.

NEW BEDFORD, MASS., U. S. A.



We guarantee our Milling Cutters absolutely, in respect to material, workmanship and accuracy

#### BARBER-COLMAN COMPANY

**ROCKFORD** 

ILLINOIS, U.S.A.

## And Now There's An EZY-OUT Set for Every Shop

YOU, who have been unable to obtain an EZY-OUT Screw Extractor Set small enough or large enough for your specialized needs, will be glad to hear that there are now

TWO ENTIRELY NEW

EZY-OUT Screw Extractor Sets

TWELVE SIZES IN ALL

(Patented 1914)

**Q** One of the three sets illustrated on the right contains the first real solution to the broken screw problem in your shop.

#### THE MODERN METHOD

HENCEFORTH, when a screw breaks, don't waste time fussing with files and punches—just drill a hole in the broken section, insert an EZY-OUT Screw Extractor, slip on a tap wrench and twist—and out will come that screw in a fraction of the time hitherto required, and without injury to the threads.

#### SOONER OR LATER YOU WILL FACE AN URGENT NEED FOR THIS TOOL

**Q** Why wait until then and risk the delay, loss and embarrassment that this unfilled need will incur? Ask us for our booklet descriptive of these new sets and the three extra large sizes not illustrated here, or better yet, choose your set and order it from your dealer today.

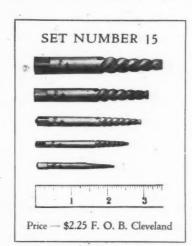


TWIST DRILL COMPANY

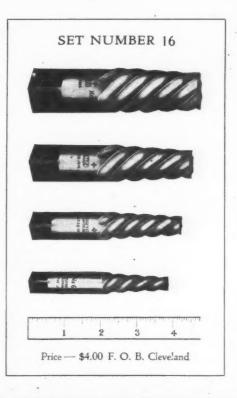
NEW YORK

CLEVELAND

CHICAGO







#### Entire Drive Runs in Oil

One pair of bevel gears and one spiral pinion, all rigidly mounted and running in oil, constitute the driving mechanism of spiralgeared

#### Gray Planers

Write for catalog describing all of their exclusive features

The G. A. GRAY CO. CINCINNATI, OHIO

Gray Dlaners

> "Made for those who want the Best"



will handle any and all classes of work equal to that done on any planer of any type.

With fewer working parts, it is the SIMPLEST PLANER ON THE MARKET.
All gears, in drive, except bull gear and its pinion are enclosed and run in oil.

Almost fool-proof.

May we send you a catalog?

#### CLEVELAND PLANER WORKS

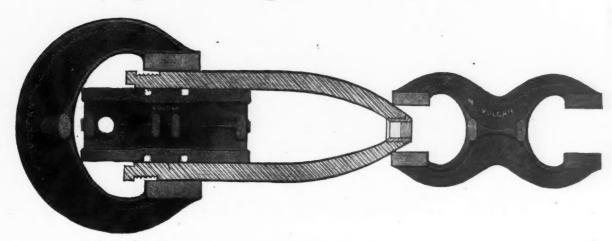
JAMES G. DORNBIRER GEO. W. FORD

3150-3152 Superior Ave., CLEVELAND, OHIO, U. S. A.

#### America Needs Gauges Now!

Some must be made separately with infinite pains, but

## Williams' "VULCAN" Drop-Forged Caliper Gauges Await Orders



for Internal, External and Eternal Service

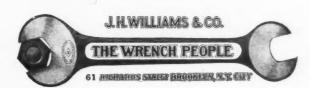
They can't be sized until detailed to their specific tasks. So that is your duty.

"We Forge, You Finish"

Every tool maker knows that "VULCAN" Gauges save much time needed to produce hand-made gauges for the work they can do as well. That time is now priceless. Wherever our Gauge can serve

**ENLIST A "VULCAN"** 

Western Office and



32A South Clinton St. Chicago, Ill.



#### The "Feel" of a Good File

Did you ever watch a really capable mechanic test a file? He has a way of passing a sensitive thumb over its jagged surface. Instinctively, unfailingly, he thereby determines whether it is fit for use.

This man invariably chooses NICHOLSON FILES. He never

buys blindly. He can "feel" that a NICH-OLSON FILE is right. He can "feel" its sharp, keen-cutting teeth, arranged in rows of perfect uniformity. There is no doubt in his mind. He buys NICHOL-SON. He makes sure of

satisfaction.



Our catalog and copy of "File Filosophy" will interest you. Write for them today.

NICHOLSON FILE CO., Providence, R. I.

(TRADE MARK)



## The Cleveland Milling Machine Co. PROFILE GRINDER

Is used to grind concave and convex cutters, cutters for fluting drills, cutters that are irregular but having a number of true curves, accurately rounding the corners on side mills and face mills, formed tools for lathes, planers and shapers.

The maximum radius that can be ground is 3 inches either convex or concave up to 12" diameter.

The center cut shows a variety of formed cutters accurately ground on this machine. This, however, is only a small percentage of the uses that this tool can be put to. Users are finding it indispensable in the tool room.

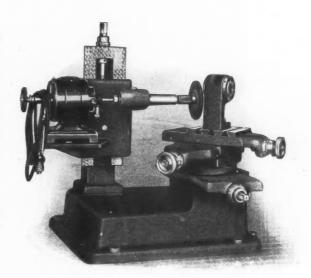
The wheel carrying spindle is direct connected onto the motor shaft and has adjustable bronze bearings and carries a wheel 4" diameter, \(\frac{1}{4}\)" wide, \(\frac{3}{8}\)" hole.

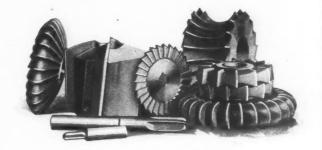
A type "D" Universal Dumore motor is furnished with ten feet of wire and lamp socket.

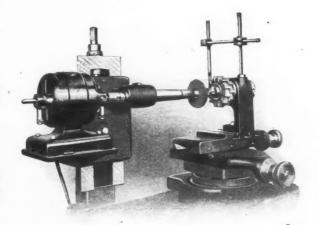
Complete equipment is furnished for all classes of work.



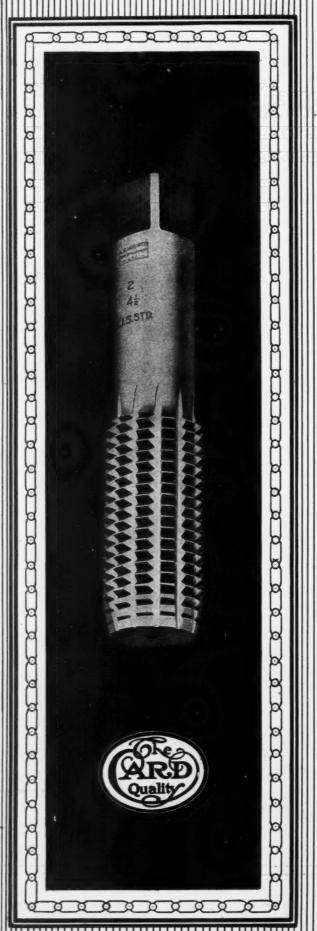
Immediate delivery if you get your order in now.







The Cleveland Milling Machine Co.
18511 EUCLID AVENUE CLEVELAND, OHIO





#### Taps of Uniform Dependable Quality

the one thing to consider in buying taps is quality; the accuracy and finish of your work depend on it—it governs tool service and tool costs.

Card Taps insure "Card Quality"—the quality that made Card Tools leaders from the start the quality that distinguishes every tool in the Card line.

> Actual experience with Card tools proves their economy. Catalog No. 28 gives full list. Send us a trial order.

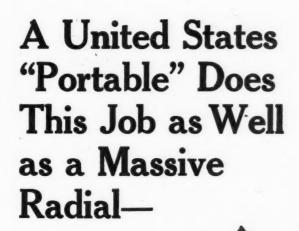
#### S. W. CARD MFG. CO.

MANSFIELD MASS.

New York Office, 62 Reade St.

European Agents: Chas. Churchill & Co., Ltd., London, Birmingham, Manchester and Glasgow; Markt & Co., Ltd., Paris; Fenwick Freres & Co., Turin; Ignacz Szekely, Budapest; V. Lowener, Stockholm, Copenhagen, Christiania; R. S. Stockvis and Zonen, Ltd., Rotterdam; R. S. Stokvis & Fils, Brussels; Andrews & George, Yokohama, Tokio, Osaka; J. Lambercier & Co., Geneva; R. D'Aulignac, Barcelona, Spain; Arthur Kayser, Berlin, S. W. 68. Oranienstr., 126. Germany.

MACHINERY



'And at a Fraction of the Cost.

We make United States Portable Drills and Grinders in types and sizes to meet all require-ments. We shall be glad to demonstrate their advantages. Let us send our catalog.

A practical and economical application of a U.S. Portable Electric Drill is shown below. At the plant of Charles S. Lewis & Co., St. Louis, Mo., they drill holes in massive pump bases in the manner shown. Over a platform on which the castings rest a traveling carriage mounts a U.S. Type G F Radial Drill. During the drilling operation the carriage is rigidly clamped in place and the holes are quickly put through the work. After drilling, the holes are tapped and the operation is complete. The advantage of handling work in this way is obvious. U. S. "Portables" have many possibilities in any plant. Think it over.

#### The United States Electrical Tool Co. 6th Ave. and Mt. Hope St. CINCINNATI, OHIO

New York Office, 50 Church Street, New York City.

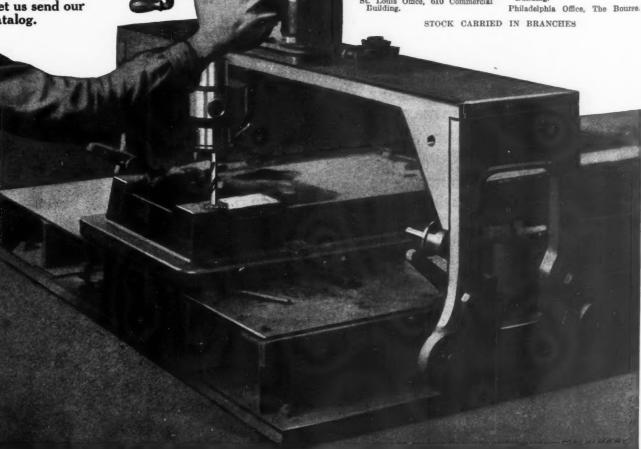
Street, New York City.

Street, New York Office, 50 Church

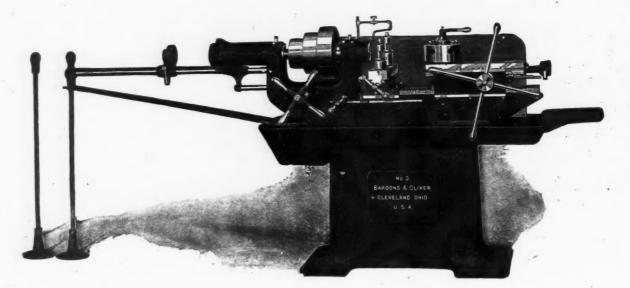
Street, Boston Office, 12 Pearl Street,

Street, Street, Chicago Office, 549 West Wash-ington Boulevard. St. Louis Office, 610 Commercial Building.

Detroit Office, 1410 Dime Bank Building.



## Bardons & Oliver TURRET LATHE



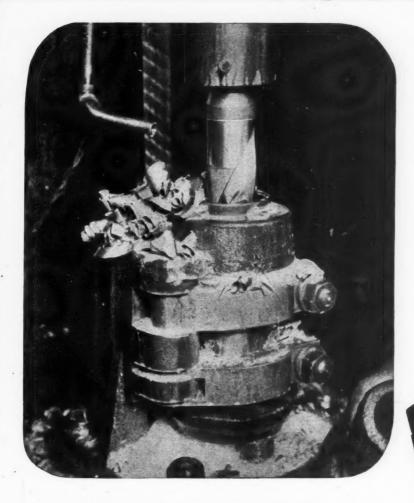
#### Conveniences That Speed Up Production

The Bardons & Oliver Turret Lathe is a machine of exceptional ease of manipulation—and any manufacturer knows that convenience is of really great importance. In these lathes the tooling system is so simple and complete that setting-up entails little loss of time, output naturally increasing in proportion as the maximum possibilities of the machine are utilized.

Operating facilities enable Bardons & Oliver Lathes to turn out an enormous amount of accurate work under ordinary conditions, and are a guarantee against any tendency to slow up under forced draft. Production never fails to jump wherever these lathes are installed. Unless you are familiar with their possibilities your output is probably far from what it should be. Let us send full description of the lathe and tell you where you can see them in action.

#### **BARDONS & OLIVER**

CLEVELAND, OHIO



## Standing Up—

Under Fifteen Thousand Pounds

A 1¼" drill should not break under *ordinary* conditions. But have you any idea of the tremendous stress it often undergoes in eating its way through the metal?

Add fifteen thousand pounds of vertical thrust to the grinding resistance and you have a fair idea of the kind of material and skill that make Union Twist Drills stand up.

Cutting coolly and rapidly, and with minimum wear, is a result that can come only from the broadest knowledge of tool requirements, together with the most scientific methods of material selection and manufacture.

The Union catalog also shows the full line of Union Tools—shall we send a copy?

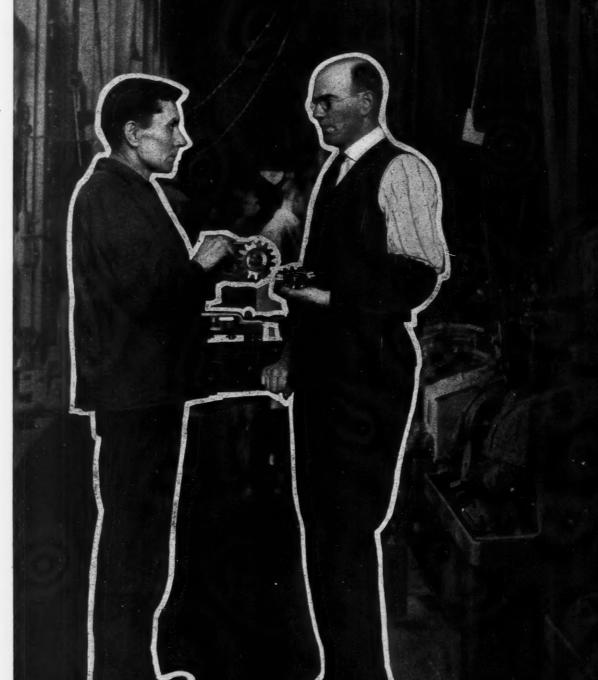
UNION TWIST DRILL CO.

ATHOL

MASSACHUSETTS



#### THE FINAL PROOF





THE FELLOWS GEAR SHAPER

FOREIGN AGENTS: Alfred Herbert Ltd. Coventry England:

#### OF ACCURACY

Don't fool yourself. You can't cut an accurate and efficient helical gear with an inaccurate cutter. Be the gear cutting machine ever so accurate, the cutter is the final arbitrator.

And speaking about cutter control, this must be positive and rigid, not flexible. If not positive, the best cutter that was ever made is no better than the worst.

In July Machinery we illustrated and explained the helical control mechanism which is used on the Fellows Helical Gear Shaper, and which guides the cutter in a positive and rigid manner.

The designer on the opposite page is now being shown the Helical Gear Shaper Cutter—the secret of perfect helical gears. This cutter has the involute curves of the teeth generated by a grinding process after hardening in the same manner as the Gear Shaper Cutter used for cutting spur gears.

#### This Point Is Important

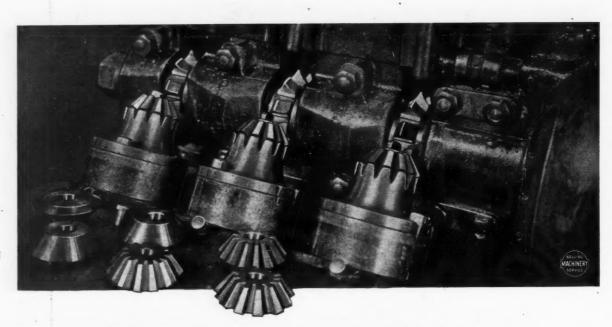
With the Helical Gear Shaper there are no "gears" to calculate. The feed of the cutter and the helix angle produced have no connection whatsoever. There is no jumping from pillar to post only to find in the end that you cannot get the helix angle you want. It is just as easy to cut a helical gear on the Gear Shaper as it is a spur gear, and the cutting of a spur gear is simplicity itself. Ask any owner of the Gear Shaper.

It is no exaggeration to say, therefore, that the Fellows Helical Gear Shaper has taken the "H—l" out of Helical and the "Myst" out of Mystery.

Don't fuss and worry along with the "old methods" any longer. There is a better way—the Gear Shaper way. Write now for our booklet, "The Fellows Helical Gear Shaper," which explains this most interesting machine.

COMPANY, Springfield, Vermont, U.S.A.

Paris, France, and Spain; Milan, Italy; Yokohama, Japan; Calcutta, India.

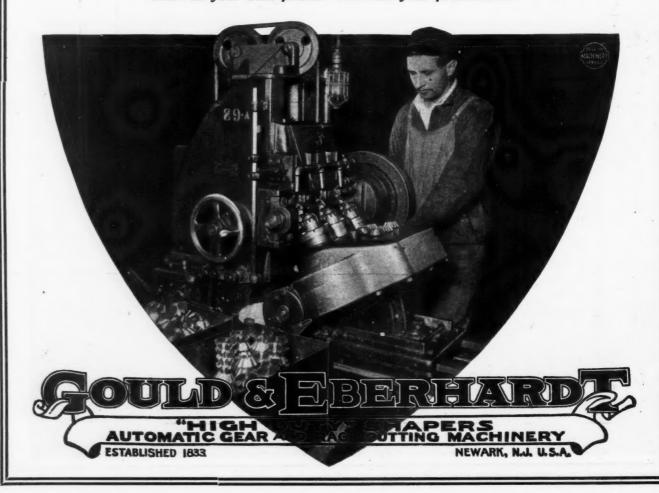


## Roughing Out Bevel Pinions on a G & E Multiple Spindle Gear Cutter

An average production of 300 pinions per ten hour day is produced on this machine—Pinion is 12 tooth, <sup>6</sup>/<sub>8</sub> pitch, <sup>3</sup>/<sub>4</sub>" face made of cold rolled steel.

In cutting 3 pinions at one time we treble ordinary production—Let us help you on your particular work with our experience.

Send us your blue prints. Increase your production.



#### Prestwich Fluid Gauge Only One Mechanical Movement

HERE'S just one mechanical movement in the action of the Prestwich Fluid Gauge—that of the diaphragm, the displacement of which by the object being gauged runs up the liquid in the tube

Th simplicity of this action, the readiness with which fine graduations can be read, the great durability of the mechanism and its wide adaptability make the Prestwich Fluid Gauge an ideal instrument for manufacturing purposes—for use where ever quantities of work must be gauged to close limits.

The range of work that can be gauged is remarkable. By raising or lowering the gauge column on its standard the measuring anvils can be extended or brought close together as required. The object is pushed between the anvils—and a glance at the level tells the story.

We'll be glad to send the complete story and show you how to speed up your measuring methods. Write us.

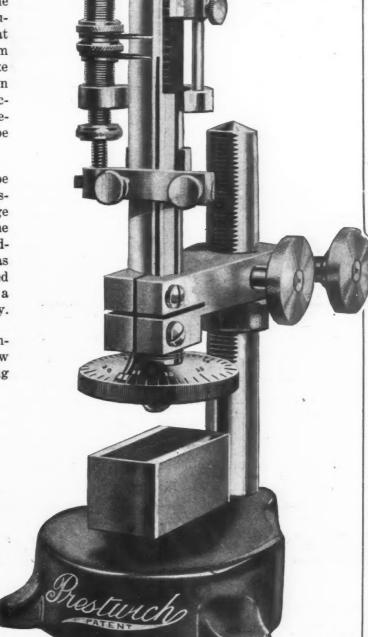
The
Standard
for
Measuring
Accuracy

Manufactured under license for the United States and Canada by

#### **Coats Machine Tool Co.**

INCORPORATED

30 Church Street NEW YORK





Assembled, tested, supplied with "juice" and cranked for a run, the Peerless looks, and is, a quality car from stem to stern. Geometric Tools—Die Heads and Collapsing Taps—help make it so. They contribute threads of the highest grade, accurate, finely finished threads, cut with remarkable speed and economy. It happens to be an internal threading job we are showing this time—differential cages in which the hole is 25% diameter, and the U. S. S. 16 pitch thread is 5% in length. Not spectacular threading this; but interesting to the production investigator because it shows how a wideawake concern secures results.

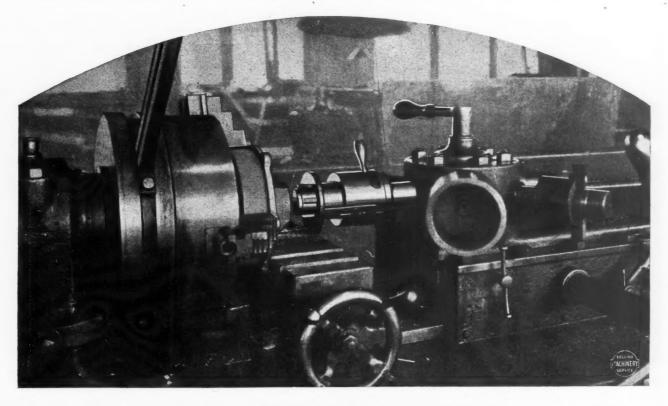
#### THE GEOMETRIC TOOL COMPANY

**CHICAGO OFFICE:** 

REGULAR AGENTS: The Chas. A. Strelinger Co., Detroit, Mich.; Hill, Clarke & Co., Inc., Boston; Vandyck Churchill Co., New York and Philadelphia; Brown & Zortman Machinery Co., Pittsburgh, Pa.; The E. A. Kinsey Co., Cincinhati, O.; Strong, Carlisle & Hammond Co., Cleveland, O. PACIFIC COAST: General Machinery & Supply Co., San Francisco, Cal.; Perine Mchy. Co., Inc., Seattle, Wash. CANADA: The A. R. Williams Machinery Co., Ltd., Toronto, Winnipeg and St. John, N. B.; Williams & Wilson, Ltd., Montreal.

# DIEHEADS

Geometric Tools are old timers with a record for universally efficient, economical service. They cut long, short, fine, coarse, tapered, inside or outside threads. Let us show how profitably they can cut threads for you. Write for the Geometric Catalog.



#### NEW HAVEN, CONNECTICUT, U.S.A.

545 W. Washington Blvd.

FOREIGN AGENTS: Chas. Churchill & Co., Ltd., London, Birmingham, Manchester, Newcastle-on-Tyne, Glasgow. Donauwerk Ernst Krause & Co., Vienna. V. Lowener's Maskinforretning, Sverre Mohn, Norway. Bevan & Edwards Pty., Ltd., Melbourne, and White & Rae, Sydney, Australia. Andrews & George, Tokyo, Japan. Also all manufacturers of Screw Machines and Turret Lathes.



#### Close Accuracy Required on Bearing Races

Heald Grinding
Is Uniformly Accurate

The hole in the small bearing is tapered 12° 6" and is 1.488" at the large end. The amount of stock removed is .012" and the grinding limits, .001" plus or minus. The output is one piece per minute per machine—60 per hour. Such a rapid and economical output is appreciated by the production man.

WORCESTER, MASS., U. S. A.

#### THE HEALD MACHINE COMPANY

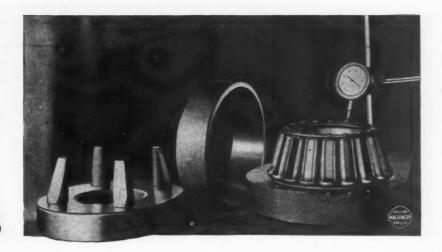
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NEW YORK, 839 Singer Bldg.

CHICAGO, 24 So. Jefferson St. DETROIT, 303 Majestic Bidg. CINCINNATI, 602 Provident Bank Bldg. CLEVELAND, 710 Engineers Bldg.

#### Good **Production** Secured with

#### Heald Grinders



We are showing bearing races ranging from 1\%'' to 11" diameter, close limit grinding of the kind that Heald Grinding Machines handle remarkably well.

There are 36 Heald Grinders used in the production of Bock Bearings, at the Bock Bearing Company's plant, Toledo, Ohio—36 thoroughly satisfactory machines.

Our Engineers will be glad to study your requirements. For quick service write the nearest branch office.



FOREIGN AGENTS: Alfred Herbert, Ltd., England, Italy, France, Switzerland, Spain and Portugal. F. W. Horne Co., Japan. Wilh. Sonesson & Co., Ltd., Sweden, Denmark and Norway. Post van der Burg & Co., Holland. Iznosskoff & Co., Russia.

## 5KF

Look for the mark SKF on the Machine Tools you build and buy

In every industrial center throughout the world the mark SKF on a ball bearing is the symbol of excellence. Its meaning is not limited. It stands not only for bearing quality and service, but also for unique design and for the brain, the skill and the spirit of the SKF organization. It stands for excellence—in all ways, in all nations, at all times.

#### **BALL BEARINGS**

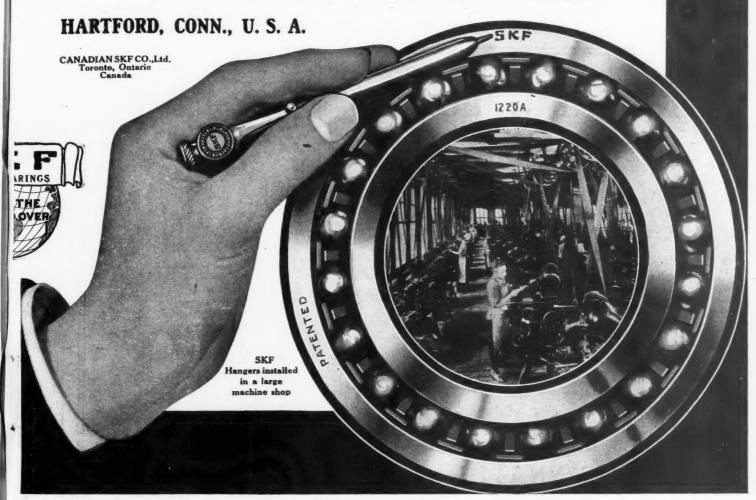


## 5KF

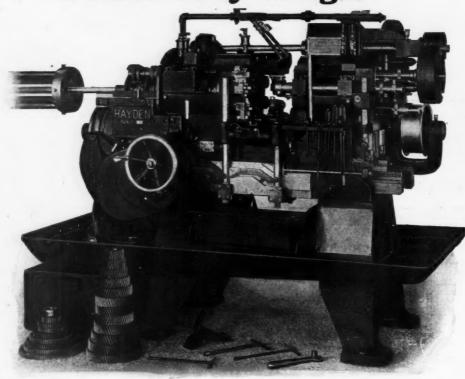
Strong, Dominating, Steadfast, SKF Quality is one with its Fame

The machine tool user or manufacturer who demands quality—who wants materials and workmanship of the highest standards—will find SKF adequate to his most exacting requirements. No effort is spared, no precaution omitted, to maintain the excellence for which SKF is famous. The mark SKF is more than the name of a ball bearing—it is the visible symbol of excellence. This is why it stands at the forefront of machine tool progress.

#### **BALL BEARINGS**



#### The Hayden Automatic From Any Angle



STUDY this machine from any viewpoint — investment, maintenance, operating costs, quantity or quality of output—and you'll understand why the Hayden Automatic always comes up for discussion when machines of this class are under consideration.

We claim that the Hayden Automatic is the superior of all other machines of its class, in every respect. And the net result is the greatest possible production at the lowest costs. These are strong claims; but we have proved them to many men and are ready to prove them to you—in any manner you may desire.

Send for the catalogue and the whole story.

CINCINNATI AUTOMATIC MACHINE CO., Oakley, Cincinnati, Ohio, U.S.A.

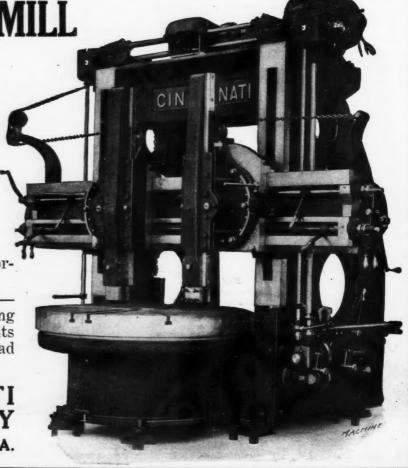
#### THE BORING MILL

The modern boring mill is more than its title indicates. It is a manufacturing tool—big, powerful, yet easy to operate, its special field being the machining of work of large diameter. It is accurate as well as powerful—carries wide forming tools and finishes such work as automobile tire molds to extremely close limits. It is carefully designed and thoroughly well built.

Such is the modern boring mill—such is the Cincinnati Boring Mill. No better machine of its class can be built. We'll be glad to prove it.

#### THE CINCINNATI PLANER COMPANY

CINCINNATI OHIO, U.S.A.





#### SHIELD BRAND MILLING CUTTERS WITH WIDE-SPACED TEETH

THESE cutters are desirable where a large amount of metal is to be removed.

They will be found especially efficient in high power milling machines.

We make them in all styles and sizes.

Write for further information.

#### THE STANDARD TOOL CO.

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London—C. W. Burton, Griffiths & Co.
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## "HAMILTON"



We have built Hamilton Lathes on the theory that as a machine is made so will it perform. We wanted accuracy, so we centered on rigidity—made the Hamilton bed wide, deep, with heavy bracings, and backed it up with a head-stock of massive and scientifically correct proportions. We wanted speed, so we provided tremendous driving power and operating helps of the simplest and most convenient kind. We have turned out a line of lathes that run second to none for capacity to turn out high grade work fast and keep ever-lastingly at it. The Hamilton spindle is forged crucible steel, bored its entire length, and accurately ground to size. Carriage is large, is securely gibbed front, center and back, scraped to solid bearing on bed its entire length and provided with power longitudinal and cross feed. All shafts and studs, lead screw, feed rod, and all rack and pinions are of high grade steel. All gearing accurately cut from the solid. All feeds are reversible from the apron.

Your chief need just now is reliable equipment. We can take care of your Lathe and Planer needs. Write for details.



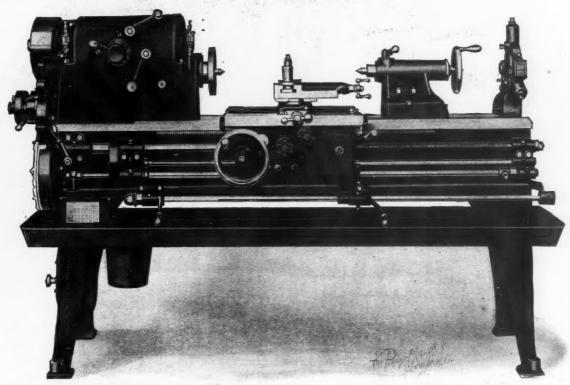
#### THE HAMILTON MACHINE TOOL CO.

HAMILTON, OHIO, U.S. A.

DOMESTIC AGENTS: T. Crowther & Co., Inc.. Boston, Mass.; M. D. Farnum, Springfield, Mass.; Garvin Machine Co., New York; Strong & Hery Co., Rochester, N. Y.; Sherritt & Stoer Co., Philadelphia, Pa.; Laughlin-Barney Mchy, Co., Pittsburgh, Pa.; Cullen Mchy, Co., Clereland, O.; Osborne & Sexton Mchy, Co., Columbus, O.; Wolverine Machinery & Supply Co., Detroit, Mich.; Stocker-Rumely-Wachs Co., Chicano, Ill.; Thomson Tool & Supply Co., Indianapolis, Minn.; Hendrie & Bolthoff Mfg. & Supply Co., St. Louis, Mo.; F. E. Satteries Co., Minneapolis, Minn.; Hendrie & Bolthoff Mfg. & Supply Co., Denver, Colo.; General Machinery & Supply Co., San Francisco, Cal.; Herberts Machinery & Supply Co., Los Angeles, Cal.; M. J. Walsh Mchy, Co., Milwaukee, Wis.; Textile Mil Supply Co., Charlotte, N. C.; Cotton States Belting & Supply Co., Atlanta, Ga.; Oliver H. Van Horn, Inc., New Orleans, La. CANADIAN AGENTS: H. W. Petrie, Ltd. Trornto. Ont.

#### SPRINGFIELD MACHINES

Set New Standards of Efficiency



Springfield Machines are not pace followers—they are pace setters and bring high production, high efficiency and remarkable range and capacity into your shop. This powerful Springfield "Ideal" 14" x 6' Single Pulley Engine Lathe is heavy, compact and practically noiseless. The design allows the use of short shafts of large diameter, which effectually frees the lathe from vibration and chatter. Thirteen gears give twelve speeds and you reach the desired speed at once without having to go through the whole series to reach it. From headstock to base this machine is made to give greatest service and value. It's more than a lathe—it's a standard.

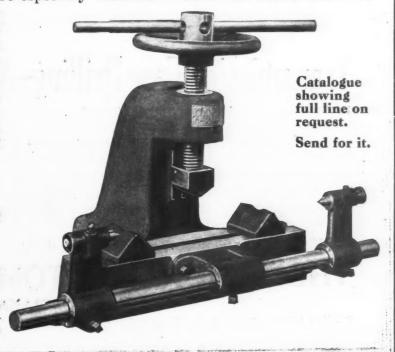
The Springfield Bench Straightening Press and Centers are made in three sizes for quick and accurate work. They are especially valuable in factories where there are

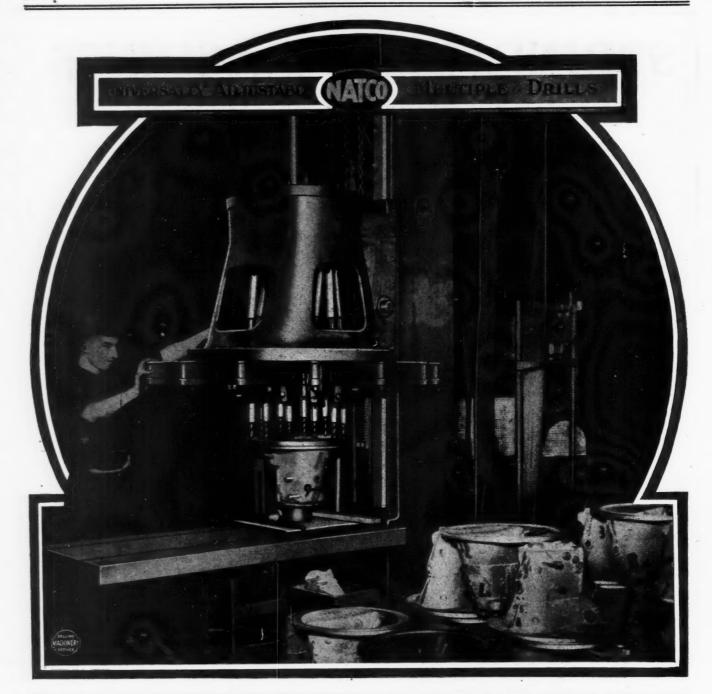
crankshafts and camshafts to straighten and where the result must be correct to promote perfect action of the machines of which the straightened shafts form a part. Work is not marred as the points of the set screw are brass covered. These are useful and competent tools and are another example of Springfield value.

#### The Springfield Machine Tool Company

631 Southern Avenue Springfield Ohio, U. S. A.

Manufacturers of Springfield Lathes and Shapers





#### Transmission Case Drilling-All on the NATCO

In the operation shown twelve 13/32-inch drills are used. The thickness of material is 1/2 inch. No lubrication. The operator completes this operation at the rate of thirty cases per hour. All the drilling on this transmission case is done the MATCO way. There are thirty-four holes in all, divided up into six operations.

The Durston Gear Co., Syracuse, New York, has another smaller MATCO drill—and each has been a profitable investment. The work done is performed at production figures as good as that quoted for this job—and the exclusive MATCO feature, independent speed adjustment for each drill, is one of the reasons.

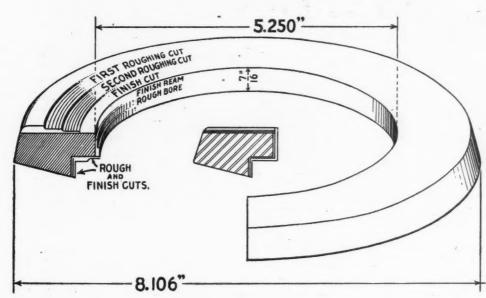
If you would drill most economically do it the MATCO way. More details on request.

#### THE NATIONAL AUTOMATIC TOOL CO.

RICHMOND, INDIANA, U. S. A.

FOREIGN AGENTS: For British Isles: Burton Griffiths & Co., Ludgate Square, Ludgate Hill, London. For France: Aux Forges De Vulcain, Paris. For Germany: Heinrich Dreyer, Berlin.

# CHROME-VANADIUM RING GEAR

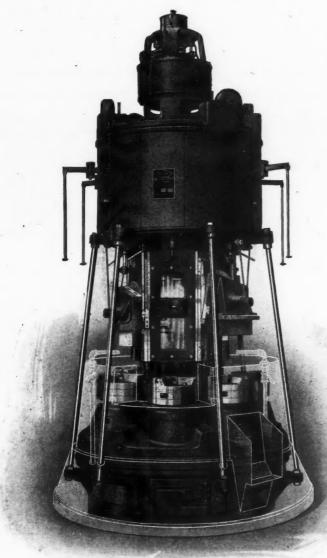


585 Every Eight Hour Shift

680, High Run, in Eight Hours

is a fine example of

Intensive Production



# BULLARD

#### MULT-AU-MATIC Vertical Lathes

Are making and maintaining similar productive records in a number of well-known plants.

Your work can be produced faster and cheaper.

Let us show you how.

# THE BULLARD MACHINE TOOL COMPANY

Bridgeport, Connecticut U. S. A.

#### IT'S UP TO YOU

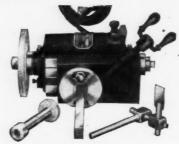
To increase your Production and Reduce your Costs by installing "CINCINNATI" Portable Electrics

TRY THIS TRIO



HAND OR BREAST DRILLS 1/4", %", 1/4", %" capacities. Weight from 7 pounds up. Gears run in grease. Single and two

SCREW-FEED DRILLS %" to 2" capacities, SCOTCH RADIAL DRILLS . %" to 2\(\frac{1}{2}\)" capacities.



TOOL POST GRINDERS
¼ to 3 H. P. Weight from 16
pounds up. Free hand feed.
Bearings adjustable to wear.
Horizontal and vertical feeds.
Different types for all purposes.

BENCH GRINDER OR BUFFER Five sizes, ¼ to 3 H. P. Also Pedestal Floor Grinder 1 to 3 H. P. Fully enclosed. Dirt- and dust-proof. Ball bearings.

Special Features:

Air Cooled. Ball and Thrust Bearings.
All working parts hardened. Overload Allowance.
Guaranteed Mechanically and Electrically.

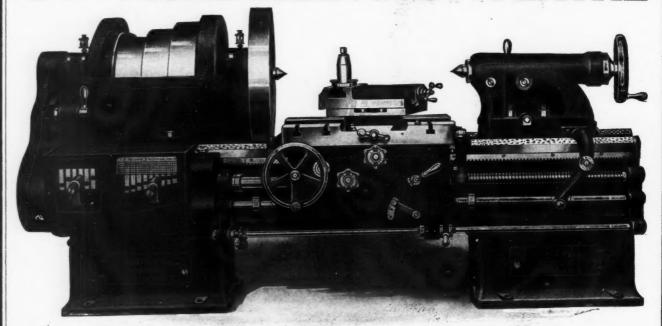
### CINCINNATI ELECTRICAL TOOL CO. 650-652 Evans Street CINCINNATI, OHIO

FOREIGN AGENTS: England: S. Wolf & Co., London. Australia: Parke & Lacy Co., Ltd., Sydney. Norway: V. Lowener, Christiania. France: R. S. Stokvis & Fils, Paris. Holland: R S. Stokvis & Zonen, Ltd., Rotterdam. Japan: Yamatake & Co., Tokyo.

New York Office, 50 Church Street

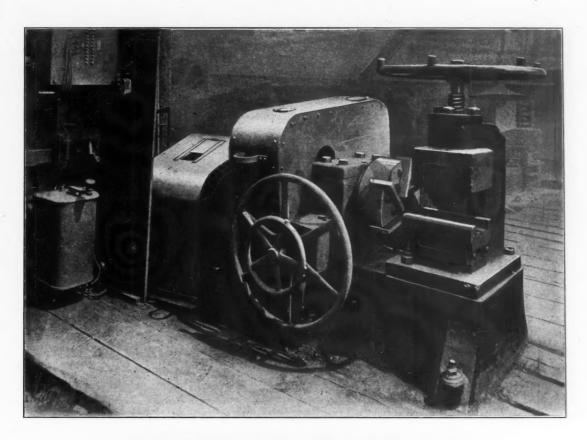
Stock and Service Department

#### G-K-MORE THAN JUST A LATHE



Most lathes are just lathes—nothing out of the ordinary, good enough for some purposes, most of them honestly built, but as like as peas in a pod. A G-K Lathe is different, different in important respects, in many details, in its very appearance. It is a better lathe—worth more because it can earn more—with an established company and years of experience behind it. Let us send the Booklet "G-K Betterments"—you'll find it worth studying.

THE GREAVES-KLUSMAN TOOL CO., Cincinnati, Ohio



# NEWTON

## An Old Rail Ending Machine That is Still "On the Job"

Although this Newton is ten years old in service, it's far from being a back number. With a few alterations, made necessary by changing conditions, it meets requirements with efficiency characteristic of the latest models.

The design of Newton Rail Ending Machines is practical, being governed primarily by the specific practice they're expected to undergo. As a result every Newton is a square peg in a square hole and covers its particular field as no other similar machine can.

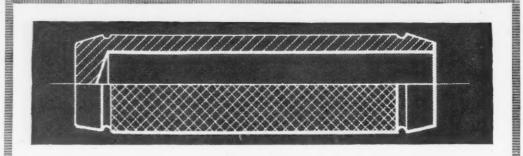
Every Newton is equipped with the very latest means for convenience and quick handling of stock; they're really ahead of ordinary practice as a matter of fact; and it's that very feature in a Newton that guarantees adaptability to meet any and all conditions satisfactorily.

The Newton line of frog, switch and rail rolling mill tools is complete; every machine characterized by power, speed and reliability to insure service of the highest order.

Send for catalog for all the details.

NEWTON MACHINE TOOL WORKS, Inc., 23rd and Vine Streets PHILADELPHIA, U. S. A.

Cat a second



# One Every Two Minutes on the CLEVELAND AUTOMATIC

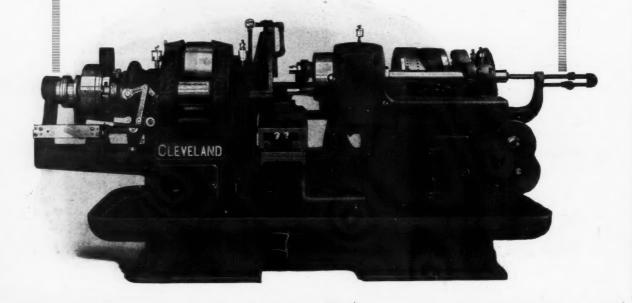
Consider the size and nature of this job, and the depth of the hole—then the 32 per hour rate at which the 1¼" Model A Cleveland Automatic turns it out will give you an idea of what the machine can do for you. The piece shown above is knurled its entire length and tapered at both ends.

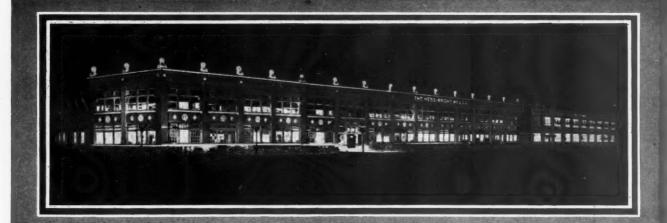
The tooling necessary on this job is as follows: Gauge stock to length; center for drill; drill half way and knurl full length; drill hole to full depth and form; cut off.

Fine finish, speed and accuracy with low labor cost are clearly defined advantages of Cleveland Automatic production. Let us give you conclusive proof.

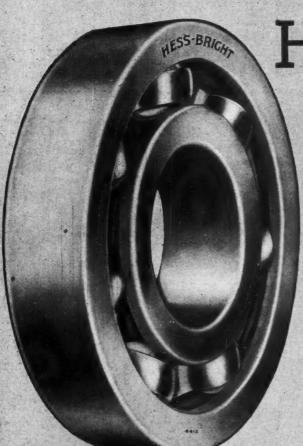
# Cleveland Automatic Machine Co. CLEVELAND, OHIO, U. S. A.

EASTERN REPRESENTATIVE: J. B. Anderson, 211 Gowan Ave., Mt. Airy, Philadelphia, WESTERN REPRESENTATIVE: Herbert E. Nunn, 565 West Washington St., Chicago, FOREIGN REPRESENTATIVES: Chas. Churchill & Co., Ltd., London, Manchester, Birmingham, Newcastle-on-Tyne and Glasgow.





## HESS-BRIGHT BALL BEARINGS



TAVE turned millions of revolutions on thousands of machines of hundreds of types for scores of purposes, standing millions of pounds of radial and thrust pressure.

They have done this in all climes, under varying conditions, with and without proper care, properly and improperly mounted or applied—and they have stood up under it all. Thus they are carrying industry's burdens to the greater benefit of mankind.

Such is their reward. Their virtues have been proved. They have stood the test of time's worst task-master—Service.

Select the right Hess-Bright for your need and your bearing problems are solved. Let our engineers aid you in the solution of your problems.

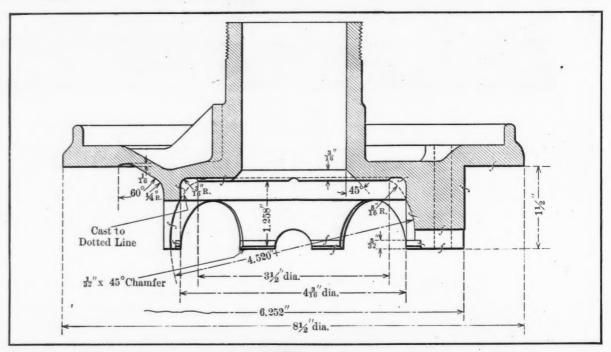
HESS-BRIGHT'S CONRAD PATENTS ARE THOROUGHLY ADJUDICATED

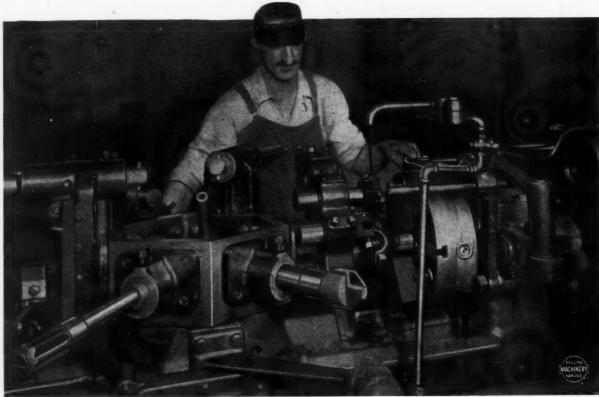
#### HESS-BRIGHT MANUFACTURING COMPANY

FRONT STREET AND ERIE AVENUE

.. PHILADELPHIA, PA.

## Again: Big Production from





#### THE WARNER & SWASEY

New York Office—Singer Bldg.

Detroit Office—Ford Bldg.

Boston Office—Oliver Bldg.

Buffalo Office—Iroquois Bldg.

Chicago Office and Show Rooms—618-622 Washington Blvd.

# Two Cuts at One Time on the Universal Hollow-Hexagon Turret Lathe

Because the Anderson Electric Car Company of Detroit machines its differential cases on the Universal Hollow-Hexagon Turret Lathe it is able to reduce operations at the first setting, normally seven, to five. Consequently a ten hour day's production at the first setting is fifty cases. The Anderson people consider this most excellent performance.

The material is malleable iron. The operations at the first setting are as follows:

First, chamfer 45 degrees. Second, rough bore, face inside race with turret, and at the same time face the 8 1-2 inch diameter flange with the carriage. Third, rough turn radius. Fourth, finish bore, and at the same time finish face gear bearing, finish flange, and finish radius surface. Fifth, ream.

This ability to take two cuts at one time is furnished by means of independent feed shafts for carriage and turret saddle. Each has ten individual feeds in either direction. While boring or turning with the hexagon turret the carriage will face, undercut or form.

Among the other good features of the Universal Hollow-Hexagon Turret Lathes are the power rapid traverse, great reserve power, and the rigidity that assures accuracy.

Send blueprints of one of your exacting jobs for a reliable estimate of the time saving effected by these machines

#### COMPANY, Cleveland, Ohio

FOREIGN AGENTS: Chas. Churchill & Co., Ltd., London, Birmingham, Manchester, Newcastle-on-Tyne and Glasgow. Allied Machinery Company, Paris and Turin. Van Rietschoten & Houwens, Rotterdam. Yamatake & Co., Tokio. Benson Brothers, Sydney and Melbourne. A. Asher Smith, Sydney. A. R. Williams Machinery Co., Ltd., Toronto, St. John, Winnipeg and Vancouver. Williams & Wilson, Ltd., Montreal.





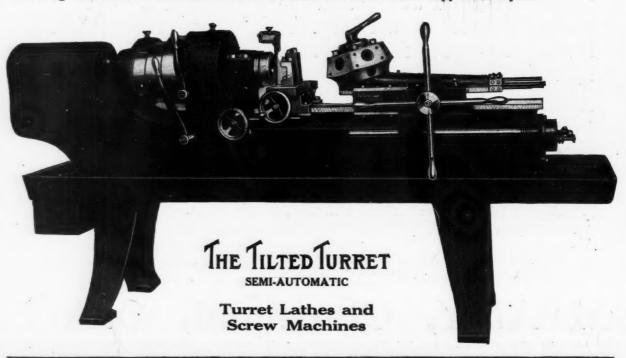
# WHERE ACCURACY and DEPENDABILITY Are Vital Factors of Construction

ACCURACY is one of the most important and prime features of construction in airplane work. Mechanical parts are subject to the most rigid and minute inspection.

It is in this class of work THE TILTED TURRET excels. No matter whether your operations be on bar stock or chuck work, where duplicate parts are essential, you will find THE TILTED TURRET a superior machine tool. At the present time, a large portion of the entire production of THE TILTED TURRET is being purchased by airplane manufacturers, which proves its DEPENDABILITY. THE TILTED TURRET is fifteen years old and the duplicate orders prove its efficiency. Ask the user.

#### Do These Facts Interest You As a User or Prospective Purchaser of Turret Machinery?

Our Catalog M-19 describes methods of construction of THE TILTED TURRET as well as showing the various sizes and models we manufacture. Your copy awaits you.

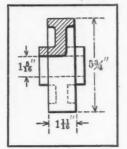


WOOD TURRET MACHINE CO.

BRAZIL INDIANA U.S.A.

If you've an unsolved production problem "Leave it to Libby." We shall be glad to show how a Libby Lathe will take care of it.

# Absolutely O.K.



# "Leave it to Libby"

The work is gear blanks 5 3/4" diameter, 1 11/16" face, 1 5/16" bore; 3/16" stock is removed, two cuts are taken, two settings finish the job. Close accuracy and fine finish are observed, yet the Libby Lathe turns out a

gear blank complete in 12 minutes. "Absolutely O. K.," says the Troy Laundry Machinery Co., Ltd., Chicago, Ill.—and they demand big things of their machines.

"Libby" users consider "Libby" speed, power, accuracy and range about the finest production combination on the market. These machines are designed and built to turn out the maximum of work at minimum cost. They are simple machines to operate, have power for heavy cuts, can be driven hard and are economical on all work they handle.

# INTERNATIONAL MACHINE TOOL CO. INDIANAPOLIS, INDIANA, U. S. A.

DOMESTIC AGENTS: Bowman-Blackman Machine Tool Co., St. Louis, Mo. Brown & Zortman Machinery Co., Pittsburgh, Pa. Eccles & Smith Co., San Francisco, Cal.; Los Angeles, Cal.; Portland, Ore. E. L. Essley Machinery Co., Chicago, Ill., and Milwaukee, Wis. Strong, Carlisle & Hammond Co., Detroit, Mich., and Cleveland, Ohio. Vandyck-Churchill Co., New York, N. Y.: New Haven, Conn., and Philadelphia, Pa. Syracuse Supply Co., Syracuse, N. Y., and Buffalo, N. Y.: FOREIGN AGENTS: Coats Machine Tool Co., Ltd., London, Eng. Ugo Violini & Co.,



POR MAXIMUM EFFICIENCY the operator of any kind of machine should be able to devote his entire attention to the turning out of work. Anything which distracts attention from the productive work, such as frequent oiling, or watching a cranky bearing to see whether it is getting hot, reduces efficiency.

When Gurney Ball Bearings are used, the increased mechanical efficiency is only a small part of the total saving. The greater saving is in the trouble-proof operation of the bearings—no frequent oiling, no watching for hot bearings, no adjustments for worn bearings, no shutdowns to replace bearings.

The big advantage of Gurney Bearings is that you can forget them once they are installed.

117

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2 8 60

GURNEY BALL BEARING CO.

CHICAGO

Conrad Patent Licensee

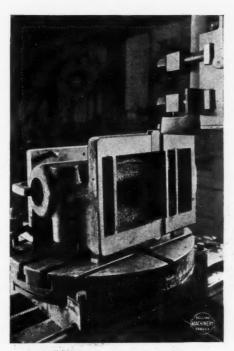
NEW YORK CITY

# DILL SLOTTER

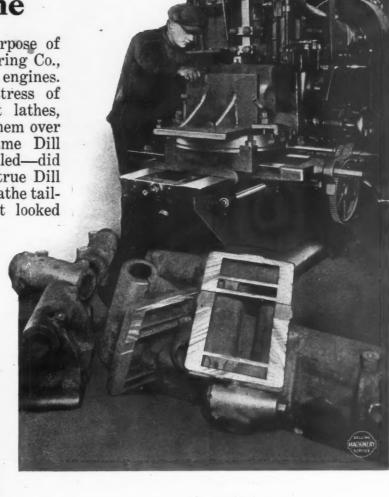
is a Manufacturing Machine

It was purchased for the purpose of helping the Shepherd Engineering Co., Williamsport, Pa., to build engines. When this concern, under stress of necessity, began turning out lathes, the machine that helped tide them over the hard spots was this same Dill Slotter. It planed, shaped, milled—did everything put up to it with true Dill efficiency. The bottoms of 20" lathe tail-stocks—a machining job that looked

like a sticker because no machine could be spared for the work—is just one of the jobs on which the Dill made a record.



Photographs secured through the courtesy of the Shepherd Engineering Company, Williamsport, Pa.



A single iron fixture holds the work. When a tail-stock comes off, even a surface plate fails to show up a low spot; the slot has been run across the surface and in the tongue recess at the rate of 25 pieces per 25 hours, floor to floor.

With a Dill Slotter handy you can do practically anything on any shape or size work. There are reasons—Dill rotating lathe, traveling head and a few others.

Write for the whole story.

#### T. C. Dill Machine Company

## The Dill Slotter People, Philadelphia, Pa.

FOREIGN AGENTS: Coventry, London, Birmingham, Leeds, Manchester, Newcastle-on-Tyne and Glasgow, Alfred Herbert, Ltd. France: Alfred Herbert, Ltd., Italy: Alfred Herbert, Ltd., Japan: Alfred Herbert, Ltd., Yokohama, Germany and Austria: Heinrich Dreyer, Berlin, Germany, Holland, P. S. Stolyis, & Zong, Ltd., Rotterdam, Relgium: R. S. Stokyis, & Fills, S.A., Brussels.

#### The "OHIO" Planer Has Table Dogs and Shifter Levers on Both Sides

This feature is right in line with the high production principle so thoroughly developed in "Ohio" Planers. There is no lost motion between the tumblers and the belt shifter arms, and the arms are located close to pulley so that belt can be shifted much more rapidly. Levers on both sides save even the time it takes a workman to walk from one side to the other.

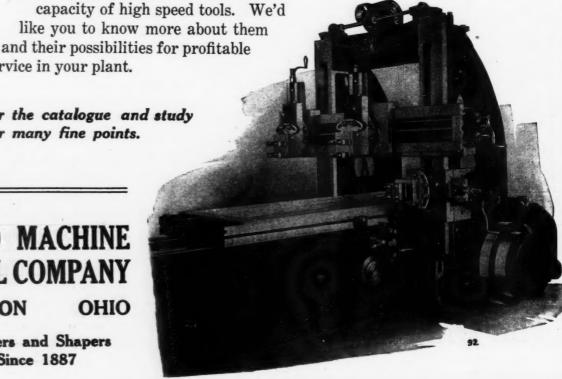
The "Ohio" represents the latest design in metal planing machines, and is built throughout for accurately machining the heaviest classes of work at the maximum

Send for the catalogue and study their many fine points.

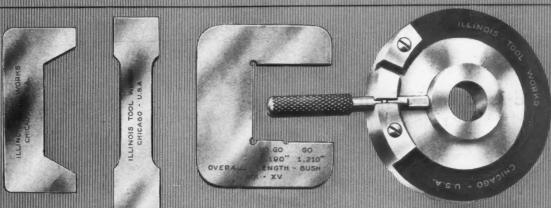
service in your plant.

#### **OHIO MACHINE TOOL COMPANY KENTON** OHIO

Planers and Shapers Since 1887









Illinois Gauges and Precision Tools are accepted as the standard of accuracy in numerous plants where the highest degree of exactness is required. For intricate Punch Press Work, Illinois Dies can be depended upon to produce uniformly perfect parts. Write or Wire for Quotations.

ILLINOIS TOOL WORKS, CHICAGO, U.S.A.

Manufacturers and Designers of Cutters—Hobs—Reamers



## Complete Line

8-inch to 50-inch Swing

(With or without Tapping Attachment)

Upright Drills

Horizontal Drills

> Gang Drills



## BARNES DRILLS

Accuracy
Convenience of Operation
Strength

MADE BY

W. F. & John Barnes
Company 231 Ruby Street
Rockford, Ill., U. S. A.

#### When East and West Agree

This punch—
Made by Mehl Machine Tool & Die Co., Roselle, N. J.—
For Western Electric Co., Hawthorne, Ill
Allowed limit of error ± .0001".

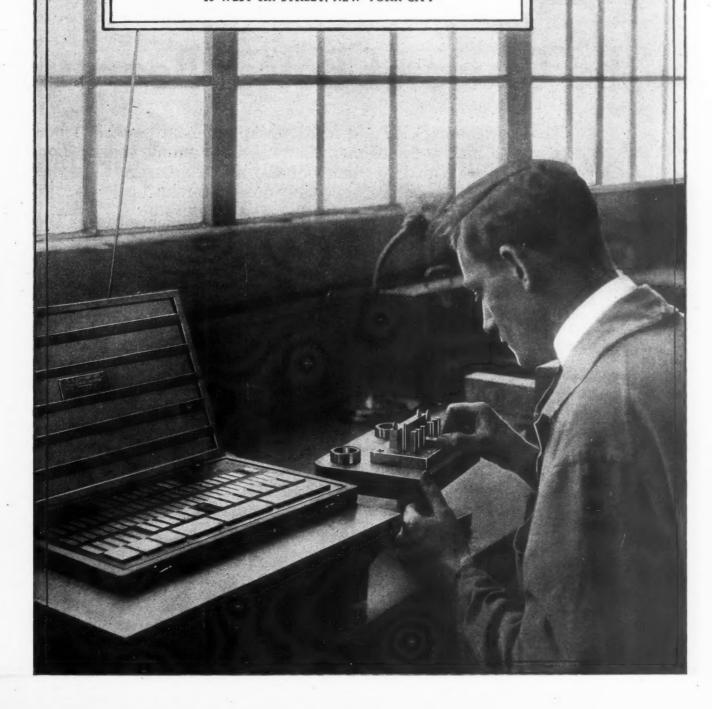
Time and material have been wasted if this punch is rejected. Will the inspector in Illinois agree with the toolmaker in New Jersey on what is .0001"? Sure!

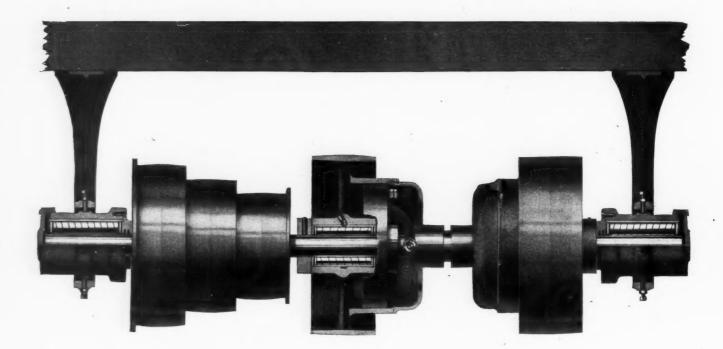
They both use Johansson Standard Gages.

Johansson Standard Gages have unlimited use in the toolroom and inspection department. Every day, toolmakers are finding new uses for them in laying out and checking jigs, dies, fixtures, gages, etc. No two manufacturers use the Johansson Standard Gages alike. All agree they cannot get along without them.

#### THE SWEDISH GAGE CO., Incorporated

16 WEST 61st STREET, NEW YORK CITY





# In the Cause of Better Bearings;

The shortcomings of old-fashioned plain bearings have been known to machine tool manufacturers for many years. Long ago it was decided by many of the manufacturers that plain bearings were a failure, especially on countershafts.

In theory plain bearings may be all right. But in practice they fall down hard.

Bad lubrication is chiefly responsible for their miserable failure. They won't hold the lubricant at all. The oil leaks out; the bearing runs dry. The machine must stop.

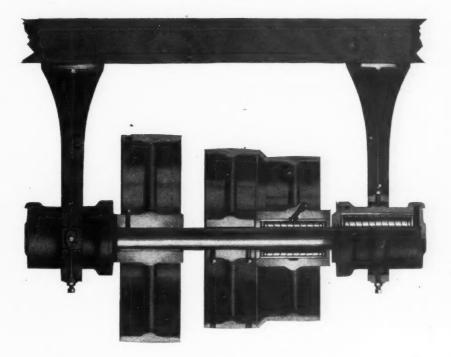
A machine tool operator must not be hampered by unreliable



bearings. He must feel free to speed up his machine whenever conditions demand it. He must not live in fear of his bearings breaking down. For the sake of his efficiency, you should save him the worry of bearing trouble. Let him have confidence in his machine—put Hyatt Bearings on the countershaft.

Hyatt Roller Bearings are anti-friction. They save power.

HYATT BEARINGS



# Greater Speeds, Constant Service

And Hyatt Roller Bearings solve lubricating troubles. Hyatt Rollers are hollow and have spiral slots. Each roller acts as a reservoir for oil. Through the spiral slots the oil is sent oozing out over the whole bearing surface and back into the roller again. The oil is always on the move and always doing good. Every drop of oil is used to such advantage that Hyatt Bearings don't need oiling more than once a month.

Greater speeds! Constant service! Long life! Ideal lubrication! That's what Hyatt Bearings should mean to you. Think the matter over.

#### PARTIAL LIST OF USERS

Cleveland Automatic Machine
Cleveland, Ohio
Hardinge Brothers,
Chicago, Ill.
Bullard Machine Tool Co.,
Bridgeport, Conn.,
Chard Lathe Co.,
New Castle, Ind.
Foote-Burt Co.,
Cleveland, Ohio
National Automatic Tool Co.,
Richmond, Ind.
Bausch Machine Tool Co.,
Springfield, Mass.
Rockford, Ill.

JSERS

Fox Machine Company,
Grand Rapids, Mich.
Ingersoll Milling Machine Co.,
Rockford, Ill.
Rockford, Ill.
Landia Tool Co.,
Waynesboro, Pa.
Fitchburg Grinder Co.,
Fitchburg Grinder Co.,
Fitchburg Grinder Co.,
Fitchburg Haber Co.,
Rockford, Ill.
Heald Machine Co.,
Worcester, Mass.
American Tool Wiss.,

HYATT ROLLER BEARING CO.
NEWARK NEW JERSEY

When you want data on HYATT BEARINGS for countershafts, drop us a line.

FOR COUNTERSHAFTS



#### And Solomon

Forgot to invite the Forgeman to the banquet celebrating the completion of the temple.

When the throne was unveiled however there sat the forgeman in the seat of honor the uninvited.

The guards rushed to cut him down; but Solomon said "How could this temple have been built but for this man?"

Now then, when building your engines, ships and machinery invite prices on

We feel honored in receiving your invitation and shall strive to secure the place of honor by taking your order.

We are thoroughly equipped to make many forgings, light or heavy, for various industries and simply add what is below as a

#### "BUYERS GUIDE" -

High and Low Carbon Bars Press Columns and Rams Water Cylinders Pull Back Cylinders Valve Bodies Valve
Plungers
Weldless Steel Rings
Lathe Spindles, solid and
hollow bered
Long Feed Screws
Crank Shafts

Eccentric Shafts
Grusher Shafts
Gear and Pinion Blanks
Side and Main Rods
Crank Pins
Axles
Locomotive
Repairs

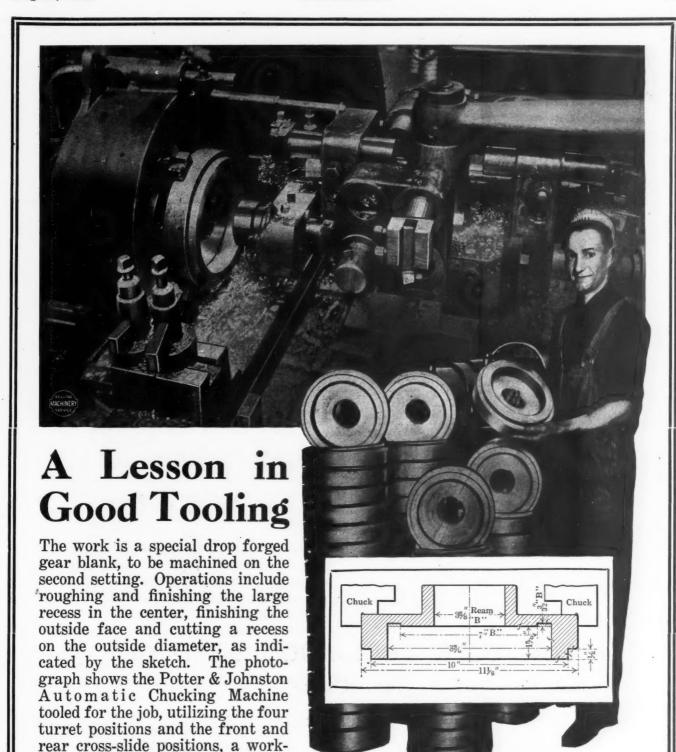
Eccentric Shafts
Side and Main Rods
Crank Pins
Axles
Fact Straps
Guides
Parts of frame both in iron and steel
Iron Bars for locomotive
Repairs

Marine Shaft
Marine Connecting and Eccentric Rods

Rolls

Rending
Feed
Straightening
Embossing
Large Wrenches
Saw Arbors
Steam Engine Forgings
Pump Crank Shafts
Pump Connecting Rods

AMDEN FORGE CO Mt.Ephraim Ave., CAMDEN, N.J.



# Potter & Johnston — The Manufacturing Automatic

ing combination that makes this accurate bit of turning an exceed-

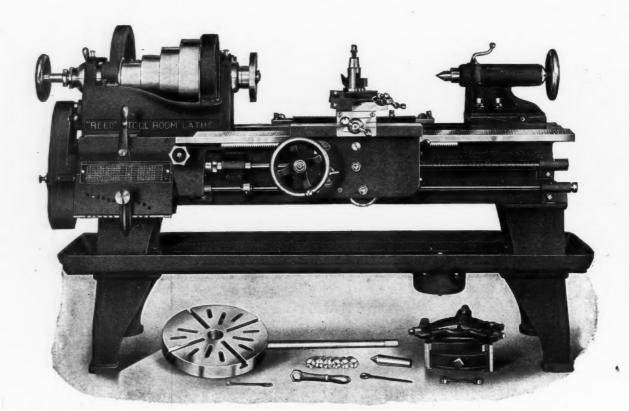
ingly rapid performance.

This machine can be tooled to handle work entirely outside the range of other lathes. All operations are automatic, one operator runs several machines; design is simple; machines are rapid, strong, durable and can be relied upon to lower costs. If the high cost of turning good work fast is one of your problems, write us.

#### POTTER @ JOHNSTON, Pawtucket, R. I., U.S.A.

OFFICES AND REPRESENTATIVES: Office for Great Britain and France: 68 Avenue de la Grand Armee, Paris, J. Ryan, Manager. New Yor Office: Fulton Bidg., 50 Church St., Walter H. Foster Co., Managers. Detroit Office: Modern Machinery and Engineering Co., 1514 Ford Bidg. Chicago Office: 4213 Sheridan Road, Chas, H. Shaw, Manager, Toronto Office: 1501 Royal Bank Bidg., E. C. Roelofson, Manager, FOREIGN AGENTS: Chas. Churchill & Co., Ltd., London, Birmingham, Manchester and Newcastle-on-Tyne, England, and Glasgow, Scotland. Ercole Vaghi Corso Porta, Nouva 34, Milan, Italy.

# PEED-DRENTICE COMPANY WORGESTER MASS. U.S.A.



# FOR YOUR TOOL-ROOM NEED GET A "REED"

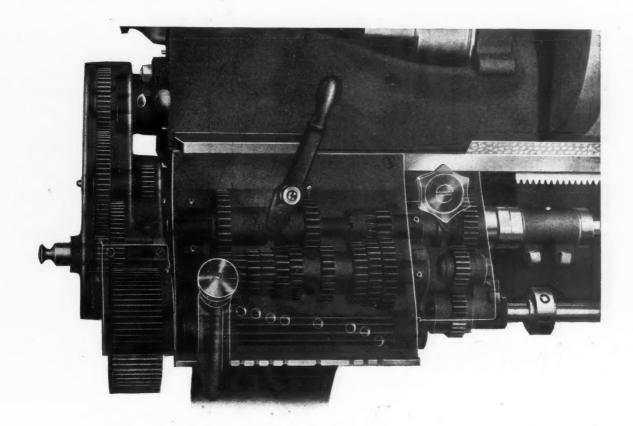
BECAUSE

FROM FOUNDRY TO FINAL INSPECTION YOU CAN ALMOST SEE THE WORD "ACCURACY" PERSONIFIED IN EVERY ACT THAT TAKES PLACE IN THE MAKING OF THESE LATHES.

THAT WORD SO OFT REPEATED IS THE VERY SPIRIT OF ALL "REED" PRODUCTION, AND WHAT THEY ABSORB IN THEIR MAKING THEY GIVE OUT IN RESULTS.

YOU WILL FIND IN MOST TOOL ROOMS THAT THE CARE-FUL JOBS GO TO THE BEST WORKMAN AND THE "REED" LATHE, FOR THE SAME REASON THAT A SURGEON DOES NOT USE A PEN-KNIFE WHEN BETTER TOOLS ARE AVAILABLE.

# PED-DRENTICE COMPANY WORCESTER MASS. U.S.A.



# THE "REED" QUICK-CHANGE GEAR SHOWN ABOVE

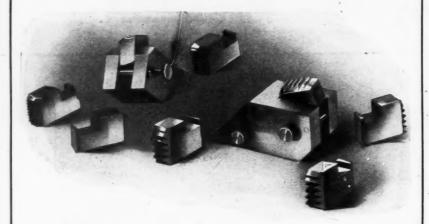
GIVES 60 CHANGES OF FEED AND 60 THREAD CUTTING VARIATIONS. THREADS FROM 2 TO 128 PER INCH ARE AT INSTANT COMMAND.

THE LEAD SCREW AND FEED ROD CANNOT BOTH ROTATE AT THE SAME TIME, AS CAN BE SEEN FROM THE X-RAY VIEW ABOVE.

YOU CAN EASILY SET TO THE CORRECT THREAD OR FEED BY READING THE MISTAKE-PROOF INDEX PLATE ATTACHED TO THE GEAR BOX. WHITWORTH-METRIC OR U. S. STANDARD LEAD SCREWS CAN BE SUPPLIED AS ORDERED.

MANNING, MAXWELL & MOORE, INC., NEW YORK ALLIED MACHINERY CO. OF AMERICA, PARIS FENWICK FRERES, PARIS

# Chasers for Hartness Dies Are Easily Ground



These jigs are supplied gratis with new dies, and are sold separately at modest prices.

Full instructions for grinding chasers are sent with chasers.

A special grinder for this purpose is not required.

These Jigs and
Any
Small Grinder
will Grind
Hartness Chasers
Quickly
and Correctly

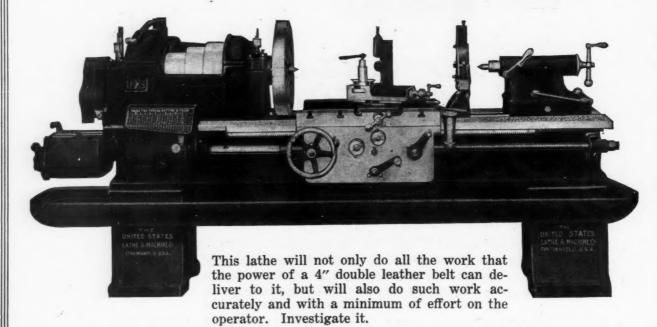
## JONES & LAMSON MACHINE CO.

AUTOMATIC DIE DEPARTMENT

109 QUEEN VICTORIA ST. LONDON, ENG. SPRINGFIELD VERMONT, U. S. A.

AMERICAN AGENTS FOR DIES AND CHASERS
Barwood-Richards Mchy. Co., Bourse Building, Philadelphia.
Boyer-Campbell Co., Detroit.
Carey Mchy. & Supply Co., Baltimore.
E. L. Essley Mchy. Co., Chicago.
The E. A. Kinsey Co., Cincinnati and Indianapolis.
Machinists Supply Co., Pittsburgh.
Pacific Tool and Supply Co., San Francisco and Los Angeles.
The W. M. Pattison Supply Co., Cleveland.
Robinson, Cary & Sands Co., St. Paul.
FOREIGN AGENTS
For France, Spain and Belgium; F. Auberty & Co., 91 Rue de Maubeuge, Paris.
For Holland: Spliethoff, Beeuwkes & Co., Rotterdam.
For Australia: McPherson's Pty., Melbourne.

#### "United States"—Lathes for Service



The United States Lathe & Machine Co. CINCINNATI, OHIO, U. S. A.



Fine Die Heads for Fine Threads

> Modern Self-Opening Adjustable Die Heads, recognized as standard for thread cutting, are regularly made in sizes with capacities from 1-16" to 5 1-2" diameter. Larger sizes to order.

> > Modern Die
> > Heads are
> > found in every
> > conceivable line of
> > manufacture; the
> > photograph illustrating
> > an instance of their adaptability. This picture was
> > secured in the plant of one of
> > the country's foremost safe and
> > vault builders, where all the screws
> > used are threaded by the Modern
> > Die Head.

This particular job is threading 34" x 1"—
14 pitch steel screws. Production is 1600 in
10 hours—every thread perfect in dimension
and clean cut.

Use Modern Die Heads for maximum efficiency and accuracy on your thread cutting. Send for the facts.

MODERN TOOL COMPANY

Main Office and Works:

SECOND AND STATE STS.

ERIE, PA., U.S.A.

Chicago Office: 32 N. Clinton St. Detroit Office: 1223 Dime Bank Bidg. New York Office: 2 Rector St. F. Wesley Parker, Residence Engineer and Export Agent, 2 Rector St., New York.

# Here's A Profitable Battery of Farwell Gear Hobbers



Profitable not only in the sense that they do their work well, but that they do it with remarkable economy. The machines are nine Farwell Gear Hobbers owned by the Stewart-Warner Speedometer Corporation, Chicago, Ill. The work is forged steel gears, average diameter 4", ½" face, ranging in pitch from 6 to 8, with special emphasis on accuracy and all the speed possible. Production per day of 8¾ hours averages 65 gears, each machine. The work is economically done, because a Farwell Gear Hobber never requires all of an operator's time. Once the work is set up and the cut started, the machine requires no further attention till the gear is completed. In many instances one operator looks after four busy machines.

Farwell Gear Hobbers are simple, efficient, powerful, rugged—record producers, profitable machines in every sense of the word.

If you buy or make gears, let us tell you more about Farwell Hobbers.

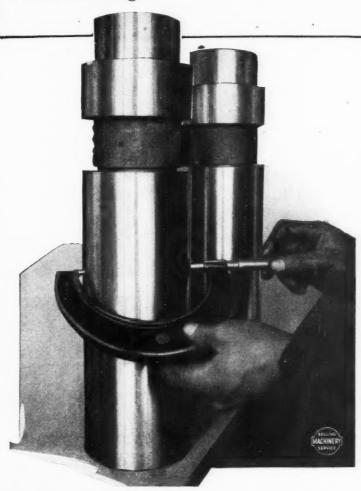
THE ADAMS COMPANY, 1903 MARKET STREET DUBUQUE, IOWA, U.S.A.

#### What the Slocomb Says is Right—The Inspector Marks O. K.

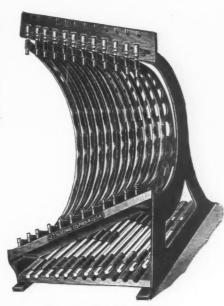
Requirements were never more severe as to accuracy, and by the same token, never were more Slocomb Micrometers in use. Manufacturers whose business is accurate production are not taking chances—they're making sure. And in an increasing number of cases they are making sure with Slocomb Micrometers, because they meet the current demand.

Slocomb Micrometers are true—absolutely true—with the strength to stand up to the usage popular tools get in busy shops. The drop forged I-section frame combines strength with lightness; the Slocomb screw is hard tool steel working in a nut giving four times the bearing surface found in other micrometers.

The Slocomb is "the longest lived micrometer that can be bought."







No. 28—12 to 24 Inches Set of Micrometer Calipers

Write for Catalogue No. 15.

#### J. T. Slocomb Company

Providence, R.I., U.S.A.

Representatives in England: Chas, Churchill & Co., Ltd., London, Birmingham, Manchester, Newcastle-on-Tyne and Glasgow.
Representatives in Japan: Alfred Herbert, Ltd., Yokohama.

Yokonama. Representatives in Italy: Chas. Civita, Milan. Representatives in Australia: Edwin Wood, Pty., Ltd., Melbourne and Sydney.



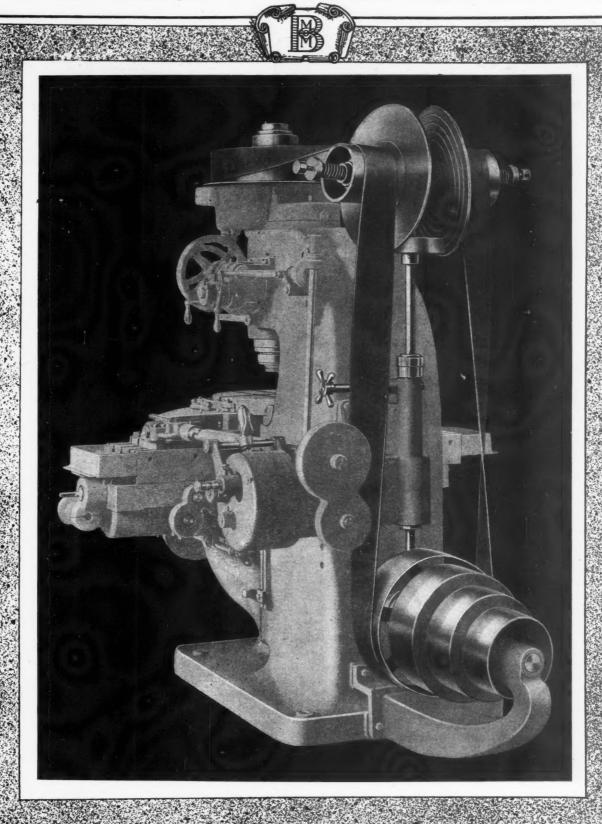
# BECKER Milling Machines THE DRIVE

Transmission gears—power wasters, noise and trouble makers—have been entirely eliminated from the Becker Drive. A large pulley, driving a wide belt at high velocity, delivers an abundance of power direct to the spindle. This gives smoothness and flexibility not possible with a geared drive, besides saving from one-half to two-thirds of the power.

The Becker Roller Feed is operated by a cone rolling between two friction discs and held in positive contact by the combined action of powerful springs and the driving belt. Infinitesimal changes of feed are obtainable from .003" to 1.245" per revolution. The increase or decrease is made smoothly and without shock and without stopping the machine. The most profitable feed for every job is always available. We shall be glad to talk over Becker possibilities with you. Write us.

#### BECKER MILLING MACHINE

AGENTS: Manning, Maxwell & Moore, Inc., New York, Pulladelphia, Pittsburgh, Chicago, St. Louis, San Francisco,



# COMPANY, Hyde Park, Mass. AGENTS: H. B. Slate, Hartford, Conn. National Supply Co., Toledo, O. Selson Engineering Co., Ltd., London, Turin and Melbourne. Allied Machinery Co. of America, Paris.



No. 107 Multiple Turning Head

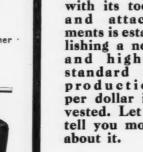




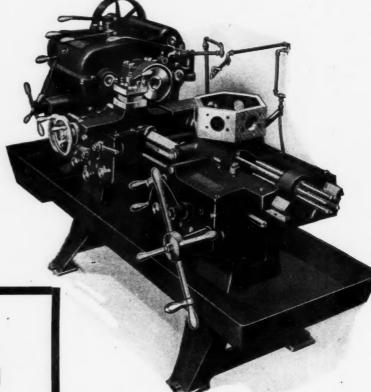
Push-Out Collet with Bushings



No. 139 Multiple Cutter Turner







No. 142 Center Drilling Tool



No. 120 Adjustable Drop-off Tap Holder



No. 143 . Knurling Tool



No. 149
Rear Forming Tool
Holder



#### The Foster 1-B Universal Turret Lathe

A machine that is adapted for manufacturing in large quantities as well as producing a wide variety of parts in small lots-a machine that brings to its work tremendous power, rigidity and strength. The Foster 1-B is provided with a complete and extensive equipment of standard tools and attachments, and with means for handling work of more or less special nature. Range includes bar and chucking work, from wide forming in steel to turning hard cast iron of large diameter. As many as twelve cutters can be mounted on the two tool carrying units; turret and cross slide can be operated simultaneously and independently with widely different feeds. A carefully devised arrangement of operating helps aids in maintaining a high rate of production.

FOSTER MACHINE COMPANY ELKHART, INDIANA, U.S.A.









# Every Belt A DUXBALA

NTER any one of the hundreds of shops where machines are used in quantity and you confront a veritable "forest" of belt drives.

In such places DUXBAK prevents a multiplication of power losses, and insures uninterrupted maximum production. DUXBAK is immune to water and oils and the failings of ordinary belts.

Why not speed-up permanently, as this great shop has done, by using DUXBAK everywhere? They have used nothing else for years.









HE broaching machine made by the J. N. Lapointe Co. scores again. At the J. I. Case Threshing Machine Company's plant, this time, broaching the bearings in transmission gears for 40 H.P. gas tractors. The gear is forged steel; bearing is 3" square by 12" long. Four broaches are required, 15 minutes complete the job. The official "communique" is "most satisfactory; profitable commercially."

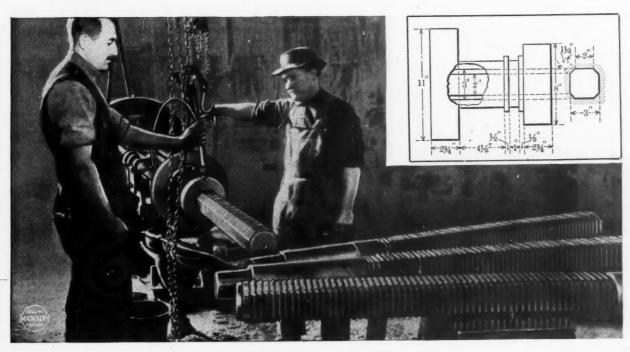
The fact that we have not only the name but the man himself, Mr. J. N. Lapointe originator of the Lapointe Broaching System, is a sufficient guarantee of the quality of our product.

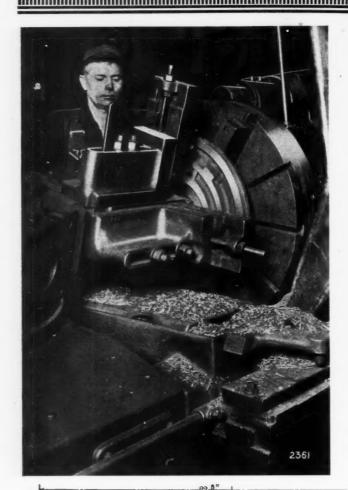
#### THE J. N. LAPOINTE COMPANY **NEW LONDON**

CONN., U. S. A.

#### Broaching Large Holes **Profitably**

Send blue prints, samples or sketches of your work





# Lowering Costs with a Gisholt Turret Lathe

The use of tool post and turret simultaneously is one of the means offered for lowering costs with the Gisholt Turret Lathe. The photographs herewith and the accompanying sketch illustrate this Gisholt practice. The machine is a standard 34" Gisholt Turret Lathe equipped with standard tools for finishing the piece shown in the line drawing as indicated by finish marks. The piece is the back plate for a 24" scroll chuck. It is of cast iron and must be finished within very close limits.

The tool post and turret are used simultaneously on this work, which makes possible the low production time of 19 minutes each for finishing the surfaces indicated. The time of 19 minutes covers the operation illustrated.

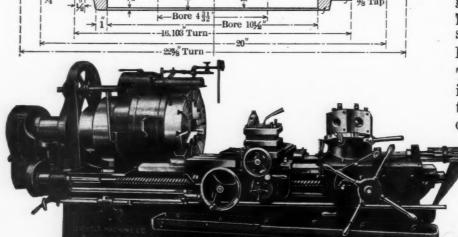
And these parts, when completed, are virtually self-assembling, and this, we claim, is the test of true efficiency in a machine tool. The Gisholt Turret Lathe has been simplified and perfected to such a degree that it produces finished parts so close to the required standard that hand-work is practically eliminated.

The Gisholt Engineering Staff is at your service. It is maintained for the purpose of cooperating with manufacturers

in an effort to reduce machining costs. We'll be glad to have you make use of it.

The "Gisholt way" is the economical way—try it.





#### GISHOLT MACHINE COMPANY

50 CHURCH STREET,

#### How Much Does It Cost per Year to Grind Your Tools

Never figured it out? It is a bigger item than you would think it could be—we can tell you that much without even knowing how many tools you grind.

Your machinists grind their own tools—every minute they are away from their machines is just so much time the machines are standing idle; every minute a man stands waiting to get at the grinder is just so much of his time wasted. And this waste, this unproductive time, costs many dollars per man each year. It totals an almost unbelievable amount in a big shop.



The Gisholt Universal Tool Grinder does away with this waste. It provides a correct mechanical means for grinding turret lathe, engine lathe, shaper, planer, boring mill and slotter tools—each tool at its correct cutting angles. It duplicates its work always. It establishes a standard of correct grinding angles. It keeps machine operators at their posts—eliminates this source of time waste by exchanging correctly ground tools for dull ones as fast as they are needed. There are other advantages; but the principal one is the savings this grinder accomplishes.

Dodge Bros. find it pays to use several Gisholt Tool Grinders; the photograph shows thousands of toolpost tools which have been reclaimed and, properly ground, are ready to be started through the shops again.

#### This machine gives you many advantages—

- -does away with idle machines and nonproductive work by machinists;
- —stops dull and unused tools from lying around machines;
- —cuts down your tool-steel investment by enabling you to get along with fewer tools;—stops loss of valuable tools;



- —gives you the increased production that comes from correctly ground tools;
- —gives you the saving that comes from reforging tools in lots instead of singly;
- —gives you general orderliness, the value of which cannot be overestimated.

No need to train anyone especially for the work. A boy can learn to operate it properly in a few hours.

1208 E. Washington Ave., Madison, Wis.

**NEW YORK CITY** 



#### LEVER QUICKER THAN SCREW CONTROL



Morris Lathes, 16, 18 and 22 inches, are made with single and double sliding back gears, special patented apron and four changes of positive feed. Complete specifications on request. We also make 21/2, 3 and 31/2 foot Radial Drills.

#### THE MORRIS MACHINE TOOL COMPANY

CINCINNATI

ENGLISH AGENTS:
A. A. Jones & Shipman, Ltd., Leicester, England

OHIO. U.S.A.

## Building the Universal Reputation A Series of "Cold Fact"



Same Machine
Same Work
Same Accuracy
for the past
Five Years

In the plant of the Continental Motor Company, Allentown, Pa., these three Universal Horizontal Boring Machines may be seen handling the same work they were doing five years ago, all showing the same degree of accuracy and high rate of production that characterized their operation then.

The work is on aluminum engine cases for Mack trucks—boring and facing three crank case bearings, three camshaft bearings and drilling two idler gear bearings.

Catalogue on request

The casting is mounted on a special boring fixture clamped to the machine table, boring all being done through the two bushed holes shown. The fixture has bushed support in the rear as well as front to facilitate operation and permit the use of the machine without rear support.

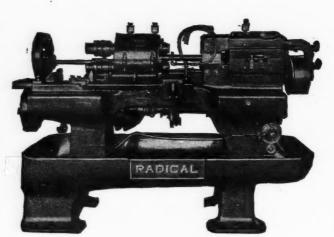
Rigidity, convenience, accuracy, durability—five years failed to develop a single weakness anywhere. Why not enjoy records like this, too?

UNIVERSAL BORING MACHINE COMPANY HUDSON MASSACHUSETTS, U. S. A.

### RADICAL FITCHBURG AUTOMATIC MACHINE WORKS

FITCHBURG, MASS.

We welcome visitors
who want proof that
The
Radical Automatic
is
Built Right



#### Fitchburg Model "A"

Compact, Economical and Rapid Grinding



No more power or time than is absolutely necessary for accurate results is used in grinding small, cylindrical work—straight or tapered—with a

#### FITCHBURG SIX-TWENTY

The machine has a wide range of speeds and feeds—made instantly available by centralized control. It is belt or motor driven—according to model—and is equipped with variable table dwell, positive stop, automatic cross feed and all features for economical operation.

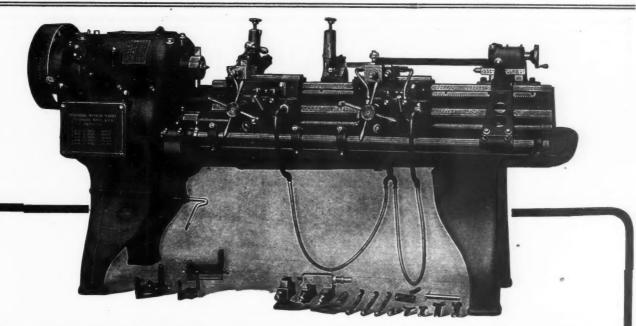
Compact design—requiring very small amount of floor space—adds another count to the good points of the Fitchburg Model Six-Twenty.

Further details in our catalog.

Fitchburg Grinding Machine Co.

76 Winter Street

Fitchburg, Mass.



#### Turning Rifle Barrels in 2½ Minutes

The accompanying sketch shows how the So-swing turns riflle barrels at the rate of 21/2 minutes apiece in one of the large rifle factories. A rifle barrel is admirably suited to the multiple turning idea, and the set-up shows just how the tools are arranged for handling the turning. Before coming to the So-swing Lathe, the barrel is spotted so that the roll rests may support it, and then the cutting tools get in their work. Notice that the extreme muzzle end of the rifle barrel is turned with a necking tool, and then the three tools that turn the tapered and straight sections start in. These tools are guided by a multiple former plate that gives the tapers and straight sections where they are required.

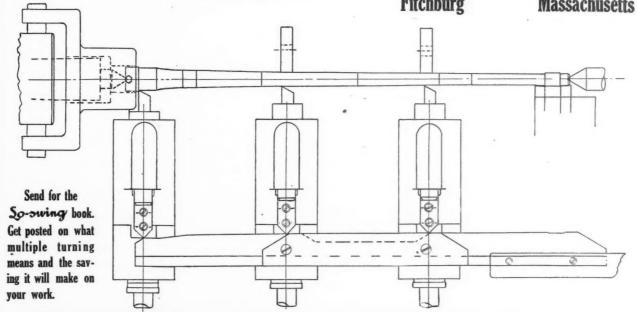
If you are interested in rifle barrel turning, or if you think there is any chance that you may be interested in rifle barrel turning, you will find we can give you some valuable information.

Perhaps your work is far removed from rifle barrel work. Perhaps you're turning camshafts, machine shafts, spindles, distance rods or other shafts that have many diameters. If so, you need to know about the **So-owing** Lathe.

# So-swing Lathe

The So-swing principle consists in turning simultaneously with a number of different cutting tools, each one of which may be adjusted to turn some particular diameter. There are two sizes of So-swing Lathes, one which takes work up to  $3\frac{1}{2}$  inches diameter and the other up to 8 inches diameter, and you can get any bed length required for your work.

### Fitchburg Machine Works Fitchburg Massachusetts





Machines for a Special Purpose



Millers





E have spent years of time and barrels of money in developing Ohio Millers for one special purpose—the low cost manufacture of such work as comes within the range of a knee type milling machine.

Ohio Millers possess the capacity, the structural power, the speed, convenience and accuracy necessary for maximum outputs at minimum costs. If you manufacture you can't find better machines. Let us tell you more about them.

The Oesterlein Machine Company

Cincinnati Ohio, U.S.A.



## Designers and Makers of Milling Cutters, Hobs, Dies, Jigs and Fixtures

If you use hobs and milling cutters of any shape or size we can make them for you.

If you have hobbing, gear cutting and milling problems to solve, our engineering department, which can give expert advice in this line, is at your service.

Michigan Tools are made right to form and carefully heat treated, insuring good work and long service.

MICHIGAN TOOL CO.

DETROIT, MICHIGAN



## At the Industrial Exposition and Export Conference

THE First Annual Industrial Exposition and Export Conference of the Allied Industries of the United States of America (that's the complete and official title) at Springfield, Mass., during the last week in June, was a most interesting and instructive affair.

The seriousness with which the problem of export trade was tackled and the character of the discussions on this subject were particularly gratifying.

#### Van Norman Machine Tools

were exhibited at Springfield. There is no reason why these tools shouldn't prove as popular on foreign soil as they have here. They are adaptable machines, highly accurate, with many exclusive features—popular because they are efficient.



Hand Milling Machines; Duplex Milling Machines in three sizes; Grinding Machines in seven types for grinding internal ball-race grooves, end thrust rings, external grooves, straight and taper holes, etc., etc.

Let us send circulars on any or all of these machines.



Van Norman Machine Tool Co.

Waltham Avenue

Springfield, Mass., U.S.A.



THE NATION PREPARED

NATIONAL Twist Drills and Tools play no small part in this gigantic undertaking

NATIONAL TWIST DRILL & TOOL CO.

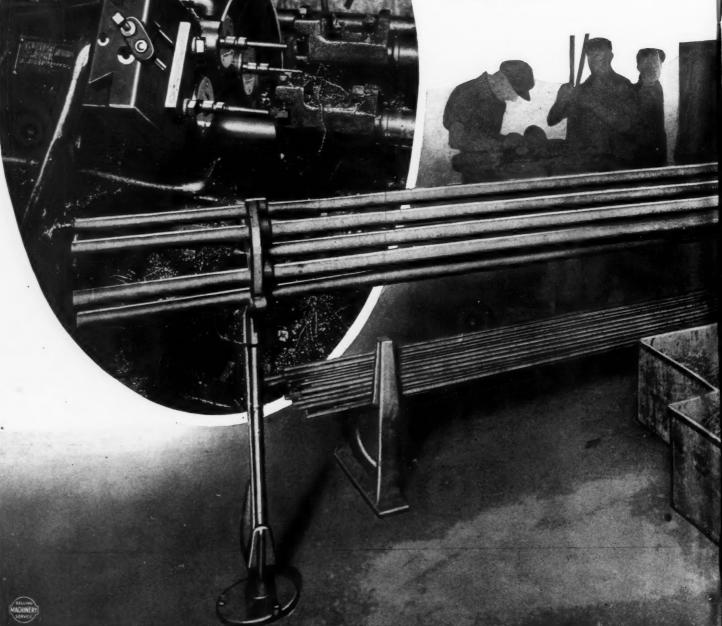
Detroit · Mich.

NEW YORK OFFICE 50 CHURCH ST.

CHICAGO OFFICE 104-106 SOUTH JEFFERSON ST.



Making the Worm Shaft for Stewart-Warner Speedometers



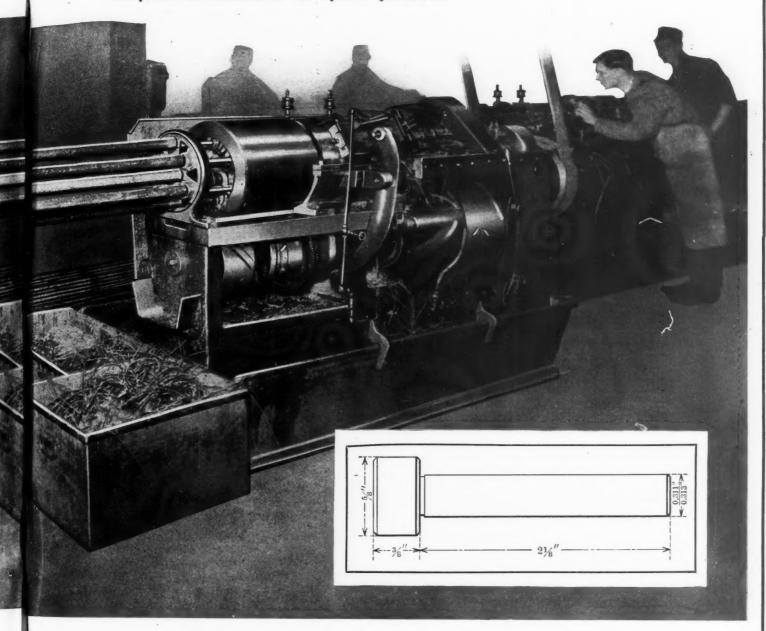
THE NEW BRITAIN MACHINE

### BRITAIN SIXES"

In every Stewart-Warner speedometer there's a worm-shaft that looks like the sketch below before the worm is cut. It is made from 5/8" round cold-rolled steel, and the turned dimensions are held to a tolerance of 0.002".

"New Britain" Six-Spindle Automatics produce these worm-shafts as well as other similar parts for the Stewart-Warner people. Two "New Britain Sixes" are shown—one operator taking care of both machines. The order of operations is as follows: First, feed stock; second, form; third, fourth and fifth, mill with box tool; sixth, cut off. Production is 220 pieces per hour from each machine. This remarkable output is made possible by the "New Britain's" unequaled tooling capacity, which permits the use of three box tools for milling the shaft.

Attention is called to the fact that, whereas it was formerly necessary to grind these shafts, the "New Britain" turns them out so smooth and accurate as to obviate the necessity of this extra operation. If you are not familiar with the advantages of the "New Britain," send samples of blueprints for estimates of "Six-Spindle" production.



CO., New Britain, Conn., U.S.A.

#### Foote-Burt High Duty Drills



With all the forces of the United States organized for offense and defense, American manufacturers are facing the busiest and most important period of industrial history. Their prime need is machines—good machines, machines built like the Foote-Burt No. 25 High Duty 24" Drilling Machine.

The No. 25 is as rigid as a machine can be made, modern to the smallest detail, and drives high speed drills, up to 3" size, to full cutting edge capacity. All speed and feed changes are made through quick change gear device of special design; spindle is of forged high carbon steel, fitted with ball bearing thrust of our own design, guaranteed not to crush under the severest duty. All levers are within easy reach. Briefly, the function of this machine is to work hard and keep at it.

#### THE FOOTE-BURT CO., Cleveland, Ohio

MILWAUKEE OFFICE, 424 Wells Building. DETROIT OFFICE, 806-8 David Whitney Building

FOREIGN AGENTS: Buck & Hickman Ltd., London, Birmingham, Manchester and Glasgow, Moscow Tool & Engine Co., Moscow, Ing. Ercole Vaghi, Milan. R. S. Stolvis & Zonen, Ltd., Rotterdam. R. S. Stokvis & Fila, Brussels. Glaenzer & Perreaud, Paris, agents for France, Switzerland, Spain and Portugal. Benson Bros. Ltd., Sydney, Australia, agents for Australia and New Zealand. Mitsui & Co., Australia, agents for Japan, Korea and Manchuria. Wilh, Sonesson & Co., Ltd., Malmo, Sweden and Copenhagen, Denmark.



How Do You Hold Your Wood-ruff Keyseat Cutters and Other Tools with 1/2" Straight Shanks?

#### LOOK

This chuck is made with a taper shank either B & S or Morse to fit the spindle of your machine. The design is such that the jaws do not fall together, but allow free entrance of the shank at all times.

Send for our catalogue and get acquainted with our tools.

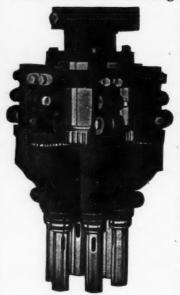
#### THE ADVANCE TOOL CO.

Canal & Jackson Sts., Cincinnati, Ohio

Agents wanted in all principal cities

#### With the Covington, Eight Holes Cost No More than One

This Multiple Drill Head is a "sure fire" production booster. It changes single drill output



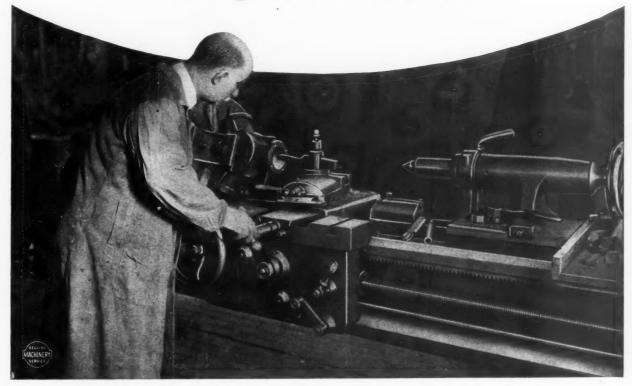
to multiple in a minute's time and with practically no additional expense. The head, furnished with from 2 to 8 spindles, can be easily adjusted to any upright drill press from 20" to 36" in size, or to large radials, and each spindle "stays put" after adjust-ment. The Covington is sturdily built throughout, handles a great variety of drilling, gives lasting service.

Circulars and Free Trial Offer Sent on Request

Covington Multiple Drill Company 2449-53 W. McMicken Ave. CINCINNATI, OHIO

#### THE ROULSTED TWENTY

### On Jobbing Work—an Adaptable Lathe



The Barbour-Stockwell Company, Cambridge, Mass., makes good use of the Roulsted Lathe. When the investigator paid the company a visit recently, here's what he saw. A cylinder casting for an oil engine strapped on an angle iron on the faceplate of the Roulsted ready to be bored out. Three cylinders were bored, the casting being re-set for each operation. Aside from the quick work of the lathe, the overhang from the faceplate is the interesting feature of this job. Roulsted spindle construction, however, is a marvel of strength. It will support work adequately at even a greater distance from the faceplate.

The Roulsted Twenty is a heavy allaround engine lathe, built by specialists. Carriage has full length bearing on the vees; apron is of double-plate type. Actual swing over bed 21", over carriage 14".



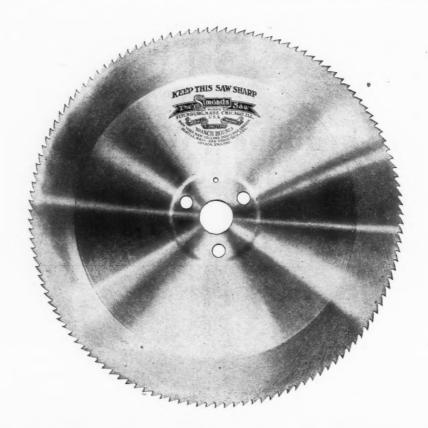
If the Roulsted Lathe is new to you ask for details

**EXCLUSIVE SELLING AGENTS** 

HILL, CLARKE & COMPANY, Inc.

BOSTON, MASS., 156 Oliver St.

NEW YORK CITY, 136 Cedar St.



# SIMONDS METAL CUTTING SAWS

Every firm using Metal Cutting Saws, Metal Slitters, Screw Slotting Saws, or Inserted Tooth Metal Saws, should find an opportunity to prove to itself that the Simonds Special Blades, which we now manufacture in large quantities, of our own steel and in our own factories are unquestionably superior and economical saw blades.

Write for Metal Saw catalog.

#### Simonds Manufacturing Company

17th Street & Western Ave.
CHICAGO, ILL.
NEW YORK CITY
PORTLAND, ORE.
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"THE SAW MAKERS" FITCHBURG, MASS.

(ESTABLISHED 1832)

NEW ORLEANS, LA. SAN FRANCISCO, CAL. St. Remi St. & Acorn Ave.
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MEMPHIS, TENN.
SEATTLE, WASH.
ST. JOHN, N. B.
LONDON, ENGLAND

# WOOD WORKERS BENCHES



#### If You Can Use a Bench at all, You Can Use the Best One Made, to the Best Advantage

Our "B" Bench as illustrated has for years been the standard. Made of thoroughly kiln dried maple, except the vise screws, which are of second growth hickory.

Tops, exclusive of vises, are 75 inches long, 24 inches wide, 2¾ inches thick, with 7 inch recess. Height 33 inches. Has two iron stops. Head vise is 18 inches wide and opens 12 inches. Tail vise is 6 inches wide, opens 10 inches. Weight 190 pounds.

We also carry all kinds of vises, hand screws and clamps and wood working tools and accessories, and, of course, our full line of metal working tools and bolts, nuts, screws, etc., etc.

Send for Catalog No. 86 of "Benches."

#### HAMMACHER, SCHLEMMER & CO.

HARDWARE, TOOLS AND SUPPLIES

NEW YORK, Since 1848

4th Avenue and 13th Street



WINNER OF THE ONLY GRAND PRIZE THE TOOL HOLDER CLASS







Use High Speed Steel efficiently and economically, and are made in a range of sizes suitable for all classes of work, light or heavy





#### Single Screw, Quick Action Boring Tool

always ready to use, very stiff, will bore close up to shoulder or bottom. Strain of cut tightens cutter. 7 sizes.







howing Tool cutting an internal thread



#### Armstrong Adjustable Boring Tool

This tool combines Convenience, Adjustability and Rigidity to a remarkable degree and is well adapted to a very wide range of work. The holder is easily adjustable to different heights and will hold bars of various diameters. The bars are made from high carbon steel seamless tubing of heavy gauge and are extremely stiff. The cutter can be adjusted and solidly fixed at various angles for boring, facing or turning. Made in four sizes.





#### **Armstrong 3-Bar Boring Tool**



The many points of advantage of this lathe attachment will be appreciated by practical machinists. A slight turn of one nut re-leases or fastens both bar and holder. Bars can be changed as needed almost instantly, thus allowing the operator to use the stiffest bar possible for each job, with the result that speeds and feeds can be increased and time saved. Made in four sizes.



#### **Armstrong Boring Tool Holder** For Small, Light Boring, Threading, Etc.

This tool will be found very handy in the tool room or in boring work of small in-ternal diameter, threading, brass turning, The boring bars furnished are made from the best tool steel properly hardened, tempered and ground ready for use. The holder is reversible, and can be used for turning either right or left hand. Made in four sizes.





A Boring Tool for Every Requirement. Write for Catalog.



MSTRONG BROS. TOOL

"THE TOOL HOLDER PEOPLE"

BIR N. FRANCISCO AVE.

CHICAGO, U.S.A.

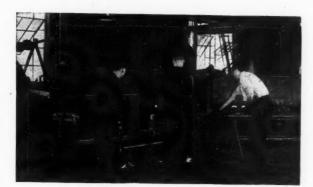


# "Doing Their Bit"

In this time of the nation's need, AJAX, like every manufacturer, takes a pretty careful inventory to find out just where he is helping and where he can help more. This is the result.

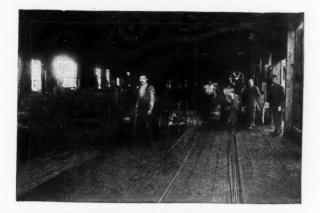
### AJAX

Trade Mark Registered



#### Forging Machines

They are not only playing an essential part in rapid production of actual fighting equipment, rifles, shrapnel, etc., but they are speeding up production and cutting cost in railroad shops, automobile plants, implement factories and other vital industries.



#### Reclaiming Rolls

On the country's biggest railroads, these rolls are turning scrap into new bars at a rate of 6 to 25 tons per day. They increase by that much the amount of steel available and release an equal tonnage for use in other vital industries.



#### Heading Machines

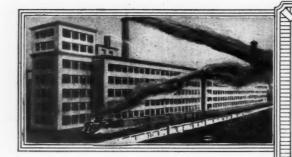
They are producing rivets and bolts, especially for ship building, car building, track work, etc., at the rate of 28,000 to 42,000 per ten hour day. The rivet is a small but a mighty important factor in this part of Uncle Sam's program.

Put your war production problem up to Ajax Engineers—they can, and will, give it special attention

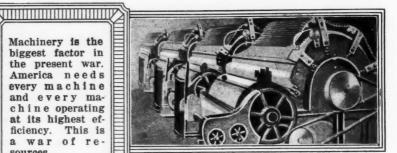
#### THE AJAX MFG. COMPANY

621 Marquette Bldg. CHICAGO, ILL. CLEVELAND, OHIO

1369 Hudson Terminal NEW YORK CITY



Machinery is the biggest factor in the present war. America needs every machine and every machine operating at its highest efficiency. This is ficiency. This is a war of resources.



#### Your Machinery is Now a National Asset

America is facing the task of feeding, clothing and equipping her Allies. Every wheel in America must be kept turning. Every machine must be regarded as a national asset and be kept "fit."

You know the resources of this great country. Do you realize the need of conserving them?

Consider the nation's oil supply. It must not be wasted, for America needs every drop of oil she can produce. Every plant owner can perform a national service by avoiding waste in lubrication.

Every plant owner must be economical in his purchase of oils.

He must be economical but not pennywise. Use good oils. It is real economy. Be sure you get the oil best suited to your needs. . Thousands of dollars, and thousands of gallons of oil can annually be saved by eliminating the "hit or miss" method of using and purchasing oils.

For every power plant, for every phase of the production of electrical energy, there is one best oil. Its use means a better manufactured article, greater production, less wear and tear on equipment and reduced overhead. The present crisis demands that you keep all these considerations in mind.

#### SWAN & COMPANY

We feel that sixty-five years' experience in the oil business qualifies us to be of real service to manufacturers of the nation in this crisis.

We know that scientific attention to oil problems will save large sums to the nation and all its manufacturers. And so we offer to help American industry maintain its topmost efficiency. We have an engineering department composed of men who know oiling problems from A to Z. These men have studied the oils you should use for various processes in your plant. Their advice will save oil and money and increase your plant efficiency. It is free for the asking.

Write us full details of your plant equipment, so that our engineering department can make individual recommendations. Or, if you prefer, we will send you booklets on the various phases of oiling and lubrication, indicated below.

Just mark what you want on the attached coupon and return to us.

SWAN & FINCH COMPANY, 165 Broadway, New York City. Please send booklets checked.			
Engine Lubrication Steam Cylinder Lubrication Crank Case Engine Lubrication Turbine Lubrication Gas Engine Lubrication	Dynamo and Motor Lubrication Compressor Lubrication Shafting Lubrication Machinery Lubrication Spindle and Loom Lubrication Transformer and Oil Switch Insulation	☐ Ice Machine Lubrication ☐ Car Journal Lubrication ☐ Printing Press Lubrication ☐ Automobile Lubrication ☐ Cutting Oils and Compounds ☐ Grease—Where and why?	Tempering Oils Core Oils Wool Oils Leather Oils and Greases Plater's Cleaning Compound
Please send your representative to personally discuss lubrication of the machinery checked.			
Firm Name			



know.

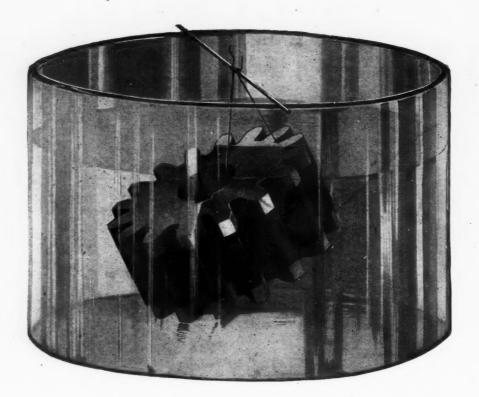
The picture shows a setup of Celfor Drills nosing their way through the flange of a 5½" x 16"

Triplex Plunger Pump. Eight drills find their way through a solid two-inch flange in one minute and forty-five seconds—and only one grinding each day.

That is drill economy and a production record of an unusual sort—yet common enough for Celfor Drills. The Goulds people use them on every job where holes are ½" or over. There are sound reasons why. Let us tell you of them.

#### CLARK EQUIPMENT COMPANY

Successor to CELFOR TOOL COMPANY BUCHANAN, MICHIGAN, U.S.A.



#### It Must Be a Fabroil Gear

Convince yourself of the ability of a **Fabroil Gear** to withstand atmospheric changes.

Put it through "the third degree." Immerse it in water—or oil. Heat it on the radiator and put it out in the cold. Turn a steam jet on it. Prove it to your own satisfaction.

Fabroil Gears come out of tests like these unchanged, retaining all their excellent qualities. You never have to guard against deterioration by long storage; consequently you can stock Fabroil Gears with perfect safety and so guard against loss of time in the day of accident or rush orders.

#### General Electric Company

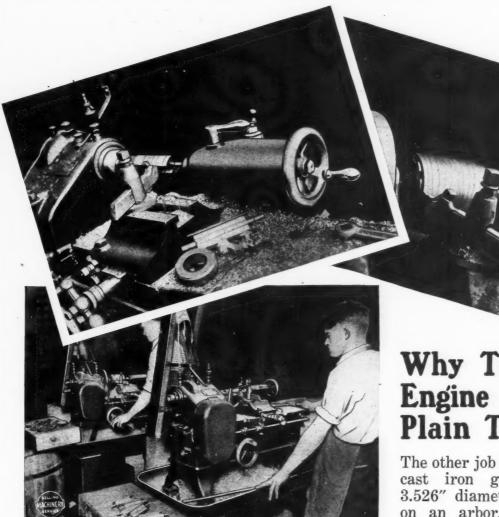


General Office: Schenectady, N. Y.

Sales offices in all large cities



5814



# The P-C Manufacturing Lathe

Just as fast, just as efficient and immeasurably more economical is the Porter-Cable Manufacturing Lathe. Here are two P-C Lathes at the Stromberg-Carlson Telephone Manufacturing Company's plant, Rochester, N. Y. One is turning armatures; (92 punched steel blanks) the cut is intermittent; the diameter must be 1.480", held with a 0.001" limit. The operator starts the cut across the armature at a speed of 140 r. p. m. and a feed of 0.040" per revolution, and goes right on filing armatures that have already been turned. All he does to the machine is take off finished work and start new work.

## Why Tie up an Engine Lathe on Plain Turning?

The other job is turning rough cast iron generator gears, 3.526" diameter, mounted 12 on an arbor. About 1/16" stock is taken off; limit is within 0.001" of standard size. When the blanks are finished the operator takes them, arbor and all, over to the two gear cutting machines that cut the teeth. He keeps them going in addition to his P-C Lathe and is by no means overworked.

Porter-Cable Manufacturing Lathes are practical, hardworking machines. They take big cuts, turn big chips, insure big output. They save money on work not over 9" diameter by 18" long, and are ideal for duplicating parts in quantity.

We'll be glad to go over P-C advantages in detail and tell specifically what our machines are doing for others. Write us.

#### The Porter-Cable Machine Co. SYRACUSE N.Y., U. S. A.

Foreign Representative: Benjamin Whittaker, 2 Norfolk Street, Strand, London

#### **AMERICAN GAS FURNACES**

#### The Sure Furnaces

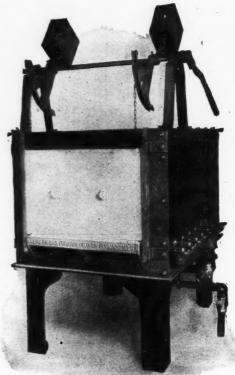
No guesswork with these machines—a heat treating operation under "American" Gas Furnace methods is an assured success. Every factor necessary for the proper handling of expensive material has been assured—perfect temperature control by means of our Automatic Controller, even fuel consumption, and quick, uniform, direct heating. This furnace for annealing, hardening and case-hardening is typical of "American" construction and a sure producer of high-grade work.

We make furnaces for every heat treating purpose and they're all listed in the catalog. If you're interested in better heat treating results, get a copy and select "sure" furnaces for your work.

#### American Gas Furnace Co.

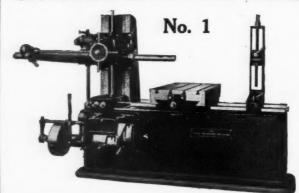
24 John Street

**New York City** 



Made in Various Sizes

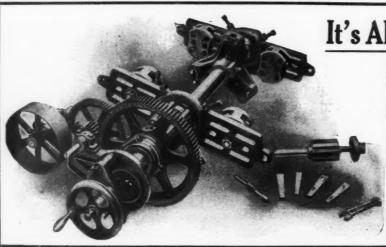
#### Cleveland Horizontal Boring, Milling and Drilling Machine



In this machine all the handles are conveniently located and are operated from a natural working position. A single handle provides a complete change of either feed or speed, the same pilot wheel controls both slow hand feed and quick traverse of the bar; all speed and feed changes are made while the machine is running, spindle can be stopped, started and reversed instantly. There are 16 feeds and 12 speeds, all gears are steel and fully enclosed.

Full details on request.

The Cleveland Machine Tool Works
CLEVELAND, OHIO, U. S. A.



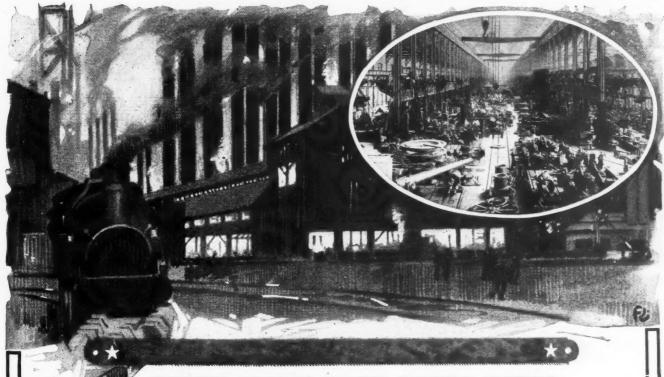
It's Always Well to Be Prepared

Don't run the risk of having to shut down every time a cylinder needs reboring—Add an UNDER-WOOD PORTABLE BORING BAR OUTFIT to your equipment. No need to dismantle the machine—simply remove the piston, attach the Underwood and bore.

We designed this machine primarily to fill a need in our own shops and are confident there is work enough for it in yours to keep it busy between emergencies.

Send for Complete Catalog of Underwood Tools

H. B. UNDERWOOD & CO.
PHILADELPHIA Est. 1870 PENNSYLVANIA



BETHLEHEM CUTS STEEL WITH FASTEST CUTTING HACK SAWS

HAT the Bethlehem Steel Co. uses STAR BLADES is vitally significant for every manufacturer who saws metal. Because every tool the famous Bethlehem plant uses has first had to prove beyond question its ability to help extend their output to the last notch.

You who are buying hack saw blades today-whether machine or hand bladesmust realize that in last analysis you are not buying blades at all but the output those blades will give you. It is not a question of getting blades at the lowest cost, but of getting blades that will give you the maximum number of cuts at the lowest cost.



#### 🗇 STAR HACK SAW BLADES 😭

#### Machine and Hand

were the first modern blades ever manufactured. and for thirty years they have held their quality supremacy. Hundreds of thousands of tests have been made to determine out of thousands of combinations exactly what relative dimensions, what shape and setting of teeth and what kind and hardness of steel would give the best cutting results.

Our special automatic machinery with its gauges to the finest limits makes possible a uniform quality of production that ordinary methods could not give and an unbelievable quantity production at a minimum of factory cost. It is significant that the present standard practice with other hack saw makers was abandoned by us more than twenty years ago

#### Flexible and All Hard

for more efficient methods. The Star line includes machine and hand blades—flexible and all hard for every purpose. Whatever your metal sawing prob-lem, there is a Star Blade that will give you the greatest cutting efficiency at the smallest blade and time cost.

Prove this fact for yourself by making the most drastic tests or place the burden of proof on us and we will demonstrate the greater efficiency in Star Blades to your thorough satisfaction. The more difficult the problem, the more we will welcome the chance to show you.

Address our Engineering Department at 200 River St., Millers Falls.

#### \$500.00 FOR YOUR EXPERIENCE

Our position as authorities on metal sawing efficiency has made us a national clearing house of information on the results blade users are getting under all classes and kinds of conditions. To encourage this clearing house idea, we offer \$500.00 in gold for the best articles on "How I Test Hack Saws." Tell us your methods in detail (either on machine or hand blades) and give us

1st Prize 2nd Prize 3rd Prize

your conclusions with absolute truth and frankness, including some of the records of your results. It is not necessary to be a Star user to win a place in this prize award. We want your experience whatever it is. Get your reply in as early as possible. The best replies will be published in book form and in our advertising. Contest closes November 30.

Manufactured by CLEMSON BROS., Middletown, New York MILLERS FALLS CO., Millers Falls, Mass.

SOLE DISTRIBUTORS

### LEES-BRADNER COLLET TYPE THREAD MILLERS



Part of the Total Installation of Lees-Bradner The Accepted Standard For Munition Manu

THESE machines will cut a full thread up to a shoulder. In operation there is no reversal of rotating parts so that no time is lost on account of back lash. The lead screw is reversed once for about fifty pieces. These Collet type thread millers are adapted for milling internal or external

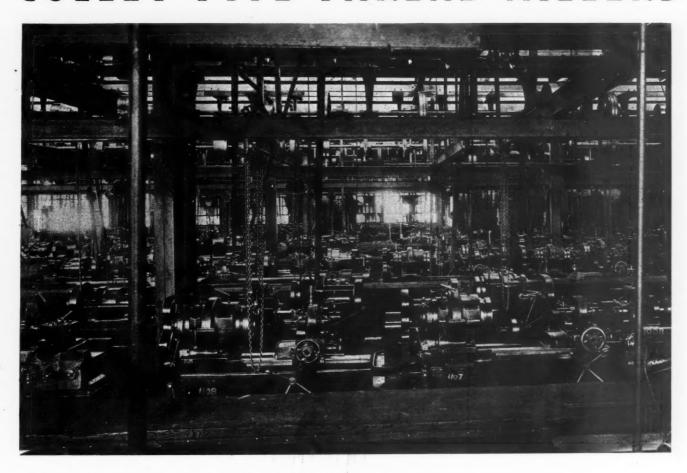
#### THE LEES-BRADNER COMPANY

CLEVELAND, U. S. A.

THREAD MILLERS

GEAR GENERATORS

### LEES-BRADNER COLLET TYPE THREAD MILLERS



Collet Type Thread Millers in One Plant facturers; Approximately 1000 in Operation

threads with a hob type cutter in one revolution of the work. The work is supported in a positive opening and closing Collet. Remarkable accuracy and production are obtained. Built in sizes up to 9½-inch Collet capacity. Send us blue prints of the work under consideration.

#### THE LEES-BRADNER COMPANY

CLEVELAND, U. S. A.

THREAD MILLERS

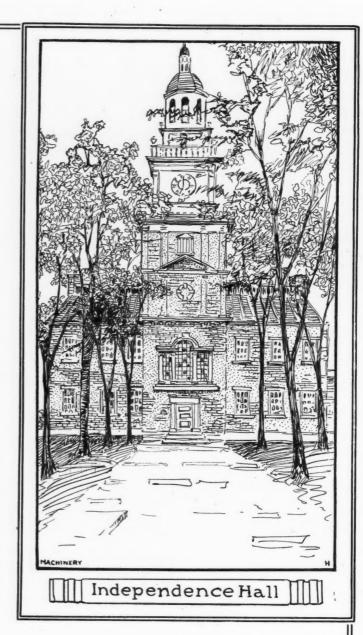
GEAR GENERATORS

# Two Stories of American Independence

NE is the story of National Independence and goes back to 1776 when the Signers of the Declaration proclaimed America free.

The other has to do with industrial independence—the freeing of American manufacturers from the handicap of uncertain supplies. The new country needed steel products of the highest grade. Hermann Boker & Company did their part to establish and maintain an adequate and accessible supply of the world's best steel specialties on American shores.

Right now we are pushing Gibraltar—"The Tool Steel without a risk." We recommend it, without qualification, for threading dies, taps, chasers, punches and dies, reamers, milling cutters, form cutters and other uses where high speed steels are unsatisfactory. We stake our reputation upon Gibraltar Tool Steel. In the 80 years of our experience we've never seen anything better. Try it. Ask for the booklet.



NOVO SUPERIOR
The Steel without an equal.

NOVO The standard in high-speed steel.

INTRA
The non-shrinking tungsten alloy tool steel.

GIBRALTAR
The tool steel without a risk.

#### H. BOKER & COMPANY, Incorporated

Successors to HERMANN BOKER & COMPANY

101 DUANE STREET

NEW YORK, N.Y.

CLEVELAND

CHICAGO

MONTREAL

PHILADELPHIA

BOSTON

ESTABLISHED 1837



as well as increased the quantity of it.

The piece is a wire basket for use in a dish-washing machine - 834 spot welds in all being made in the several baskets that go into one machine.

Walker Bros. Company, Syracuse, N. Y., reduced the time on this one particular job from eight hours to seven hours and bettered the quality of their product beyond comparison—with a Relectric Welder. The time to make one weld is about one second—quicker than it takes to tell about it.

This we has been in use over three years. It is a highly satisfactory installation from every point of view. We have the Walker Company's statement that it is indispensable for their work.

Believed Electric Welders pay big returns wherever they are used. They better both quality and quantity. Let us tell you more about them.

#### The Electric Welder Company WARREN, OHIO, U. S, A.

Manufacturers of All Types of Spot, Butt, Jump and Seam Welders, Electric Welders and Rollers for Safe Ending Locomotive Boiler Tubes

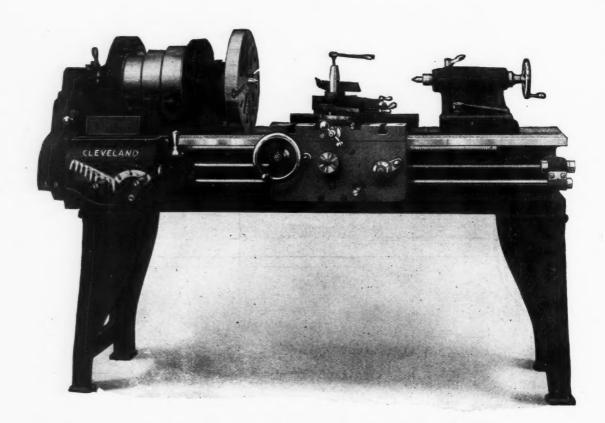
The airplane has reached a point in its development where it becomes, in the opinions of men who should know, the greatest single factor in the greatest war ever fought. It is confidently expected to prove the deciding factor. It is already known as the "Eyes of the Army" without which that army is almost helpless.

Manufacti

GREENBER



Courtesy of Pesacola Board of Trade



# Immediate Delivery! When? Now!

#### A LIMITED NUMBER READY TO BOX

Next to Workmanship and Design is Delivery. We have them ALL

Our lathes have margin enough to cover a large range of work. Built either as shown or with 4-step cone and single back gears. Heavy; extremely accurate; beautifully finished; all parts made to standard jigs and gauges; all interchangeable.

These lathes, owing to the large cone pulleys and wide bearings, are capable of taking extremely heavy cuts at coarse feed. We guarantee them to reduce 50 point carbon steel 1 3/4 inches at 1/16 inch feed.

We make ball bearing drills also, from 21" to 42". Send for Circulars

#### THE CLEVELAND MACHINERY & SUPPLY CO.

General Offices: CLEVELAND, OHIO

Factories: HAMILTON, O. COLUMBUS, O. RICHMOND, IND.

## GODDARD Milling Cutters and Hobs

Are Made Right

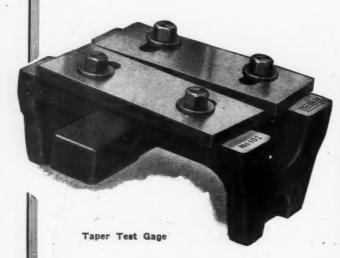
They Give Satisfaction

Quick Deliveries

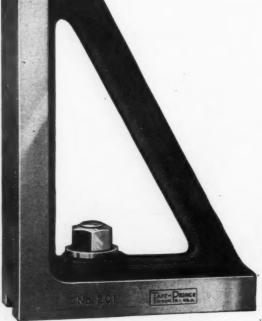
Goddard Tool Co.

Chicago, Ill. Detroit, Mich. U.S.A.

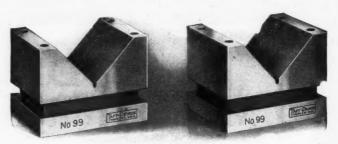




THESE and other T-P small tools are standardized and are manufactured in quantities. You can secure duplicates at any time.



Measuring Iron No. 200



Hardened Steel V-Blocks

# **TAFT-PEIRCE**Tool Room Specialties

In these days of shop activity, any factor or equipment which might help you keep output strictly in line with promises of delivery, should receive careful consideration. No shop aids have proved more efficient in this respect than Taft-Peirce Tool Room Specialties. If you are still making your own, the substitution of these tools will save buying extra materials, save work in your tool room, do away with congestion in tool room and the retarding of production sure to result. These specialties, manufactured in quantities and standardized, are unvarying in their accuracy.

A careful consideration of their advantages should convince you that real shop efficiency demands their adoption. Write for Catalogue B for further details.

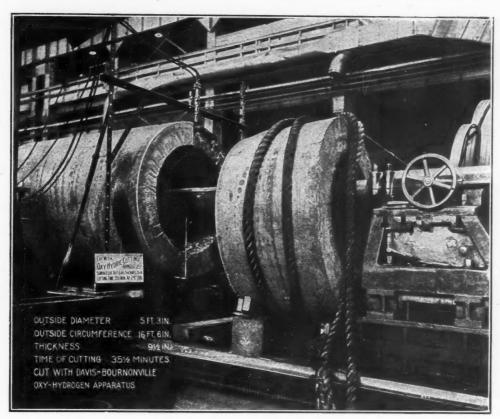
The Taft-Peirce Mfg. Co. WOONSOCKET RHODE ISLAND

New York, Woolworth Building Detroit, Majestic Building



Double-end Internal Limit Gage

# 50,000 lbs.—5-ft.3-in.diam.—9½-in.thick How Did They Cut It in 35½ Minutes?



(Photo by New York Shipbuilding Corp.)

It was cut with a torch and gas flame—Davis-Bournonville Oxy-Hydrogen Cutting Apparatus—in the New York Shipbuilding Yards; a cast steel rotor 14½ inches thick at the head, 5 inches thick at the foot, 9½ inches thick and 5 feet 3 inches diameter where it was cut—cut slick and clean as shown in the illustration, in 35½ minutes cutting time. It would have taken many hours, and been a considerable problem, by any other method. Davis-Bournonville Oxy-Acetylene and Oxy-Hydrogen Apparatus is applied successfully to the problems in metal working, and is in use by most of the big metal working concerns—foundries, steel mills, ship yards, navy yards, locomotive and car shops, munitions plants, sheet metal working factories, etc. Make inquiry about it, or write us.

"Davis Apparatus" Leads the World in Range, Efficiency, and Number of Successful Users



#### **DAVIS-BOURNONVILLE COMPANY**

General Offices and Factory, JERSEY CITY, N. J.

NEW YORK BOSTON PHILADELPHIA PITTSBURGH

-BRANCHES-

DETROIT ST. LOUIS SEATTLE SAN FRANCISCO TORONTO, ONT. (Carter Welding Co.)





Quality Files

for

Quality Work

FINE FILING not only requires special skill and a dexterous touch, but calls for files that are absolutely correct in shape and cut. American Swiss Files designed especially for the finer classes of work, give unqualified satisfaction and can be duplicated accurately,

There are now more American Swiss Files in use than at any time since they were first marketed.

Specify "American Swiss"

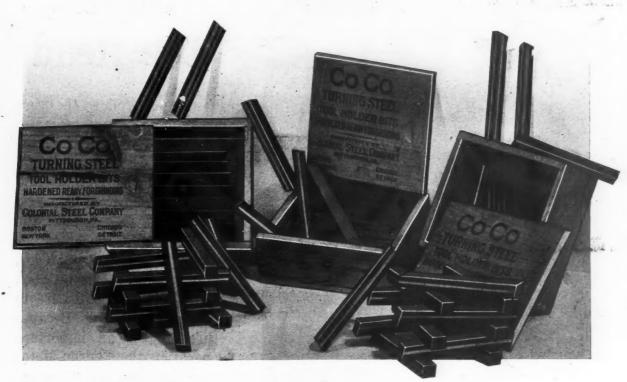
AMERICAN SWISS FILE & TOOL COMPANY

24 IOHN STREET

NEW YORK, U.S.A.



"THE BIT WITH THE GROOVE"



#### What "CoCo" Is Doing On Other Jobs

"CoCo" will do the same in your shop-will cut faster or longer than other steels. Here are some proofs:

"CoCo" is cutting Semi-steel Castings at 100 ft. per minute, cut ½" deep. 30 hours continuous service between grinds.

"CoCo" is turning Cast Iron Hydrant Caps at 169 ft. per minute, feed 1/8", cut 3/8" and turns 4 hydrants per grind where less than one per grind used to be standard.

"CoCo" is turning .40 Carbon O. H. Forged Rams at 95 ft. per minute, feed 1/4", cut 3/32", turning 3 rams in the same. time it formerly took to do one.

"CoCo" Steel does not do stunts-It does the work. It will do yours as well. Ask us.

#### CAN YOU BEAT IT?

PITTSBURGH

BOSTON

DETROIT

NEW YORK PHILADELPHIA

ST. LOUIS



# BOEHM HEAD

# The "Super-Six" and the Super Die Head

Could you follow the construction of a fine mechanical creation such as the Hudson "Super-Six," you'd find up-to-date methods and the most improved tools and machines throughout the Big machines or plant. small, any device whatever, only the best can be good enough if standards are to be maintained. Because threading is an important operation, the Hudson Motor Car Co. uses the "Boehm" Die Head for that work. The photograph shows a 34" Die Head threading nickel steel studs (1/2"—20 pitch—1" of threads) and giving perfect satisfaction from the standpoints of both the "big boss" and the operator. On this work a set of "Boehm"

chasers averages 21,000 studs, pretty good evidence of the efficiency "Boehm" tools develop on this operation.

The "Boehm" is the only Die Head carrying a universal taper attachment cam, and it possesses the added advantage of having the triangular cam on the side of the head adjustable for any desired taper or length of thread. There are other points of superiority you should know about if you're interested in better threading and lower costs. Let us send complete description.

RICKERT-SHAFER COMPANY

612 West 12th Street

ERIE, PA., U. S. A.



# Do You Know About Nichrome

Nichrome is a nickel-iron-Chromium alloy that may be cast up to 1200 pounds. It has the properties of being hard and strong while hot, and resistance to the action of many acids. It is easily machined.

There are a thousand and one uses for Nichrome in connection with apparatus for heat-treating operations; case-hardening boxes, dipping baskets and other apparatus that require strength while hot. Particularly is Nichrome valuable for apparatus that must be alternately heated and cooled. It can be heated and cooled repeatedly without appreciable scaling.

# Get this Sample of Nichrome



We would like to demonstrate the qualities of Nichrome to you—and have prepared a little sample which we will send for examination. It may suggest some uses in your own plant, and at any rate, we would be glad to give you all the information you desire.

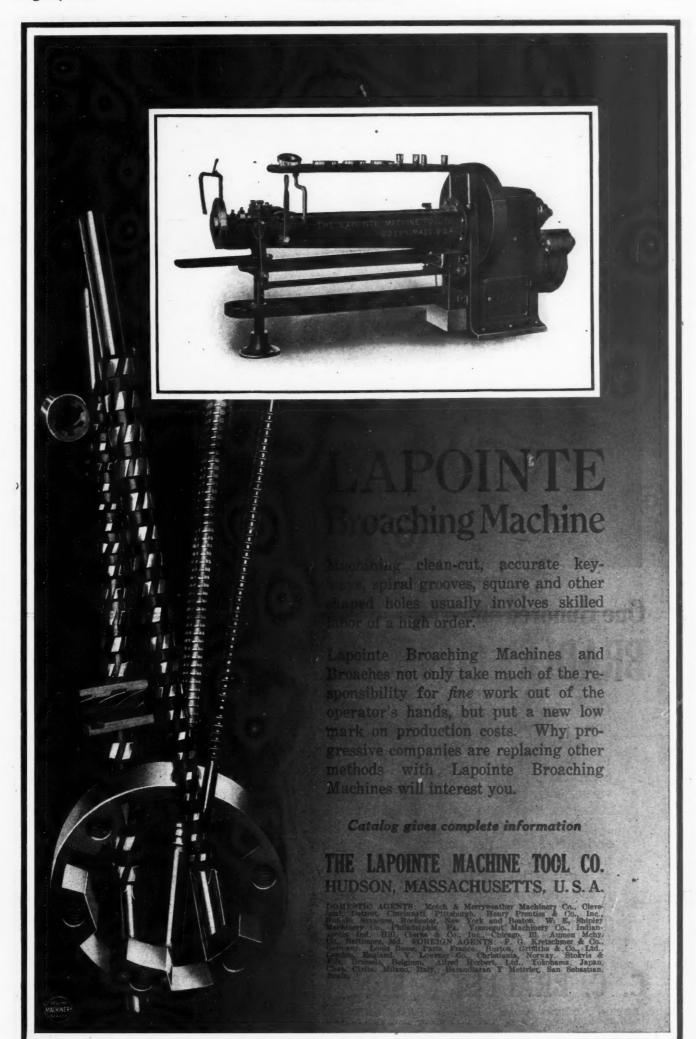
Write Us

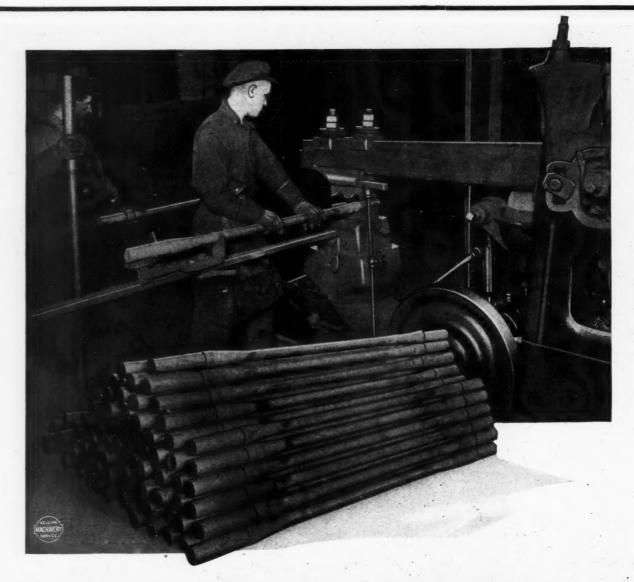
Manufactured under Henderson Patent Number 1,190,652

DRIVER-HARRIS COMPANY

CHICAGO 28 So. JEFFERSON ST HARRISON, N. J.

MANCHESTER





# One Hundred and Thirty of These Forgings Per Day on a BRADLEY CUSHIONED HELVE HAMMER

Could any doubter of Bradley superiority take a walk through the shop of one of the largest car building concerns in the country and watch the eighteen 80-pound Bradley Helve Hammers busy at work there, he'd have to change his mind. A typical job at this plant is forging bridge beam compression members. These members are first upset on a forging machine, then the hammer reduces the diameter of each end from  $2\frac{1}{2}$ " to 2". A helper heats one end of the rod and the blacksmith does the reducing with the aid of the simple holding "rig" noted in the photograph. 260 ends are forged per day of ten hours, or 130 complete members. For over nine years Bradley speed, control, power and economy have been a source of satisfaction to this concern—and there are many others who consider it the finest machine on the market for its purpose.

The Bradley line of hammers includes Horizontal and Upright type and the Bradley "Compact." Catalogue gives full particulars—send for it.

## C. C. BRADLEY & SON, Inc., SYRACUSE, N. Y.

FOREIGN AGENTS: France, Belgium, Switzerland, Spain and Portugal; Fenwick Freres & Co., 8 Rue de Rocroy, Paris. Italy, Taddeo Giusti, Modena, Italy. England, Buck & Hickman, Ltd., London.

## **MONARCH LATHES**

Give complete SATIS-FACTION in rapid manufacturing of duplicate parts for BUTTER-FIELD & COMPANY, Tap and Die Makers at Derby Line, Vt.

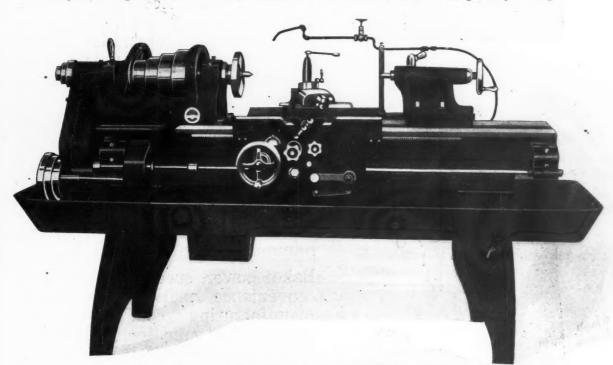
They have eight Monarch Lathes in use similar to illustration below, and they write:

"We are entirely satisfied with these eight Monarch Lathes. They are doing good work and they are satisfactory in every respect."



View showing 8 Monarch Lathes in the manufacturing department of Butterfield & Company, Tap. and Die Makers, Derby Line, Vt.

Monarch Lathes are giving universal satisfaction in hundreds of such plants. Whether for manufacturing of duplicate parts or for fine tool work, there is a Monarch Lathe that we guarantee to give you satisfaction and to save you money. The prices of Monarch Lathes are reasonable. The quality is right.



14 in. x 6 ft. Monarch plain turning lathe as used by BUTTERFIELD & COMPANY for duplicate manufacturing. Equipped with pan, pump and piping, automatic length stops, taper attachment and compound rise and fall rests.

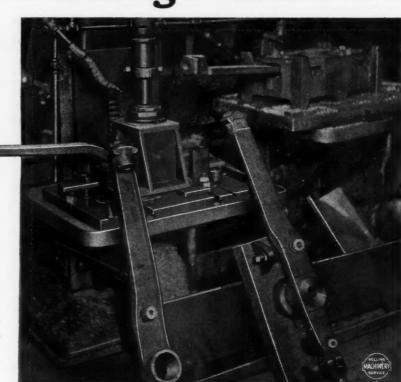
Monarch Lathes are built in all styles in 14-, 16-, 18-, 20-inch swings.

THE MONARCH MACHINE TOOL CO. SIDNEY, OHIO, U. S. A.

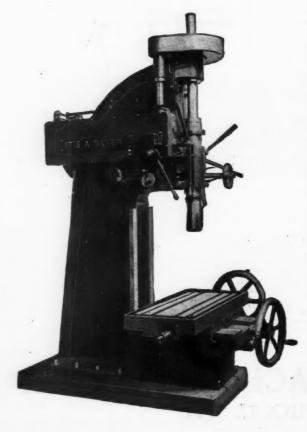
# **BAKER Drilling Machines**

For Making Automobile Parts

We are showing a "close up" of two Baker Drilling Machines that have been doing hard, heavy drilling in steel for years in a New England automobile plant.



IT'S A BAKER



The work is cast steel distance rods. They are first rough drilled, then finish drilled, hollow milled on one side, turned, and hollow milled on the other. Nothing startling in these operations, to be sure; but they throw an interesting light on what machines used for automobile building have to stand up to as a steady job. There is a row of Baker Drilling Machines at this plant—practical, productive, dependable machines that lower costs to the minimum on the work they do.

Baker power, speed, accuracy and convenience make a profitable manufacturing combination no matter what your line. The Baker limit is the limit of what your tools can stand.

Let us work out your boring problem.

BAKER BROTHERS TOLEDO, OHIO, U.S.A.



THE Master Lathe is a high-grade, geared head tool in a  $12\frac{1}{2}$ " swing; of solid construction, rigid throughout, and of an efficient design.

First class in every respect. Is built from the finest materials and under conditions ideal for producing a fine machine. Absolutely guaranteed as to accuracy of performance and perfection in workmanship and material.

The Master Lathe possesses many time-saving features—in addi-

tion to the recognized advantage of the geared head which transmits power to the cutting tool without belt slippage, etc.

Length of bed  $4' 8\frac{1}{2}''$ ; distance between centers, 2' 6''; speeds of head spindle (6) 28, 46, 85, 135, 225, 418.

Just now, shipment of a few Master Lathes with pulley drive can be made within ten days from the receipt of order. With motor drive attachment, within thirty days from receipt of order.

Send for particulars today

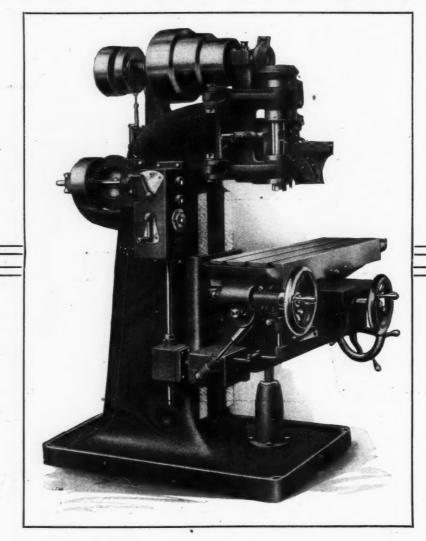
THE MASTER MACHINE TOOL COMPANY

110-112 WEST 40th STREET

**NEW YORK CITY** 

# **Duplex Typeless Die Sinking Machine**

Cuts Labor and Time in Making Drop Forge Dies



This shows "Duplex" No. 6—A vertical Milling Machine with additional head for cutting semi-circular impressions in drop-forge dies.

The "Duplex" will save you more money than any other machine in your Die Department.

With the "Duplex," Dies for cranks, camshafts, knuckle joints, etc., can be machined in one setting, in one-half to one-tenth the time required by typing and without the cost of types.

For prompt delivery write for Circular and Price.

#### JACKSON MACHINE TOOL COMPANY

Cable "Die Sinker Jackson"

JACKSON, MICHIGAN, U.S.A.

# WALCOTTS

## Lathes of Superior Endurance

Walcott Lathes are particularly productive in plants where machine tools are driven continually to the last notch of capacity, and on special demands even to carry an overload. To enable them to stand the pace, they are designed along lines heavier than generally followed.

Bearings and wearing surfaces are as large as practicable, much larger than usually found on lathes of corresponding sizes. Parts subject to greatest strain are reinforced, new features have been introduced and standards of design perfected. Every Walcott represents the results of 35 years of lathe building and is a wonder for high production in continuous heavy service.

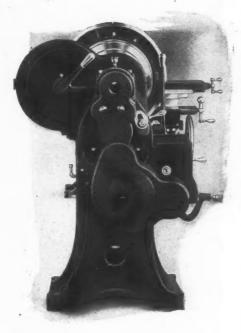
Walcotts are made in sizes from 14" to 28". Send for circulars.

### Walcott Lathe Company

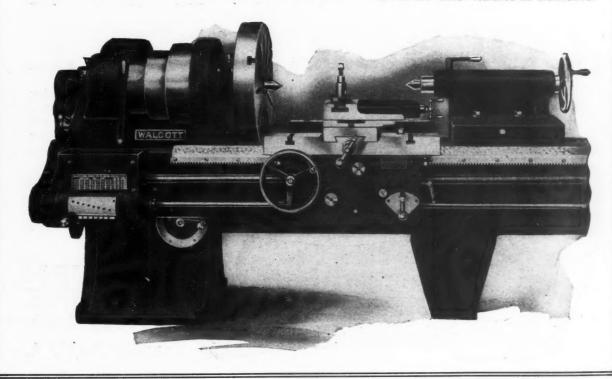
Established 188

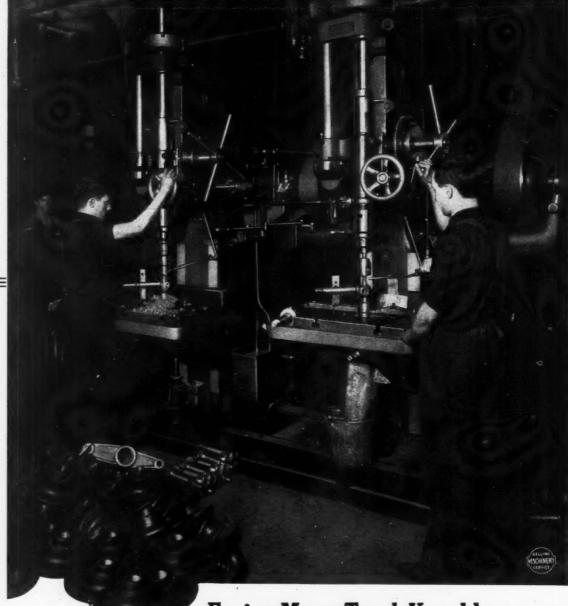
414-420 Jackson St.

Jackson, Michigan



This 28" machine is typical of the line. Bed is extremely heavy; there is a large front way on the bed, a double plate apron with drop forged gears, rigid compound rest, heavy back gear arm reinforced by single-piece gear guard and headstock. Gears are enclosed, feed gears run in oil. Other features as distinctive.





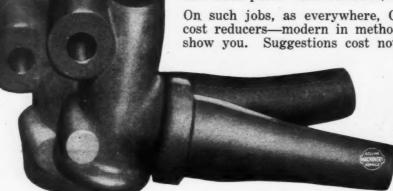
## Facing Motor Truck Knuckles—on a

The success of Colburn Heavy Duty Drilling Machines is due not alone to their wonderful power and rigidity, though you will see them handling the heaviest work everywhere; but to their convenience and accuracy and speed on lighter kinds of work. This is demon-

strated in the work at the Timken-Detroit Axle Company, where Colburn Machines finish a wide range of automobile and truck parts—axle knuckles, axles, etc.

On such jobs, as everywhere, Colburn Machines are real cost reducers—modern in methods and economies. Let us show you. Suggestions cost nothing. Tell us what your problems are and we'll

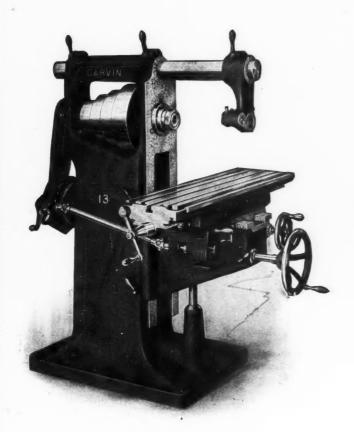
do the rest.



Franklin, Pa., U.S A.

# GARVIN MILLING MACHINES

Made to Stand Long and Hard Usage



GARVIN No. 13 Plain Milling Machine
Use Code Accession

Known for their Rigidity, Simplicity, Efficiency and Maximum of Output. In the manufacture of these machines the best materials are used, hardened and ground where necessary.

Equipped with our

## SQUARE LOCKED SOLID TOP EXTENDED KNEE

doing away with all possibility of weakness or chattering.

Rigid and powerful under the most exacting cuts.

There are other exclusive GARVIN Features.

#### Adjustments of No. 13 Plain Miller

Table F	eed				6				24	in.
In and (	Out	Ad	just	me	nt				7	in.
Vertical	Ad	just	tme	nt			۰	۰	19	in.
Weight	0							17	25	lbs.

Ask a GARVIN User

FOR FURTHER INFORMATION ASK YOUR DEALER OR WRITE US DIRECT

MANUFACTURED BY

## THE GARVIN MACHINE CO.

Spring and Varick Streets

50 Years in NEW YORK CITY

VISITORS WELCOME



# You Can Get Small Single Motors from Stock

Remember this when you plan motor drives for small shops. Arrange the layout for individual drives—\frac{1}{4}, \frac{1}{2}, \frac{3}{4} \text{ H.P.—and get a stock shipment of} \frac{\single \text{Single Phase}}{\text{Phase}} \text{Motors}

Don't wait for the lineshafts, pulleys, etc., necessary for a group drive. Just pick up one of these little RI Motors, install it on the floor beside the machine and have the outfit running—all in the same day.

These fractional RI Motors have all the good mechanical and electrical characteristics of their bigger brothers (the line runs up to 20 H.P.).

The direction of rotation of RI Motors can be easily changed by loosening a screw and moving the brush rigging—or if reversible service is wanted a four pole switch is all that is required.

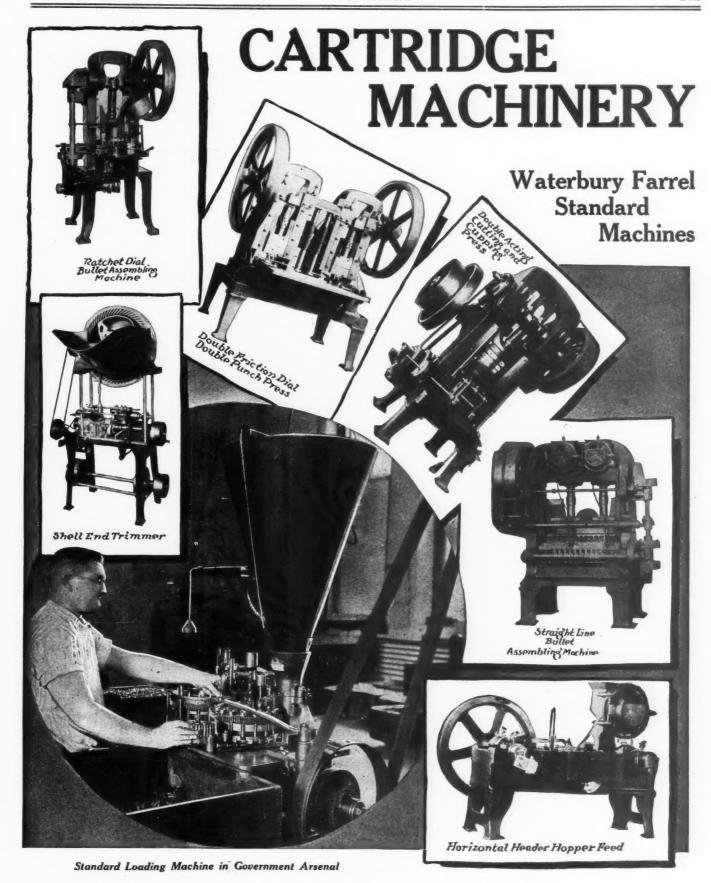
Ask our nearest office about stock shipments on the RI Motors in the 1/4, 1/2 and 3/4 H.P. 1800 R.P.M. sizes.

## General Electric Company

General Office: Schenectady, N. Y.



Sales offices in all large cities



The Waterbury Farrel Foundry & Machine Co., of Waterbury, Conn., U. S. A., has appointed me to be the sole manufacturer for export of their entire line of Cartridge and Shot Shell-Making Machinery. Proposals and Estimates covering complete plants or separate units required for export will be furnished on request.

FREDERICK S. BLACKALL NEW YORK, U. S. A.



Combination Grinder with exten-sion removed and Angle Plate fitted for external work



Combination Internal and External Grinder. Two sizes,  $\frac{1}{4}$  and  $\frac{1}{2}$  H.P.



Hand Drill. Eight styles and speeds

# ISEY

**Electric Machine Tools** 



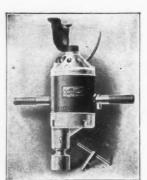
Ball Bearing Floor Grinder. Five sizes, ½ to 5 H.P.

Most Complete Line of Hand and Breast Drills, Radial Drills, Sensitive Bench Drills, Portable Hand Grinders, Buffers, Bench and Pedestal Grinders, Beveling and Glass Blocking Machines.

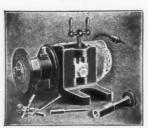
Complete catalog No. 12 on request.



Tool Post Grinder. Ten styles



Hand and Breast Drill. Twelve styles and sizes, ½- to ½-inch capacity

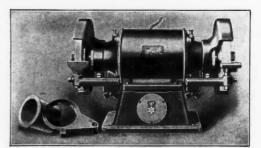


Heavy Duty Drill. Seven sizes, ½- to 2½-inch capacity

## The Hisey-Wolf Machine Co.

CINCINNATI, OHIO, U.S.A.

> New York Office: 50 Church Street



Ball Bearing Bench Grinder. Four sizes, ½ to 3 H.P.



## "Just the Ticket" for a Bolt-Threading Machine

This is the word of the operator who runs this double-spindle Acme Bolt Threading Machine in one of the best equipped street-railway shops in the Middle West.

To keep his daily output at top notch it is necessary to have a dependable drive giving plenty of power at the right speed for all sizes of bolts. This 5 H.P. Type AS Reliance Adjustable Speed Motor gives just the results he wants.

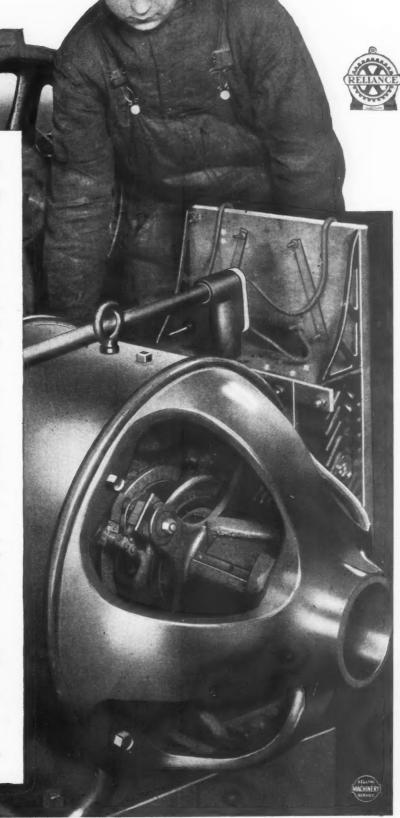
Type AS Motors run at any speed and develop full power over ranges as great as 1 to 10. They make machine tools turn out more work.

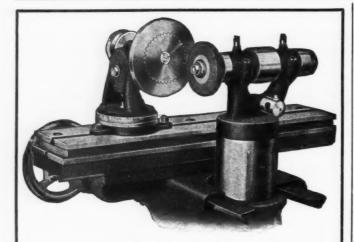
Get Our Folder 10M for Details

# Reliance Electric & Engineering Co.

1056 IVANHOE ROAD CLEVELAND, OHIO

Branches: New York, Philadelphia, Pittsburgh, Toledo, Chicago







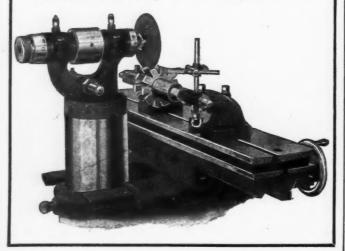
## Universal Grinder

We know of no tool room or general grinding job-surface, cylindrical, internal—within the capacity of a ma-chine of this size that the Greenfield Grinder cannot handle easily and efficiently. We have made the "Greenfield" a rigid, accurate, smooth running machine, and supply as regular equipment attachments which make it a truly universal grinder. Changes from one job to another are quickly made; controlling wheels are directly in front of operator no matter what the set-up. The Greenfield Grinder is conceded by experienced operators to be one of the most practical and economical allaround grinders on the market.

Write for the catalog.

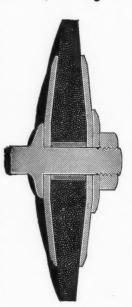
#### THE GREENFIELD MACHINE COMPANY

GREENFIELD, MASS., U. S. A.



## Safety First and Always

There can be no grinding wheel accidents in the shop equipped with Safety Grinding Wheels and Safety Collars. These wheels are tested at the factory at speeds 50 per cent higher than actual practice demands, and they're held in the collars with such a bulldog grip that pieces couldn't possibly fly, even though the unusual happened, and a wheel did They are perbreak. fectly safe at maximum speed. You owe it to your workmen to make your shop safe; you owe it to yourself as a sound business investment.



Full Line of Wheels, Grinding Machines and Grinding Room Equipment in Catalog.

## THE SAFETY EMERY WHEEL COMPANY

SPRINGFIELD, OHIO, U.S. A.

FOREIGN REPRESENTATIVES: Farmer & Co., London. Adler & Eisenschitz, Milan. Allied Machinery Co. of America, Paris.

#### Perfection Cylinder Grinder Strong, Durable, Convenient

Designed for automobile cylinder grinding on hollow spindle lathes swinging 14" or over. Has centering device, micrometer adjustment is cessive set. ment, is easily set up and detached. Two models.



Write for Details

WOOD & SAFFORD MACHINE WORKS

#### REAL GRINDING ECONOMY



Ine Bridgeport Combination

Wet and Dry Grinder—

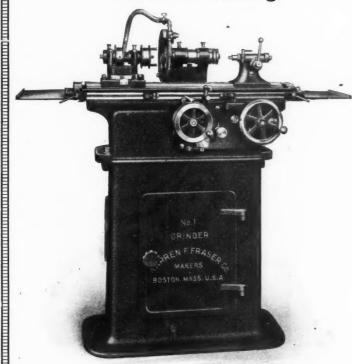
a complete Wet Tool
Grinder at one end—
a Dry Grinder at the
other—does the work
of two machines—
costs little more than
one. 3 sizes—belt or motor
driven. See our exhibit at
Foundrymen's Convention,
Boston, September 25th to
28th, 1917, Booth No. 273,
Section C.

The Design of the service of the section of the service of the ser

The Bridgeport Safety Emery Wheel Co., Inc. Bridgeport, Conn., U. S. A.

## FRASER UNIVERSAL GRINDER

The Logical Machine for Varied Grinding



No other similar machine offers greater speed and all-round convenience in changing from one set-up to another than the "Fraser." It's only a matter of a few minutes, after finishing an internal grinding operation, for instance, to make ready for either cylindrical or surface work.

For internal grinding, capacity is 8" outside diameter, for cylindrical grinding 8" diameter by 20" length, for surface grinding work up to 6" in width and 20" long.

Some of the more striking features of design are: Variable table movement as low as  $\frac{5}{8}$ " large bearings, double end wheel taking spindle for wheels up to  $\frac{1}{2}$ " face and 8" diameter, box type base, three point suspension for upper part of machine, unit construction of apron permitting feed mechanism to be removed as a unit, two wheel speeds, four table speeds, five work rotation speeds. Let us tell you all about the possibilities of the "Fraser" for fine grinding on tools, gauges, jigs and fixtures as well as for production work within its range.

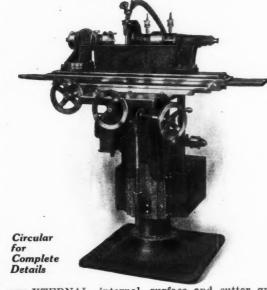
Detailed description on request.

THE WARREN F. FRASER CO.

Freeport Street

BOSTON, MASS.

#### The Connecticut Universal Grinder



EXTERNAL, internal, surface and cutter grinding can be handled on this machine with remarkable ease and adaptability. The unique column construction allows the table to swing in a complete circle, and with the head fastened to the column, any position is available without twisting the belt. The Universal Headstock is fitted with draw-back attachment to receive special collets for grinding small cylinders—a valuable feature for tool room work.

Middlesex Machine Works CONN., U. S. A.



## This Substitute is Better than the Original

DIAMO CARBO Emery Wheel Dressers wear longer and give more uniform service than diamond point dressers. We'll send you one on trial, to prove it, if you are willing to be convinced. Diamo-Carbo is much less expensive than diamond points—so much so that each wheel can have its own dresser.

The quality is uniform, which can not be said of diamond point dressers, since the shortage of diamonds puts many inferior stones on the market. Send trial order today.



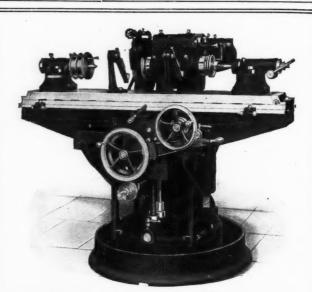
Number 3, 10 inches long.....\$3.50 Number 5, 12 inches long......\$4.00 DESMOND-STEPHAN MFG. CO. URBANA, OHIO, U.S.A.

Alfred Herbert, I.td., Agents for Great Britain. The Canadian Desmond-Stephan Mfg. Co., I.td., Hamilton, Ont., Distributors for Canada.





STAR CORUNDUM WHEEL CO. DETROIT **MICHIGAN** 



## A Whole Grinding Department

The Thompson Universal Grinder combines in a single machine means for handling every possible grinding operation within ordinary range. The head is fixed, work table being adjustable to any position to the wheel, rendering possible plain grinding, surface, edge, die, cutter and internal grinding. It's truly a universal machine with a full measure of strength, accuracy and convenience incorporated to insure high working efficiency.

Write for full particulars.

The Thompson Grinder Company SPRINGFIELD OHIO, U. S. A.

Schmidt's Internal Grinders Equip NOW



Here is a grinder that sells at a popular price and does the work of rachines costing three times as much. Designed to grind worn automocylinders and do other internal grinding. There is a handsome profit in cylinder grind-

Write for Particulars.

B. L. SCHMIDT CO. Davenport, Iowa, U.S.A.

PATENTED



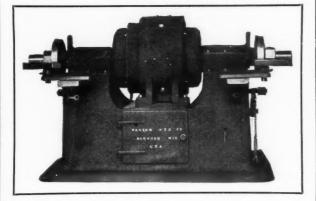
#### A Tryout—A Big Reorder

Invariably a trial (sometimes a skeptical one) of this improved dresser means a big reorder. The largest shops in the country recognize the superiority of the "Brandenburg" Emery Wheel Dresser, and are adopting it because the "Brandenburg" measures up to their rigid requirements.

#### THE "BRANDENBURG"

is a cost cutting, efficient dresser, in which the cutters are automatically lubricated by flake graphite fed from the hollow handle. Greatly saves the cutters and eliminates the cost of lubrication. Standard cutters are used. Let us help you cut costs.

THE HETHERINGTON-McCABE CO. PIQUA, OHIO, U.S.A.



Above cut shows our No. 48 Motor Driven Grinding Machine. It is built to do the heaviest kind of grinding and especially in steel foundries.

Size of wheels  $24 \times 4^{\circ}$  Weight about 4000 lbs. Size of journals  $15 \times 3^{1}/4^{\circ}$  H. P. of motor 10

As shown above, it is equipped with Ransom Patent Speed Controller and without guards. Different types of guards can be furnished.

If interested, send for our Catalogue.

## Ransom Manufacturing Co. OSHKOSH, WISCONSIN, U. S. A.

#### Tell Us What You Grind

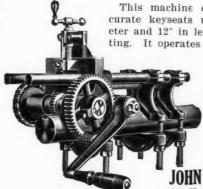


and we will tell you the wheel to use. Unless you get the wheel made for the particular grinding you do, results cannot be the

you do, results cannot be the best—therefore Sterling Service goes with Sterling Wheels. Catalog.

The Sterling
Grinding Wheel Co.
TIFFIN, OHIO
Seiling Agency: New York, 75 Barclay St.
Chicage Store: 30 N. Clinton St.

#### Burr No. 1 Portable Shaft Keyseater



This machine cuts absolutely accurate keyseats up to 5" in diameter and 12" in length without resetting. It operates without chatter or

jar, is very fast, easy to set up and remove, and can be used in practically any position. Has automatic feed and adjustable depth gauge.

JOHN T. BURR & SON 429 Kent Ave., Brooklyn, N. Y.



## SIMMONS UNIVERSAL TOOL AND CUTTER GRINDER

You know the advantages of sharp tools; but do you know the merits of the Simmons Tool and Cutter Grinder? It not merely keeps tools sharp, but puts an accurate edge on them. In addition to grinding cutters, reamers, counterbores, twist drills, etc., it is adapted for cylindrical and internal grinding. The efficiency of the Simmons "Universal" includes prompt delivery service.

Write for description.

SIMMONS MACHINE COMPANY, Inc.

987 Broadway ALBANY, N. Y.

and spindle

and correct

1001 Singer Bldg. NEW YORK CITY

#### THE MINSTER HI-DUTY DRILL

This new machine has a wide range of feeds and speeds, covers a broad field of drilling and is designed to meet requirements of modern work. The massive column and heavy table give ample rigidity for heavy duty; a special spindle construction provides for small high speed drilling as well as heavy work; flood lubrication of all gears, ball thrust bearings on pulley

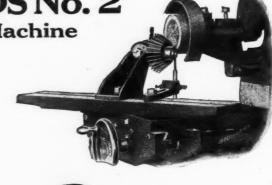
balance insure smooth running. Driving pulley speed 550 R. P. M. Drills in solid steel up to  $2\frac{1}{2}$ ".

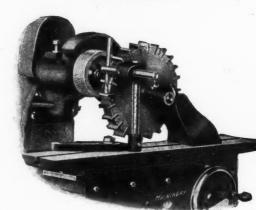
THE MINSTER MACHINE CO. MINSTER! OHIO, U. S. A.



A Really Universal Grinding Machine







Not a toy—Not a makeshift—Not "The best possible for so low a price"—But THE BEST MACHINE FOR YOUR TOOL ROOM IRRESPECTIVE OF PRICE—And yet the price is low.

Fully illustrated circular free on request-Don't fail to ask for yours.

GRAND RAPIDS GRINDING MACHINE CO. GRAND RAPIDS, MICHIGAN, U. S. A.

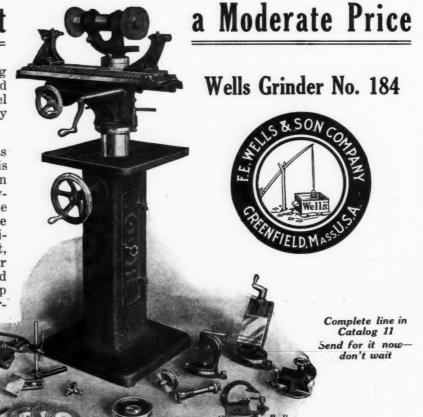
## A Modern Grinder at

You can grind almost anything with the Wells No. 184 Cutter and Reamer Grinder, and the Swivel Table permits grinding at any angle.

Cup wheels can be used as easily as any other as the swivel table is fitted with vertical adjustment—an advantage which no other low-priced tool grinder possesses. The table revolves entirely around the head, the slides have both horizontal and transverse movement, and the top slide swivels for taper work. All slides are hand scraped and fitted with gibs for taking up the wear. Suindle is ground, thor-

oughly protected by dust caps and has spring take-up for end thrust.

A rapid and dependable machine for general shop use.



F. E. WELLS & SON COMPANY, Greenfield, Mass., U.S.A.



## A Pull to Start— A Push to Stop

Simplicity is a dominant characteristic of the Reid No. 2 Surface Grinder and its influence is direct in promoting ease and convenience of operation. A pull on a rod operating from the center of the longitudinal feed wheel starts the machine, a push stops it. Table travel is automatic in either direction and can be reversed by dogs at the front side of the table that trip the reversing lever. Feed, which is positive, may be set to operate at end of each stroke or at the end of a complete forward and return stroke, and may be varied from 0.007" to 0.084". The machine is designed for production grinding as well as toolroom operation and will handle work up to 18" length, 6" width and 12" height. Wheel spindle takes wheels up to 7" diameter, 1/2" face and 3/4"

Boston Scale & Machine Co.
381-389 Congress Street BOSTON, MASS.

## Piston Rings for Hudson Cars

Piston ring production has reached such unprecedented figures that manufacturers of such parts have eagerly accepted a machine which will increase the output, remove stock quickly and hold to a limit of .0005", with a perfect finish.

## **Persons-Arter Grinders**

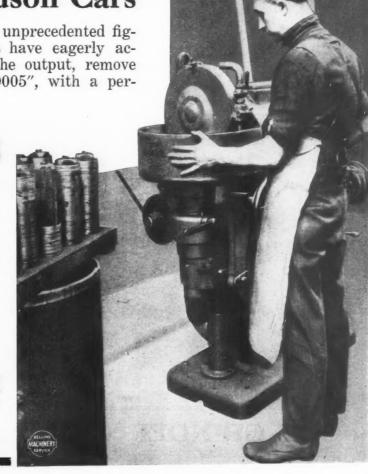
are the machines which get the preference in so many shops because of their exceptional speed, accuracy, convenience and economy. You undoubtedly have work that could be handled to better advantage on Persons-Arter Grinders. Tell us what you grind—will be glad to point out the improvement these machines will insure.

Send for catalog, too.

## THE PERSONS-ARTER MACHINE COMPANY

WORCESTER

MASS.

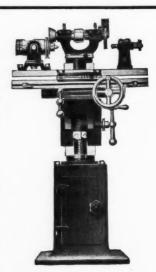


## "Sterling" Grinders

"Sterling" Grinders are well-designed, carefully built machines that can be depended upon for close accuracy and speedy production on any work within their range. They are *simple* machines—highly skilled operators are not necessary to secure best results.

#### Universal Tool and Reamer Grinder

Completely universal in all movements. The table revolves entirely around the head, permitting the use of the wheel at any desired angle. Gibbed slides take the travel of the knee, which revolves around a center column, and which can be locked securely in position before moving the knee. This feature is very important on work requiring close accuracy. It will pay to look into some of the possibilities of this little machine.



# Ask for details.

#### Plain, Universal or Crankshaft Grinder

A heavy machine for manufacturing purposes; hand or power feed table; takes work up to 50 inches between centers; three point suspension is a feature, by means of which weight is carried at the same points and strains always come through the same channels; many other advantages. Prompt deliveries.

#### McDONOUGH MFG. CO. Machine Tool Department EAU CLAIRE, WIS.

YOUNG, CORLEY & DOLAN, Incorporated NEW YORK CITY

L. R. MEISENHELTER MACHINERY CO., Philadelphia, Pa.

## Ott Universal Grinding Machine



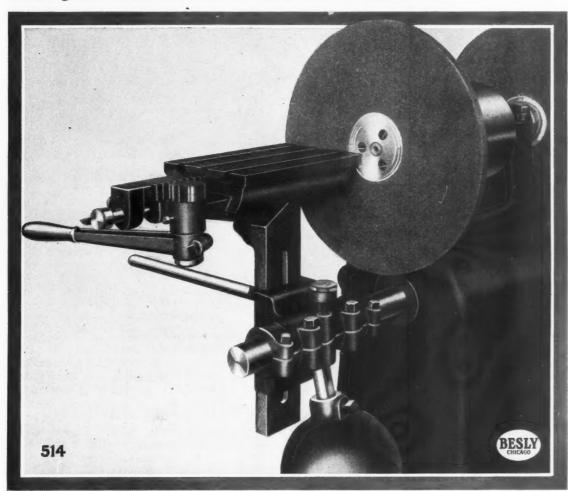
This machine supplies the need for a fast, accurate, economical grinder for universal application. Wheel arrangements for face, surface and internal grinding are ideal, the machine is exceptionally easy to con-trol, and is strongly and rigidly constructed throughout to give a long life of continuous service. For work within a range of 9" x 26" it's the superior of many larger, higher priced machines.

Full details should interest you. Write.

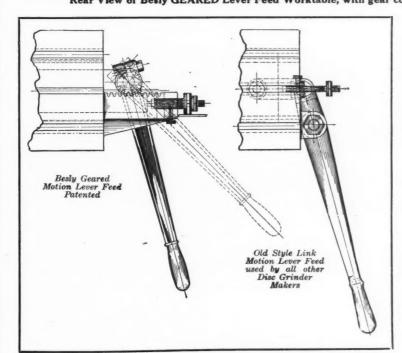
OTT GRINDER CO., Main Office Indianapolis, Ind.

# The BESLY GRINDER will do MORE WORK with LESS FATIGUE than any other disc grinder on the market

WHY? Because the Besly GEARED Lever Feed Worktable (Patented) gives three to five times greater leverage, making the work that much easier for the operator.



Rear View of Besly GEARED Lever Feed Worktable, with gear cover removed to show construction



Avoid the old style link motion lever feed with long, unhandy fixed lever and small ratio of leverage offered by imitators.

Insist on the Besly GEARED motion lever feed with short, handy, adjustable lever and large ratio of leverage.

Besly construction gives

MAXIMUM LEVERAGE MINIMUM FATIGUE

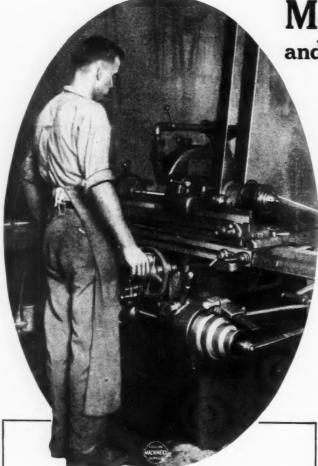
CHARLES H. BESLY & CO.

120-B North Clinton Street



CHICAGO U. S. A.

(Originators of Disc Grinders)



The Norton Limit is the Grinding Limit

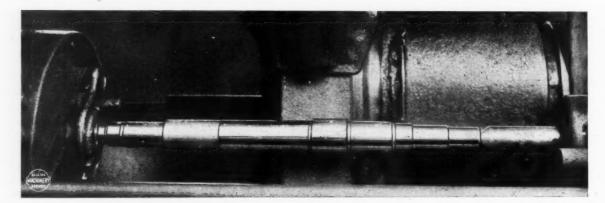
Mostly Figures and Worth Looking Over

We are indebted to the Robbins & Myers Company, Springfield, Ohio, for facts, figures and photographs of some remarkably good grinding operations. The work is point 30 Corona Steel armature shafts 12.899" long with nine diameters to turn as follows:

1st Diameter: 0.6875'' + 0.0005'' - 0.000''length 0.968'' + 0.005'' - 0.005''2nd Diameter: 0.798" + 0.002" - 0.000" length 1.157" + 0.005" - 0.005" 3rd Diameter: 0.875" length 0.625" + 0.001" - 0.000" + 0.005" - 0.005" 0.000" + 0.000" - 0.0005" + 0.005" - 0.005" 4th Diameter: 1.001" length 1.391" + 0.005" 5th Diameter: 1.125" 0.005" length 1.094" + 0.005" -6th Diameter: 1.001" length 4.703" + 0.000" -- 0.0005 + 0.005" -- 0.005" - 0.0005" 7th Diameter: 0.8135" + 0.000" - 0.0005"length 1.312" + 0.005" - 0.005"8th Diameter: 0.7876" + 0.001" - 0.000" length 0.531" + 0.005" - 0.005" 9th Diameter: 0.6595" + 0.0005" - 0.000" length 1.118" + 0.005" - 0.005"

The operator grinds 50 to 60 shafts on one diameter, then dresses the wheel and grinds the next diameter until the shaft is completed, dressing the wheel between each diameter. The wheel used is a 14" x 21/4. Norton 24-M. Wheel speed, 5500 feet per minute; work speed 70 feet per minute. Output per 11-hour day, 110 complete shafts.

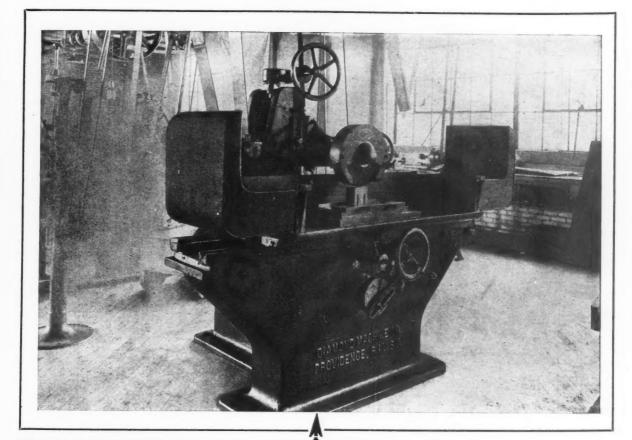
Let us tell you more about Norton Grinding—show what it can do for you.



## NORTON GRINDING COMPANY, Worcester, Mass., U.S.A.

CHICAGO STORE: 11 North Jefferson Street

AGENTS: Vonnegut Machinery Co., Indianapolis, Ind. Robinson, Cary & Sands Co., St. Paul, Minn.; Duluth, Minn. Manning, Maxwell & Moore, Inc., St. Louis, Mo. Henry Prentiss & Co., Inc., New York., N. Y., Boston, Mass., Buffalo, N. Y., Rochester, N. Y., Syracuse, N. Y., Scranton, Pa. The Motch & Merryweather Machinery Co., Cleveland, O., Detroit, Mich., Pittsburgh, Pa., Cincinnati, O. Eccles & Smith Co., San Francisco, Cal., Los Angeles, Cal., Portland, Ore. The Canadian Fairbanks-Morse Co., Montreal, Que, Toronto, Ont., Vancouver, B. C. C. T. Patterson Co., Ltd., New Orleans, La. Kemp Machinery Co., Baltimore, Md. W. E. Shipley Machinery Co., Philadelphia, Pa. Alfred Herbert, Ltd., Coventry, England, Paris, France, Milan, Italy. Post Van der Burg & Co., Rotterdam, Holland. The F. W. Horne Company, Tokio, Japan. Iznosskoff & Company, Petrograd, Moecow and Ekaterinburg, Russia.



### The Diamond Surface Grinder in the National Scale Works

The biggest thing in sight, in this corner of the toolroom at the National Scale Company's shops, is the Diamond Surface Grinder.

It's a big producer—"... a wonderful producer," they call it in a recent letter, and add that it is giving them "excellent satisfaction."

In the National's shop the "Diamond" is used principally for grinding the sides of dies, from the rough, and for re-sharpening—an average of .005 to 1/16" of stock being removed from each surface.

Such work is by no means the extent of the "Diamond" range. It gives excellent service on surfacing anything from cutlery to castings.

DIAMOND SURFACE GRINDERS are easy to operate, accurate, rapid and economical.

Complete Catalogue on Request.

DIAMOND MACHINE COMPANY
PROVIDENCE, PHODE ISLAND

DIAMOND MACHINE CO.



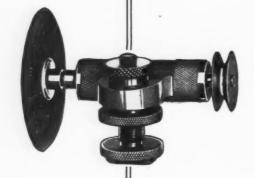




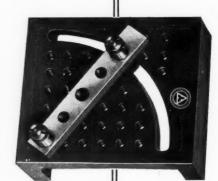




## S.A.S. PRECISION TOOLS



Made by Skilled
Workmen
Who Thoroughly
Appreciate
the Demand for
High Grade Tools



Superior in Materials and Finish Built for Endurance

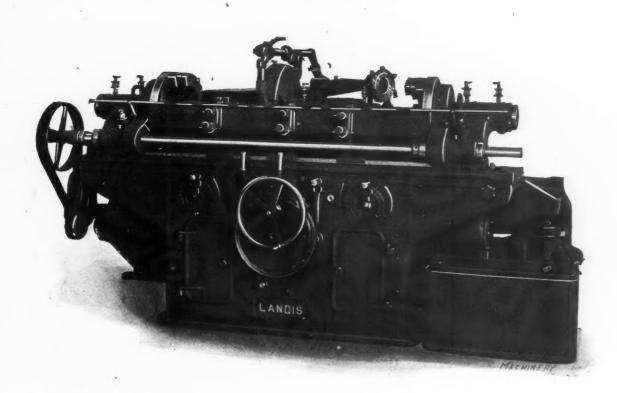
Write for Description and Prices

SLOCUM, AVRAM & SLOCUM LABORATORIES, Inc.

550 West 21st Street

**NEW YORK CITY** 





#### LANDIS

We'd like to send you the catalogue and show you just what to expect from LANDIS Grinding Machines. Send drawings along for figures—we'll be glad to prepare them. Grinding machines for all manufacturing purposes.

## LANDIS TOOL COMPANY

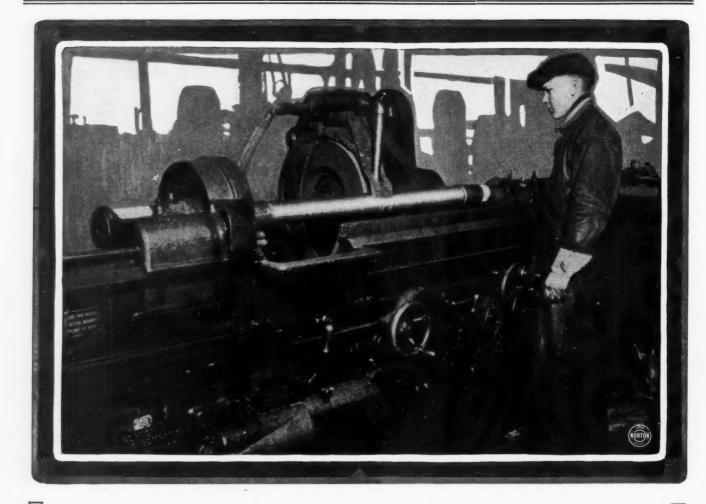
Main Office and Works
WAYNESBORO
PA. U.S.A.

## It's Not Difficult to Secure New Business

Not when you can refer New Business to Old Business—not when the machines in use back up the claims you make for the machine you hope to sell.

And that is why it is easy to sell LANDIS Grinding Machines to men who have work for them to do. LANDIS Grinding Machines, in use all over the world, back up every claim we make for them. They are correct in design—the grinding wheel travels and the work table is stationary—production is large—accuracy is just as close as you may want to make it—finish is unsurpassed.

More weight, less floor space. More work, less wheel expense—and it is all in the design. Ask any LANDIS user.



## Grinding "Big Four" Piston Rods



HIS photograph was taken in a large eastern railway shop and shows a "Big Four" piston rod being ground on a NORTON machine and with a NORTON wheel.

The wheel used is a 24 x 3% x 5", 24 combination, grade M, ALUNDUM, and is giving satisfactory results.

Under slightly different conditions a 24 combination L ALUNDUM has also proven satisfactory.

#### **NORTON COMPANY**

WORCESTER, MASS.

New York Store 151 Chambers St. ELECTRIC FURNACE PLANTS Chippawa, Ont., Can. Niagara Falls, N. Y.

Chicago Store 11 N. Jefferson St.



**Drill Grinder** 

All it has cost the owner of this "New Yankee" for ten years' drill saving service is the price of oil and grinding wheels.

Granted a first-class drilling machine, the chief factor essential to high production is accurately ground drills. "New Yankee" accuracy is positive and uniform. The machine is so simple a wideawake boy can run it.

Over
Ten Years'
Service and
Not a Cent
for Repairs

It does its work so efficiently that from 50 to 75% is saved on drill costs. There's a "New Yankee" to meet every modern drill grinding requirement Write for catalog No. 106.

Wilmarth & Morman Co.

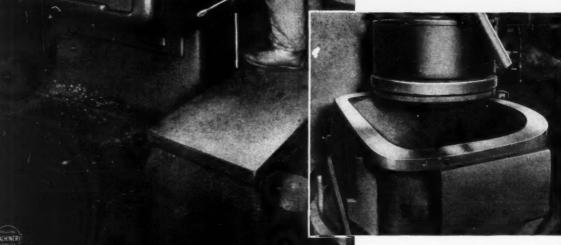
2180 Monroe Ave., N. W. Grand Rapids, Mich.

Manufacturers of Drill Grinders, Surface Grinders, Universal Grinders.

## Five Years' Heavy Work for this

BLANCHARD GRINDER

The Blanchard is a rapid producer. These chilled cast iron mouth pieces for retorts, for example, are faced off on one side at the Leetsdale plant of the Riter-Conley Mfg. Co., Pittsburgh, Pa., at an average of twenty minutes per piece. From each one of these mouth pieces % of an inch of chilled cast iron is removed, enough to square up and clean up the surface.



The all over size of the face is approximately twenty inches by thirty inches, and the flange is one and one-half inches wide.

This Blanchard Grinder has been run by comparatively inexperienced labor since 1912, and has given excellent satisfaction. We can show you thousands of illustrations of Blanchard grinding varying from work as large as this down to the smallest of punchings from thin sheet metal, all handled efficiently and economically as well as accurately.

Let us send more details.

## THE BLANCHARD MACHINE COMPANY 64 STATE STREET CAMBRIDGE, MASS., U. S. A.

DOMESTIC AGENTS: Henry Prentiss & Co., Inc., Motch & Merryweather Machinery Co., Marshall & Huschart Machinery Co., W. E. Shipley Machinery Co., Kemp Machinery Co., Robinson, Cary & Sands Co., Pacific Tool & Supply Co. CANADA: Williams & Wilson, Ltd., A. R. Williams Machinery Co., Ltd. GREAT BRITAIN: Burton, Griffiths & Co., Ltd. FRANCE: Aux Forges de Vulcain.

# What is Y-O-U-R Grinding Problem?



IF you are facing a grinding problem you are facing a need for AMERICAN GRINDING WHEELS.

We can solve that grinding problem for YOU if you will put it up to us.

Our Service Department is waiting for a line from YOU.

**AMERICAN EMERY WHEEL WORKS** 

PROVIDENCE, R. I.



Interest in this job centers about the facts of close accuracy and unusual speed. The operator is grinding an over-all width of 3.4375" on universal joint housings, allowable error, plus or minus, 0.0005". This machine is a Gardner Grinder—built like all Gardner machines, to grind accurately under all conditions. The wheels used are Norton 20-K, 16" x 4" x 10", driven smoothly and evenly in the regular Gardner way, at a speed of 1000 R. P. M. Output is 800 accurately and economically ground housings per 10-hour day.

## 800 Universal Joint Housings in 10 Hours

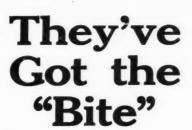
There is no quicker, surer way of securing a smooth, accurate finish than Gardner grinding—a statement we are ready to prove as soon as you give the word. "Procrastination is the thief of time"—and profits. Write us.

# THE GARDNER MACHINE COMPANY

The Largest Manufacturers of Disc Grinders in the World BELOIT WISCONSIN

# "ABRASIVE" GRINDING WHEELS

Mr. Storekeeper in one of the steel casting companies has seen a good many grinding wheels come—and go. Then he saw Abrasive Wheels enter the lists, and not only stay, but crowd every other grinding wheel out. It takes "bite," and plenty of it, to handle his company's grinding efficiently and economically. There's "bite" in every abrasive grain. Moreover, Abrasive Wheels are uniform. When a man asks for a duplicate of the wheel he's been using, he gets that particular wheel's "twin."



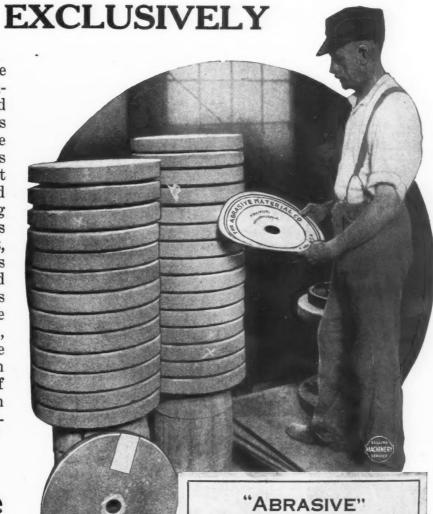
Abrasive Wheels are a sure aid to lower production costs. If your work is material of high tensile strength it calls for "Boro-Carbone" Wheels. For low tensile strength materials we recommend "Electrolon" Wheels. Should you have grinding problems, don't worry about them—send them to us.

New Abrasive Catalog on request.

## ABRASIVE COMPANY

BRIDESBURG PHILADELPHIA, U.S.A.

Chicago Branch, 566 W. Washington Blvd.



GRINDING WHEELS

ABRASIVE ORDER No. B 87180 CUSTOMER ORDER No. 13159

SIZE 18x2x2

GRAIN 14 GRADE Q FACE NO.
SHAPE SAFETY

TESTED AT 1925

SPEED RECOMMENDED

R. P. M. 1925 to 1275

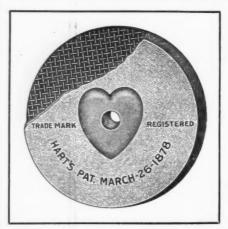
Speed within above range is dependent on condition machine, method of grinding and safety appliances used.

Abrasive Material Co.

BRIDESBURG, PHILADELPHIA, U. S. A. Chicago Branch. 566 W. Randolph St.

Retain tag for duplicate order.

(OVER)



#### Detroit High Grade Grinding Wheels— A Dependable Source of Supply

We furnish reliable wheels for any grinding operation and fill re-orders with *exact duplicates*, at *economical figures*. If you are not grinding with Detroit Wheels just give the line a trial. Catalog.

#### DETROIT GRINDING WHEEL CO.

DETROIT, MICHIGAN, U. S. A.

## The BLOUNT No. 5 Grinder



provides grinding facilities for two men. It's a space and power saver, designed and built to give efficient service. It is rigid, strong and maintains a smooth, even speed. Has self-oiling line reamed babitted bearings, carbon

bitted bearings, carbon steel spindle ground to size, adjustable wheel guards and can be furnished with surface grinding attachment if desired.

> Let us tell you more about Blount Grinders

> 25 Years on the Market

J.G.BLOUNT COMPANY

EVERETT MASS., U. S. A.

#### **EMERY WHEEL DRESSERS**

No. 0 For Small Wheels

No. 2 For Large Wheels



NO. 1 FOR REGULAR SHOP USE

These Dressers in connection with our Cutters make a most powerful and efficient tool, especially our No. 0 for small wheels 6 inches and under, and No. 2 which is made proportionately larger and stronger for large wheels.

#### **CUTTERS**

We make the regular "Huntington" (pattern) for No. 0 and "Huntington" (pattern) Paragon Cutter and Roughing Cutter for Dresser No. 1 and the "Huntington" (pattern) and Roughing Cutters for Dresser No. 2. Let us send you descriptive circular and prices.

GEO. H. CALDER, Lancaster, Pa., U.S. A.

#### LATHE CENTER GRINDER

Will grind lathe centers mechanically with scientific accuracy in fraction of time required with other methods.

Builders of ''Ideal'' Patented Portable Electric Tools, Grinders, Drills, Saws, Screw Drivers, Nut, Bolt and Lag Screw Setters.



# The Reason They're Vitrified

Vitrified Grinding Wheels are vitrified to harden the bond, which hardening gives it almost the cutting quality of the abrasive it binds. In addition the evaporation of moisture, due to the intense heat necessary for vitrification, renders the wheels porous, makes them free cutters and eliminates all possibility of glaz-

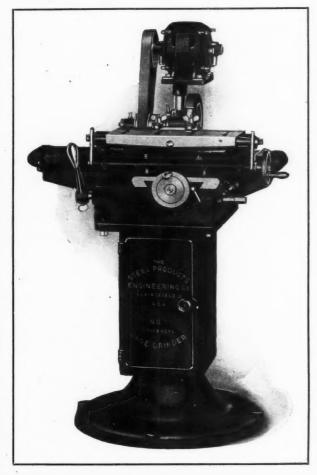


ing or creating sufficient heat to draw temper from the tools.

Vitrified Grinding Wheels are made in all required shapes and sizes. We guarantee satisfaction—replacing any wheel not giving satisfactory service.

Send for Catalog 8

Vitrified Wheel Company Westfield Mass., U. S. A.



# Gauge Grinding

With this machine you get the very highest degree of accuracy with the least possible expense.

Particular attention is called to the flat table and the provisions that have been made for quick, easy adjustments. It is very simple throughout and easy to operate.

Are you familiar with all the details that have helped to make this machine a success?

Let us help you acquire them.

# THE STEEL PRODUCTS ENGINEERING CO.

SPRINGFIELD

OHIO

# Bryant Chucking Grinder Company

Springfield, Vermont, U. S. A. Detroit Office: 924 Dime Bank Bldg., Detroit, Mich.

Builders of One, Two and Three Spindle Chucking Grinders.

### \$75.00 No Better Grinder for the Money



AT this price the "Waterbury"
Toolroom Die and Surface
Grinder is surely a paying investment. It is adapted for a wide
variety of work, is fast and accurate,
fitted with up-to-date conveniences
and means for compensating wear,
strong and rigid throughout, lasting
in service. Better values for the
money would indeed be hard
to find.

Detailed description on request

The Blake & Johnson Co. WATERBURY, CONN.

### Solid Comfort in Grinding

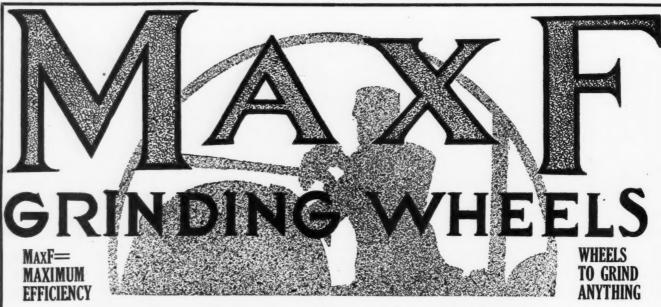


DILLON Electric Grinder

overcomes the usual grinding troubles. The motor is rugged and dustproof. Large shaft of high carbon steel and S K F ball bearings insure perfect balance. Extra heavy wheel guards, broad grinding rests, generous water cup and con-

veniently placed snap switch control make the "Dillon" safe and easy to operate.

THE DILLON ELECTRIC COMPANY OHIO, U. S. A.

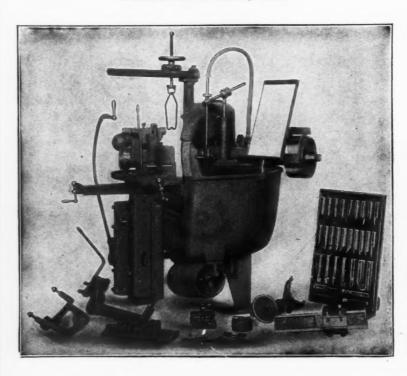


Are You Grinding Down Your Efficiency?

ONE weak tool lowers the efficiency of the whole shop. If grinding is your weak spot write us about it. MAXF Grinding Service not only supplies wheels for every grinding need, but puts the knowledge and experience of its engineers at your disposal to advise you in your selection. This makes us responsible for the result and guarantees your grinding service.

SPRINGFIELD GRINDING CO., Factory and Sales Dept. Chester, Mass.

PHILADELPHIA, PA.



# Mers Hoganory. Labor Saving Machine Tools

Three of the reasons why machine shops find THE SELLERS TOOL GRINDER so profitable that it is regarded as indispensable, are

### Large Output Accurate Work Low Cost of Maintenance

For quickly, correctly and economically forming and grinding cutting tools for Lathes, Planers, Slotters, etc., it is without an equal. It produces and duplicates any desired shapes and angles. Tools treated by it do much more work before regrinding than when sharpened in any other way.

Does not require a mechanic for operator. Saves grinding time. Saves money.

**Shafting - Drill Grinders** 



# FURNACES

for oil, natural gas or manufactured gas

#### CATALOG-?

Catalog 8-M (1917 Edition) shows the latest improvements in heattreating equipment. Do you want a copy?

# Standard Types for Every Need—

THE average furnace order is a rush order—that is, there is urgent need for the furnace well in advance of its installation. In such cases standard furnaces—requiring no special patterns, special machine work or special castings—are the buyer's salvation.

The 75 standard furnaces of the Frankfort family give the buyer the opportunity to buy exactly what he needs and buy it **practically from stock.** Delivery becomes merely a matter of assembling.

For Fast Delivery Consult Our Furnace Department.

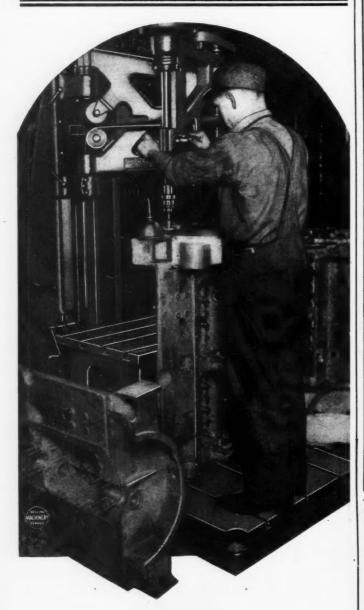
### The Strong, Carlisle & Hammond Co.

Frankfort Avenue

Cleveland, Ohio

Boston New York BRANCHES: — Chicago Philadelphia

Detroit Pittsburgh



# THE HAMMOND RADIAL

### As a Manufacturing Machine

The shop in which this photograph was secured is known as the "little shop with the big production," and the "Hammond" plays no small part in enabling it to merit the distinction. For example, on this crankcase job, eight 5/16" holes are drilled, and eight 3/8"-16 P holes tapped at one setting, operation necessitating bolting flywheel to the case and taking down again when finished. Regardless of this detail, 120 cases—1920 holes—are completed every 9½ hours. "Hammond" service pays here—will pay in your shop, too. Try it.

### THE HAMMOND MFG. CO.

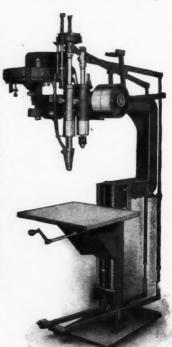
CLEVELAND, OHIO

### Save Time and Avoid Inaccuracy

Many an able man can't set a screw straight by hand, but any intelligent boy can operate the Reynolds Automatic Screw Driving Machine and average two to five times greater output than by hand methods. Every screw sets true.

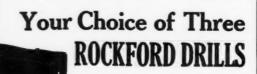
Adapted for wood or metal. Screws may be driven flush or to any desired depth by automatic adjustment.

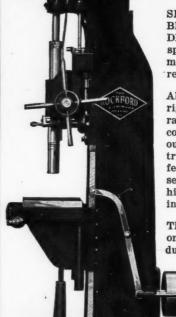
> Catalogue Gives Details—write for Yours Today



Our Record is 18,000 Screws set in 10 hours

REYNOLDS PATTERN & MACHINE CO.
MASSILLON, OHIO





SINGLE PULLEY, DOUBLE PULLEY or DIRECT DRIVE with variable speed motor — whichever meets your special drilling requirements.

All three have the same rigid frame; the same rapid operation and easy control, four instantaneous feed changes and a trip lock for throwing out feed automatically at point set. All of them will drive high-speed drills up to  $2\frac{1}{2}$  inches diameter.

There's work for at least one of these modern, heavy duty drills in your shop.

> Write for Booklet

Rockford Drilling Machine Company ROCKFORD ILLINOIS

## A Whitcomb-Blaisdell Planer



There are other planers in this plant but the Whitcomb-Blaisdell  $36" \times 42" \times 14'$  Planer, with its three heads, individual motor drive, hand-operated dogs, trouble-proof head-raising mechanism and second-belt features is the leader of them all—and we have the company's own word for it.

On work such as illustrated, planing large grinder bases, the roughing cuts are as heavy as one-half inch, through sand, scale and tough iron; but it is impossible to stall the planer. And it takes the finishing cuts to just as close limits as are needed.

When you buy a Whitcomb-Blaisdell Planer you get the maximum in planer service. Let us send the catalogue.

WHITCOMB-BLAISDELL MACHINE TOOL CO. WORCESTER, MASS., U. S. A.



## Dreadnought HIGHSPEEDSTEEL

Makes Durable Inserted Tooth Cutters

Dreadnought tools stand up in a noteworthy way under hard usage. For example, here's a tool 14" diameter with 17 inserts of  $\frac{5}{8}$ " square Dreadnought High Speed Steel, that works like a charm in sandy iron castings. The work is part of a clothes pressing machine, is 13" wide at widest part, and 39" in length. Notwithstanding the edge-dulling nature of the work, this Dreadnought Cutter cleans up a round 200 castings before the inserts have to be re-ground. Dreadnought is the prince of steels for hard service cutters, lathe and planer tools, etc. Economical production depends to a great degree on the wearing and working qualities of your tools.

Unless you know your present tool equipment is the most profitable for your work, give Dreadnought Steel a trial.

## HALCOMB STEEL COMPANY SYRACUSE NEW YORK

Branches: Chicago, Cleveland, Philadelphia, Boston, New York

# Remarkable Ductility of "NATIONAL" Pipe



170 quarts of nitroglycerine failed to crack this piece of "NATIONAL" Casing. The terrific force of the explosion reduced the length from about 18 feet to less than 6; although crushed, twisted and distorted there was no fracture.

### "NATIONAL" Pipe for Mechanical Purposes



This piece of 10-inch "NATIONAL" Casing dropped 236 feet through a 12½-inch hole without fracturing the material. Although the end is distorted, as the thread protector was driven up over the threads by the force of the impact, THE MATERIAL SHOWS NO SIGN OF FRACTURE.

These three illustrations should be convincing proof of the extraordinary ductility of "NATIONAL" Pipe. No mill test ever devised could equal the terrific strains effected by the unusual accidents which produced the results shown.

¶ It is therefore a reasonable deduction that as "NATIONAL" Pipe has withstood such enormous forces without a fracture in the material, it is essentially qualified to withstand the strains incident to the mechanical uses for which it is recommended.

¶ As a matter of fact "NATIONAL" Pipe is used for thousands of parts of different machines which are used for thousands of different purposes.

¶ The inherent ductility of "NATIONAL" Pipe lends itself most satisfactorily to mechanical manipulations, and in service withstands without failure the jars and shocks to which the incessant vibrations of machinery are inevitably subjected.



1440 feet of 8½-inch "NATIONAL" Casing dropped 200 feet in a well, and as a result of the impact on solid stone three sections of the casing were telescoped with NO SIGN OF FRACTURE.



### NATIONAL TUBE COMPANY, General Sales Offices PITTSBURGH, PA.

DISTRICT SALES OFFICES: Atlanta Boston Chicago Denver St. Louis St. Paul Salt Lake City PACIFIC COAST REPRESENTATIVES: U. S. Steel Products Co., New York City.



The Nationally Known First Quality
HIGH SPEED STEEL

PROCLAIMED

By the Men Who Use It

THE BEST FOR ALL MACHINE WORK

VANADIUM-ALLOYS STEEL CO.

Carried in Stock in These Warehouses:
ET WARD'S SONS GEO. NASH CO. FIELD & CO.Inc. YANDIUM-ALLOYS STEEL CO. GEO. NASH CO.
44 Farnsworth St. BOSTON Mass. 304 Hudson St. NEW YORK N.Y. 721 Arch St. PHILADELPHIA. Pa. PITTS BURGH. Pa. & LATROBE Pa. 64 6 Washington Blvd CHICAGO!



The above cut shows the wrench in its two positions

which, for the first time in the construction of this type of wrench, accomplishes reversibility of action -works either way without disengaging and turning.

The Billings

Chain-Pipe Wrench, because of its new and exclusive feature, saves many an hour and solves many an awkward situation. Read the facts:

The important and exclusive feature of this wrench is its double-action or reversibility. Pipe can be turned in either direction without the process of removing and turning over the wrench. This is due to the angular position of the elliptical jaws, which allows the engagement of either the outer or

The combination feature of this wrench consists of its adaptability to pipe fittings and short connections, as well as ordinary pipe. By removing the outside elliptical jaws, thereby bringing into play the narrow jaw attached to the under part of the handle, the wrench is immediately converted into an efficient tool for narrow or irregular work where a broader wrench would be ineffectual.

The elliptical jaws are serrated on all sides and may be easily changed end for end, thus giving double life to the wrench. With the outer jaws removed, the wrench is available for nut and bolt heads, as well as pipe fittings. The handle is so designed as to give the necessary strength with minimum of weight. The handle and jaws are made from steel drop forging of superior quality, the jaws being carefully hardened. All parts are interchangeable.

The above cut shows the wrench as adapted to fitting nipples, etc.

The tool is made with either a flat link or cable chain. The chains are made in our own factory, and are of sufficient safety-test to insure an absolutely reli-able tool.

#### Prompt Deliveries

Descriptive literature and price lists upon request.

### JESSOP'S "ARK"

Has an Unexcelled Record.



### HIGH SPEED STEEL

Note the Following Facts.

In turning 100 railway car wheel tires, Jessop's "Ark" High Speed Steel has the record of losing less steel, due to grinding, than any other make.



The actual amount of steel ground off the tool in turning 100 wheels was 3 ounces. This is an unrivalled performance in steel economy.

We have a large stock of Carbon Tool Steel and High Speed Steel. Write for Catalogue.

JESSOP & SONS, Incorporated 91 JOHN STREET, NEW YORK, N. Y.

Boston Warehouse: 163 High Street

Branch Warehouses throughout the United States

### DRILL VISE

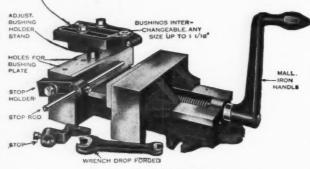


Fig. 1. With Jig Attachments

Always a good vise for meral shop use on driller, iller, shaper or planer, and at the same time holds



Fig. 2. Without Jig Attachments

For use in Drillers from 20-inch to Largest Radial For Twist Drills 0\* to 34\* requiring speeds up to 3000 R. P. M.

No. 3. jaws 6", opens 4½", with attachments, \$22.00; without, \$20.00. List.

No. 5, jaws 12", opens 9½", with attach-ments, \$40.00; without \$36.00. List.

#### DRILL SPEEDER

No. 2, with chuck, drills 0" to 5/16". List, \$25.00.

No. 3, with chuck, drills 0" to ½". List, \$27.50.

No. 3B, with No. 1 Morse hole instead of chuck, \$27.50.

No. 4, with chuck, drills 0" to 34". List, \$40.00.

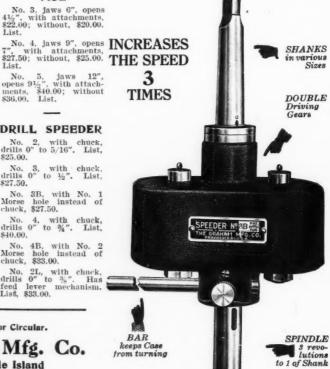
No. 4B, with No. 2 Morse hole instead of chuck, \$33.00.

No. 2L, with chuck, drills 0" to 3/s". Has feed lever mechanism. List, \$33.00.

All Patented. Send for Circular.

The Graham Mfg. Co. Providence, Rhode Island

Great Britain: C. W. Burton, Griffiths & Co. Germany, Austria-Hungary, Scandinavia: A. Kayser, Berlin, S. W. 68. France, Italy, Switzerland, Spain and Holland: Fenwick Freres & Co.



This cut shows Nos. 3B and 4B only. There are two other styles and sizes.

Fig. 3. V-Jaw for Round Work



## Starrett Tools

### Tell the Truth

After all, the principle of micrometers and other fine measuring tools is quite simple. The only requirement is that they tell the truth.

This test indicator, for example, has done its full duty when it has registered its story in thousandths.

Starrett Tools have a reputation for truth telling. Their character is well established. That's why it pays to use the line of 2100 styles and sizes of micrometers, calipers, gages, squares, height and depth gages, and other precision tools described in our Catalog No. 21 D.

The L. S. Starrett Co., Athol, Mass.

The World's Greatest Toolmakers

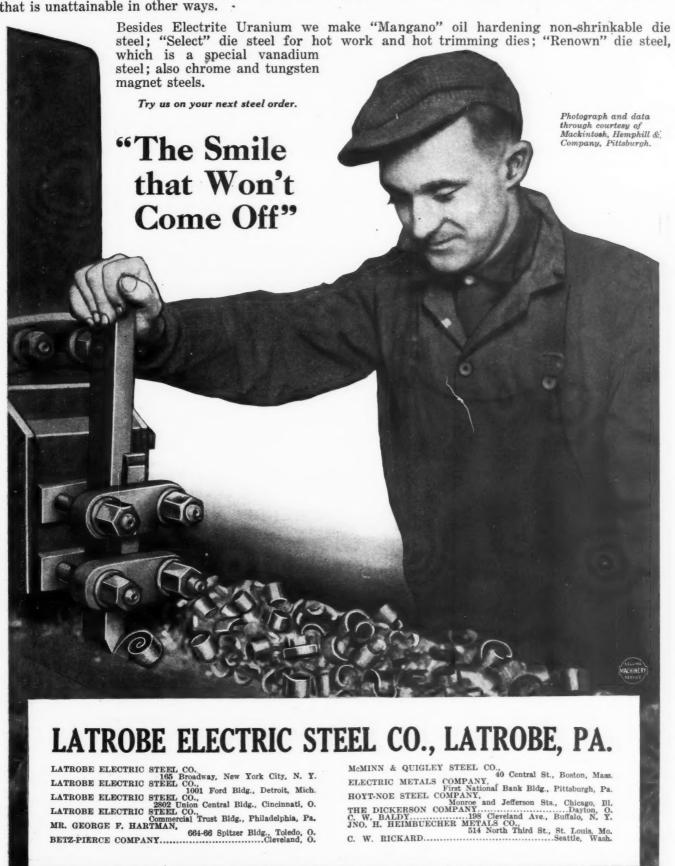


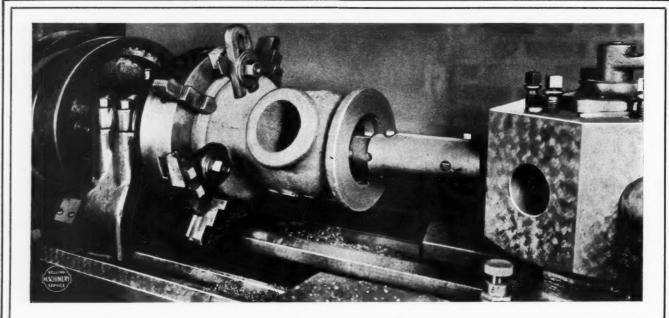
42-682



### ELECTRITE URANIUM STEEL

This planer hand is happy—and with good reason. He has a lot of stock to remove from the plate he is finishing and he has a tool that will carry a good cut—an Electrite Uranium High Speed Steel Tool. He is planing 40—50 point carbon steel with a 1/16 inch speed and a 1/2 inch deep chip. The reason for the staying quality in Electrite Uranium High Speed Steel is due largely to the element Uranium that is introduced by the most modern steel working practice. Uranium gives this steel a toughness that is unattainable in other ways.

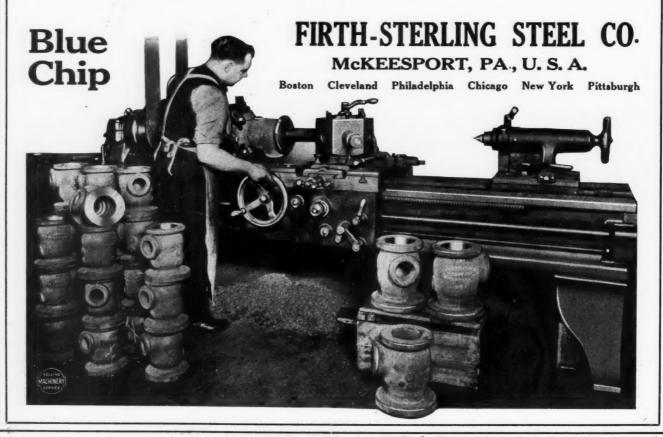


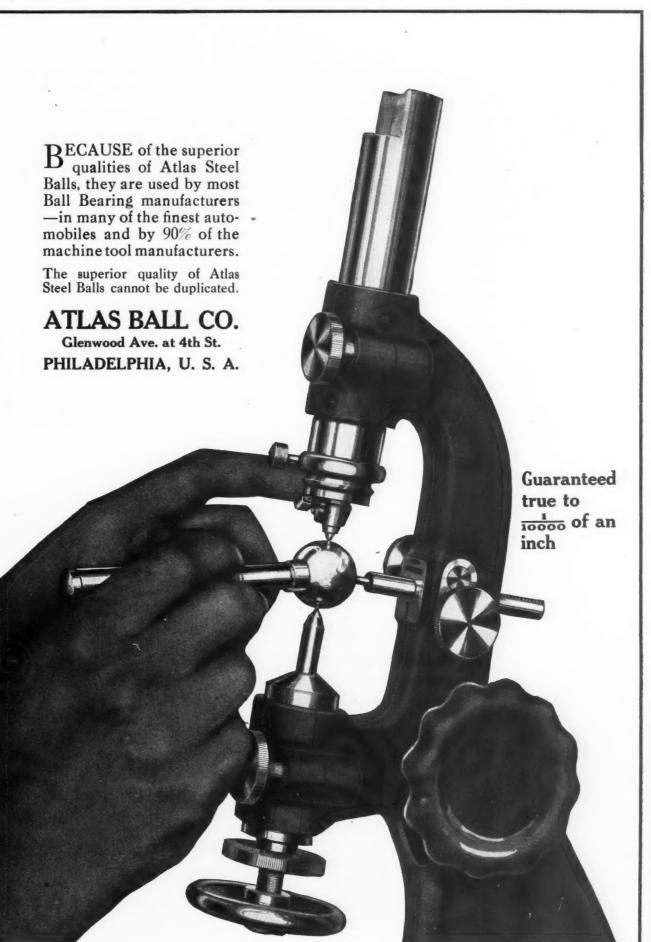


# BLUE CHIP HIGH SPEED STEEL Boosts Boring and Turning Output

The work is cast iron valve bodies which are made in large quantities by a New England manufacturer. When higher production was required heavier turning lathes were installed, but no change was made in the tools. It was a *Blue Chip High Speed Steel* job on the old machines; the same tools are handling it now under a drive that means 100% increase in output.

The work is particularly hard on tools; material is hard and scaly; for boring and facing the tool must work from the end of a 12" bar, on a casting that overhangs 12" from the faceplate; cut varies from 1/8" to 3/16" deep and not a chatter mark is to be seen. Tools made from Blue Chip High Speed Steel stand all the power the heaviest machines are capable of pulling. For turning and boring tools, taps, dies, reamers, etc. Write us.





# RATON & KNIGH Standardized Series LEATHER BELTING



belting.

Leather that is properly tanned for belting is tough, flexible, durable and pre-hensile. It preserves the natural softness and mobility of the skin, ensuring an effective grip on the pulley surface.

We have standardized these requirements of perfectly tanned belt leather. The standard in each case is the highest working efficiency in the finished belt.

Since the market cannot supply tarned belt leather that continuously measures up to Graton & Knight Standards, we tan our own hides. Last year we tanned 285,000 of them, in our own tannery. We tanned them for belts. We tanned them to definite and uniform standards of belting requirements. ing requirements.

This standardization of material is the foundation of Graton & Knight quality.

It makes the Standardization of Graton & Knight Belts an actual, practical thing.

Think what other standardized products have done for you—and consider the standardiza-tion of belting on that basis. Let us send you complete information on the subject.

### The Graton & Knight Mfg. Company

Oak Leather Tanners and Makers of Leather Belting

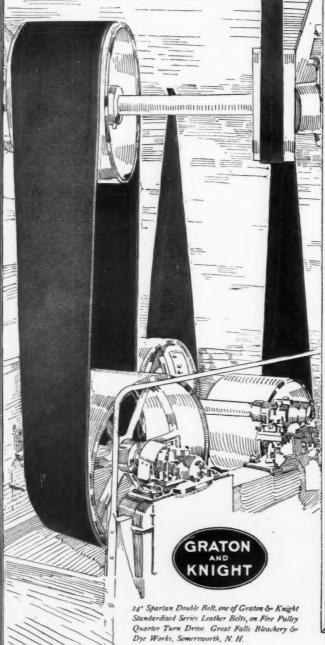
Worcester, Massachusetts, U.S.A.

BRANCHES

Atlanta, Boston, Chicago, Cleveland, Detroit, Fall River, Kansas City, Minneapolis, New Orleans, New York, Philadelphia, Pittaburgh, Portland, Ore., Seattle, St. Louis, Leicester, England.

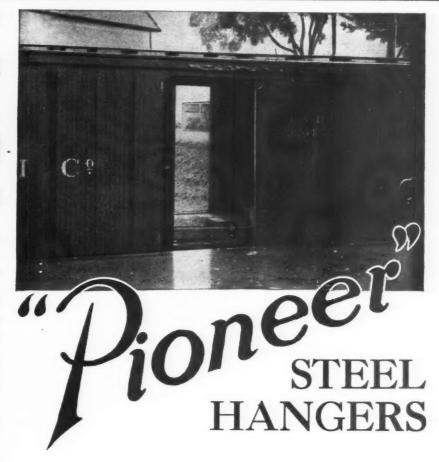
SELLING AGENTS

Graton & Knight Mfg. Co. of Texas, Dallas, Texas. Graton & Knight Mfg. Co. of Wisconsin, Milwaukee, Wis. Graton & Knight Mfg. Co. of California, San Francisco, Cal.



# One Concern Buys 200 to 300 Every Month

When the photographer snapped this 300-lot of "Pioneer" Pressed Steel Hangers consigned to the Jones & Lamson Machine Company, he learned something of the J. & L. hanger supply. For example, buyers of Jones & Lamson machines have their choice of hanger equipment; if they simply specify "best equipment," they are furnished "Pioneer" Hangers—and from 200 to 300 "Pioneer" Hangers per month is the regular Jones & Lamson order.



"Pioneer" Hangers are designed to carry the tremendous weight of shafting, couplings, pulleys, etc., and stand the tug of belts with absolute safety. They are made from open-hearth steel, weigh only one-third as much as cast-iron hangers, cost less to haul and erect, are guaranteed unbreakable, and are actually the cheapest hangers you can install.

Machine tool builders give "Pioneer" hangers the preference for "safety-first" reasons and for quality. Write for booklet, "Transmission Data."

Standard Pressed Steel Co.



# Westinghouse

Reversing Planer Motors and Control



HTTSBURGH P

# The Right Motor At The Right Time

The right motor is that one which will give you the most intense production, combined with high efficiency and utmost reliability. And NOW is the right time for such a motor. Our government must depend primarily for means of transportation upon the car shops, and it naturally follows that the car shops should employ those methods which insure MAXIMUM OUTPUT in MINIMUM TIME with HIGHEST EFFICIENCY.

The accompanying views show a portion of the machine shops of the Pressed Steel Car Co. of Pittsburgh and the Westinghouse Reversing Planer Motors employed on these planers. Westinghouse Automatic Control, also installed, so simplifies the work of the operator that there is no loss of time.

It has taken a great deal of study of machine tool practice to bring our Motors and Control Equipment up to their present acknowledged high standard. Let us help you put your plant on the most efficient basis NOW. It's the right time.

Send for Book No. 3042.

Westinghouse Electric & Manufacturing Co.

East Pittsburgh, Pa.



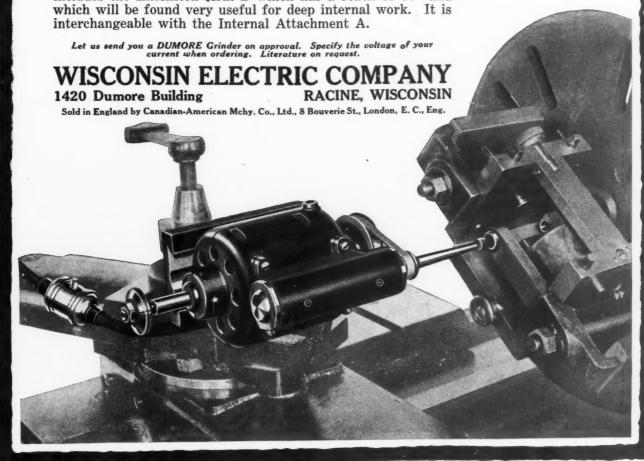
# GrindingBushings OnDrillingJigs

This is one of the many jobs where the DUMORE comes in handy in a tool room. The hardened steel bushings in this Drilling Jig must be finished accurately and both bushings must be ground at the same operation in order to insure perfect alignment. The

### DUMORE PORTABLE ELECTRIC GRINDER

is the ideal tool for grinding dies, gauges and similar work where extreme accuracy is necessary. It is used in hundreds of machine and repair shops for all kinds of grinding jobs. Manufacturers regard it as indispensable for handling the many difficult, hard-to-get-at jobs that continually arise. It will be the most popular tool in your shop.

The high speed at which the DUMORE Grinders operate—10,000 R. P. M. and 30,000 R. P. M.—gives the correct surface speed to wheels of very small diameter. This prevents the wheels from breaking down and your work will be ground accurately and will be entirely free from bell mouth, Equipment A as shown below includes the Internal Attachment A which operates at a speed of 30,000 R. P. M. Equipment B includes the Extension Arm B which has a reach of 10" and



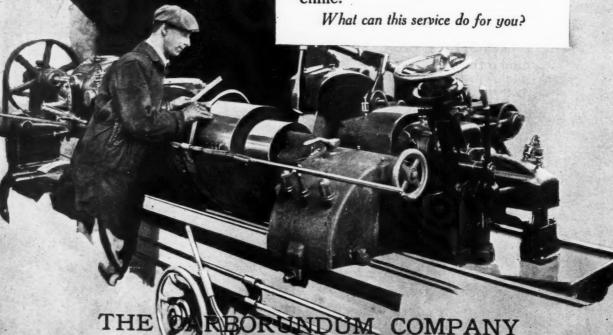
A Page From a
Carborundum
Service Man's
Note Book says:

### "Our Customer Considers this an Extraordinarily Good Performance"

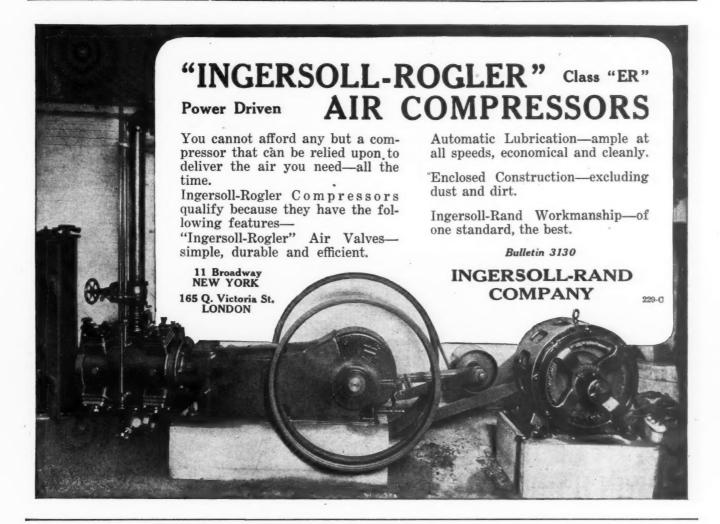
The job is grinding, rough from the sand, chilled iron rolls on a Landis special grinder. The rolls are 32 inches long, 16% inches in diameter and %6 stock is removed. It takes the Carborundum Wheel, 24 grit, L grade, G 3 + bond just 4% hours to do the work.

■ The finish is uniform, the wheel cuts clean and it loses but 1/15 of an inch.

¶ It is the unbeatable grinding combination that gets these results.
 —The right wheel, Carborundum service and a good grinding machine.



NEW YORK CHICAGO PHILADELPHIA CLEVELAND CINCINNATI BOSTON PITTSBURGH



# For Fast, Heavy Duty Metal Cutting THE RACINE

For cutting Angles, Channels, I-Beams, Die Blocks, Pipe, Tubing, etc., at high speed, this Racine Machine leads the pack. It is equipped with the patent return stroke, automatic lifting device-original with these machines— which means higher output and greater blade economy than is possible with any similar machine of equal Blades can capacity. be tightened without wrenches, saw-frame holds itself automatically at any height, stock can be held firmly at any angle and short lengths cut without trouble.

RACINE TOOL & MACHINE CO.

250 Fifteenth Street RACINE WIS., U. S. A.







Spur or Bevel Gears

CAPACITY

No.  $1\frac{1}{2}$ -14 Pitch No.  $2\frac{1}{2}$ -10 Pitch No.  $3\frac{1}{2}$ -8 Pitch

### The Bilton Machine Tool Co.

Succeeding THE STANDARD MFG. CO.

Housatonic Ave., Bridgeport, Conn.

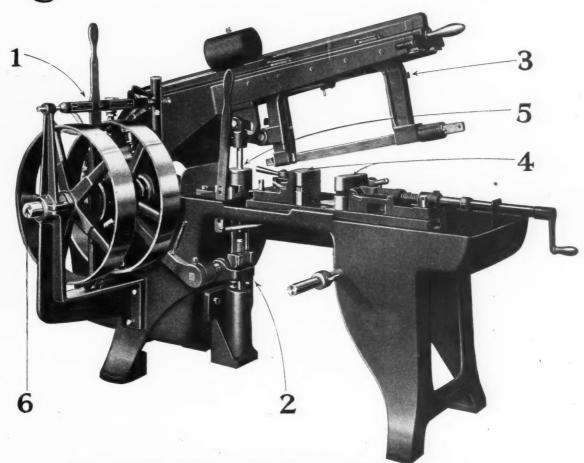
Also Manufacturers of

PLAIN HORIZONTAL MILLERS **AUTOMATIC MILLERS** GEAR HOBBING MACHINES PLAIN AND BALL BEARING BENCH AND COLUMN DRILLS RIVETING MACHINES MILLING CUTTERS

CATALOGUE 20-G ON REQUEST

FOREIGN AGENTS: Alfred Herbert, Ltd., M. Mett Chas. Churchill & Co., Ltd Engineering Co.

# Distinctive Features of the No. 5 M.S.W. High Speed Hack Saw Machine



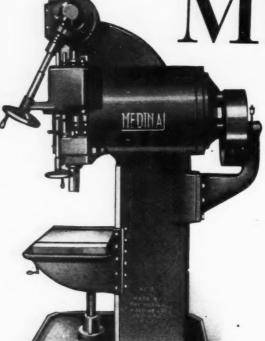
#### DISTINCTIVE FEATURES

- 1. Two Speeds.
- 2. Shock Absorber.
- 3. Extension Frame.
- 4. Patent Swivel-Jawed Vise.
- 5. Automatic Patent Lift.
- 6. Frame Swings on Shaft
- 7. Rotary Pump.
- 8. Knock-off.
- 9. Frame Bearings.
- 10. Tank
- 11. Perfect Blade Alignment.
- 12. Lubricating System.
- 13. Draw-Cut.

For Explanation of these and other features send for Circular

The Massachusetts Saw Works
Springfield, Mass., U.S.A.





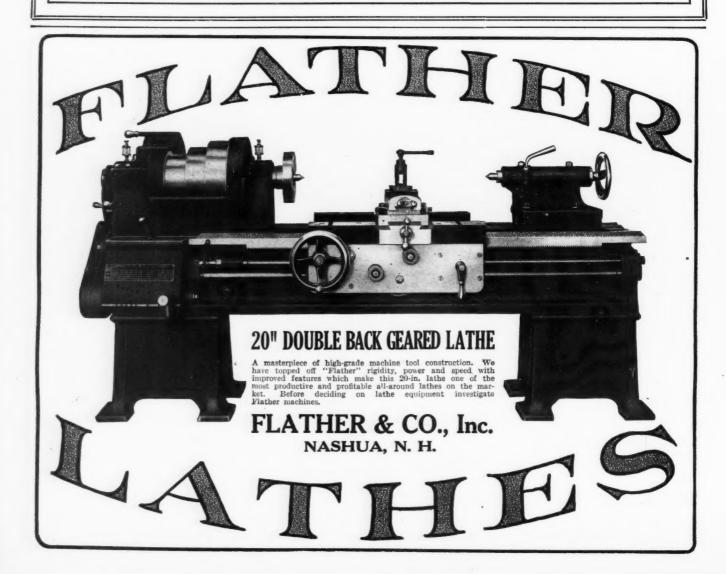
# A Powerful Machine for Heavy Manufacturing

To the experienced man there's evidence of power even in appearance, and some of accuracy, too; for the Medina has the proportion and balance and backing-up metal necessary for absolute rigidity. But for the FULL facts about the accuracy and output that make Medina Drilling Machines extra efficient for manufacturing purposes, it is necessary to go into detail.

Ask us—even if you're not in the market for drilling machines right now.

### MEDINA MACHINE CO.

MEDINA, OHIO, U. S. A.



# The Chicago Automatic

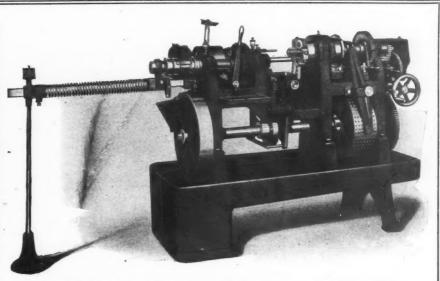
Built Around the Cornerstone of Simplicity

### Chicago Automatic Machine Company

Chicago, Illinois, U. S. A.

Eastern Representative

John MacNab Machinery Co. 90 West St., New York John MacNab, Hyde, England



### The Chicago Automatic Screw Machine

owes a great deal of its serviceability to simple design. There are no complicated mechanisms or involved systems of cams to cause trouble; no countershafts and overhead belts to waste power and interfere with additional equipment, spindle speeds suitable for any stock are obtained by changing two gears on the spindle head; threads are cut withopt slowing spindle speed by means of a die holder revolving in the same direction as the spindle but at higher speed. A clutch mechanism indexes the turret and skips holes not in use. The machine is rigidly built throughout, maintaining alignments and accuracy of work under long, continuous operation.

Write for complete description.



THE PHILIP SMITH MFG. CO., Sidney, Ohio



# Another Angle from Which a STAR LATHE is a Paying Investment

The "Star" Lathe is a paying investment from any angle, but here's one in particular. In the plant of the Hartford Drop Forge Company, Hartford, Conn., a complete, thread-cutting, small capacity lathe is required for intermittent service. Many lathes are a losing proposition under such conditions; but on account of the low cost compared with others, a Star Lathe need not be run all the time to insure proper returns on the investment. It is an ideal lathe for requirements of this kind. Accuracy of construction and operation is second to none, and with taper attachment incorporated it handles a considerable range of work with efficiency not exceeded by lathes at double the cost.

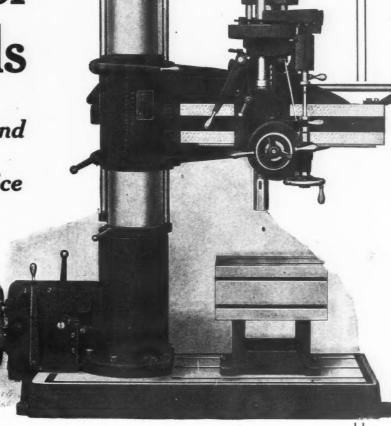
If you have work of this character you need the "Star"; if you have tool room work sufficient to keep a lathe busy all the time, it's still unquestionably the lathe to buy.

Write for catalogue for descriptions of the line.

SENECA FALLS MANUFACTURING CO. 330 FALL STREET SENECA FALLS, N. Y.

# Mueller Radials

Examined and Passed for Active Service



Mueller Radial Drills have been thoroughly examined, tried and tested under ordinary and unusual conditions and are admitted to be in every way qualified for any service they may be called upon to perform.

Material, reinforcement and design of the best.

Speeds, feeds and ranges, many and varied.

Controls, in every case simple, convenient and rapid. Ask for details.

### THE MUELLER MACHINE TOOL CO.

CINCINNATI, OHIO, U. S. A.

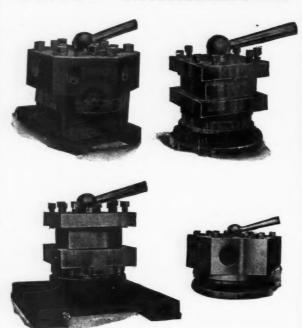
RADIALS

DRILLS

LATHES

### **PHOENIX**

### **Turret Attachments**



### A Necessity in the Modern Shop

Phœnix Attachments are adapted for a multitude of lathe operations that ordinarily require special tools; being particularly well fitted for handling economically, the "shortjobs" so difficult for either turret or engine lathe.

It is an easy matter to attach them to the cross slide of any engine lathe; they are perfectly rigid when set up, extremely easy to use, and are readily released by a three-quarter turn of the handle.

If you'd like to get 100% efficiency from your engine lathes, you'll want to know more about them.

Complete description on request.

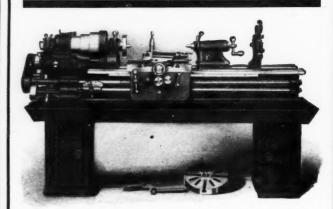
### PHOENIX MANUFACTURING CO.

**EAU CLAIRE** 

**WISCONSIN** 

CLEVELAND OFFICE: 1430 WEST 6th STREET

# The WILLARD 13" Engine Lathe



FITTED with cabinet legs and pan base, is especially adapted for tool room and school purposes. Extra powerful drive permits handling work beyond the ordinary small lathe range. Convenient operation makes for speed. Rigid construction insures uniform accuracy. The "Willard" swings full 13", has complete range of feeds, stands hard driving, is complete in every detail.

We should like to tell you more about these exceptional machines. May we?

The Willard Machine Tool Co.

### W & P PLANERS

Planers with rigidity, strength and power to meet the heaviest demands.

We build rapid, accurate, long service planers of every type, know planer requirements from A to Z, and will be glad to help you pick the machine best suited to your work.

Write for particulars.

WOODWARD & POWELL PLANER CO.

WORCESTER

MASS., U. S. A.



### SOUTH BEND LATHES For the Machine

and Repair Shop
A Practical Lathe at Low Price. 11-inch

to 18 inch Swing. Straight or Gap Beds. Send for free catalog. SOUTH BEND LATHE WORKS 426 E. Madison St., South Bend, Ind.

#### **ENGINE LATHES**

18' to 48' Swing

THE BOYE & EMMES MACHINE TOOL CO.

### USERS OF THE LATHE WITH THE PULL

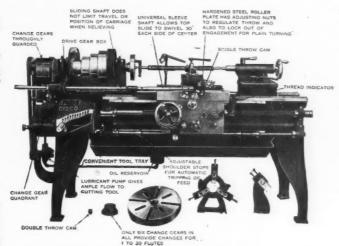
PLEASE NOTE

We find that we have been selling

# **CISCO**Lathes

underweight. That every lathe

manufactured weighs about 200 pounds more than the published weight.



You have been getting your money's worth and always will. Better and better all the time

That's CISCO

### BETTER BUY CISCO

Made in 14", 16", 18", 24" sizes

### THE CINCINNATI IRON & STEEL COMPANY, CINCINNATI, U. S. A.

Harron, Rickard & McCone, San Francisco and Los Angeles. A. R. Williams Mchy. Co., Ltd., Winnipeg, St. Johns, Toronto, Montreal and Vancouver, Can. Hendrie & Bolthoff Mfg. & Supply Co., Denver, Colo. Young, Corley & Dolan, Inc., New York, N. Y. Knight & Wall Co., Tampa, Fla. McArdle, New Orleans, La. R. L. Scrutton & Co., Sydney, N. S. W. Perine Machinery Co., Seattle, Wash. W. F. Davis Machine Tool Co., Cleveland, O. Laughlim-Barney Mchy. Co., Pittsburgh, Pa. Southern Mchy. Exchange, Jacksonville, F.a. J. L. Lindsay, Richmond, Va. Stratton & Bragg Co., Petersburg, Va. Manufacturers Selling Agency, Birmingham, Ala. Marshall & Huschart Mchy. Co., St. Louis, Mo. C. E. Fales Mchy. Co., Detroit, Mich. S. R. Meisen-Helter Mchy. Co., Philadelphia, Pa. Purinton & Smith, Hartford, Conn. H. A. Smith Mchy. Co., Syracuse, N. Y. Herbert R. Lowe, Providence, R. I. Badger-Packard Mchy. Co., Milwaukee, Wis. Dale-Brewster Mchy. Co., Chicago, Ill. Thompson Tool and Supply Co., Indianapolis, Ind. John MacNab, Hyde, England, Grimaldi & Co., Genoa, Italy. A. J. Coccaro & Co. (New York) for France and Spain, Chinese-American Products Exchange Co. (New York) for China.

### "PREPAREDNESS

RISING COSTS"



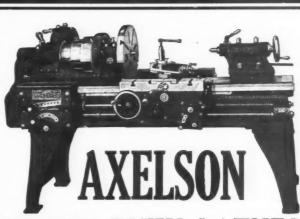
Are you prepared to make those small parts the most economical way—the Dalton way?

With a "Dalton Six" Type B-4 as part of your shop equipment, is to be prepared to combat your most powerful enemy, "Rising Costs."

Add a "Dalton

Six" to your battery of machinery. You will then be prepared to meet the enemy.

Dalton Manufacturing Corporation
1911-15 Park Ave. New York, U. S. A.



HEAVY DUTY LATHES ALWAYS SATISFY

BECAUSE they are the very best lathes for ALL-AROUND work—very best in every sense: Quality of Material, Workmanship, Accuracy, Rigidity and numerous other qualities.

You cannot buy a better lathe. Scores of satisfied owners of AXELSON LATHES are our best arguments. Better investigate.

**AXELSON MACHINE CO.** 

Dept. B

Literature

sent upon

request.

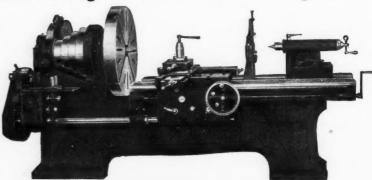
LOS ANGELES, CAL.

### Two Lathes in One at a Great Saving in Cost -22-36" Gap Lathe

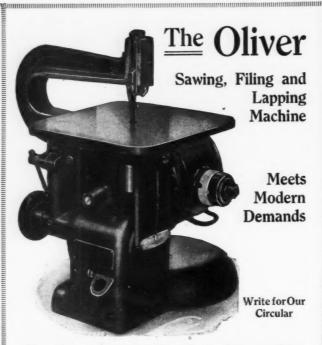
Our Heavy Duty Sliding Extension Gap Lathe is a most necessary tool to the shop with a wide range of work. Being practically two lathes in one, it is sure to be kept busy all the time.

This lathe has main and sliding beds, very heavy and broad. They are braced over their entire length. The lathe loses none of the accuracy and rigidity of the usual type lathe. It is equipped with powerful back gears—has 6 quick changes of geared feeds, 12 spindle speeds and cuts threads 2 to 30—all steel gears throughout.

Let us send full details in Bulletin "M."



BARNES DRILL COMPANY, Inc, 814 Chestnut Street, Rockford, Ill., U. S. A.



The order of the day calls for the "latest models." Machines must be changed frequently to meet this demand—new parts must be designed, new patterns made. There is no time for the handmade dies of yesterday—yet the work must be just as accurate, just as well finished.

The OLIVER FILING AND LAPPING MACHINE is the solution of the skilled patternmaker's problem. He can devote all his time to planning and designing new parts while an ordinary mechanic cuts and finishes them in 30 to 60 per cent less time with the "Oliver."

Oliver Instrument Company ADRIAN, MICHIGAN

# DWIGHT SLATE MARKING MACHINE Send for Catalogue Trade Marks, Letters or Numbers put on your work at REDUCED COST with quality improved by these machines. Lettering Dies cut by EXPERT ENGRAVERS.

Noble & Westbrook Mfg. Co. Hartford, Conn. U.S.A.

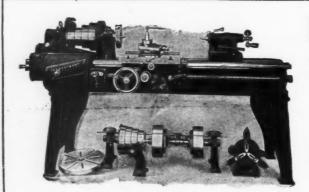
### **Crescent Wood Working Machinery**



will satisfy those particular buyers who want enduring service in wood working equipment. Ask today for catalog telling about our line of

band saws, jointers, saw tables, planers, disk grinders, planers and matchers, swing cut-off saws, shapers, borers, hollow chisel mortisers, variety and universal wood workers.

THE CRESCENT MACHINE CO.
56 MAIN STREET LEETONIA, OHIO



### Read Our Specifications

Before going ahead get a copy of our specifications of this 14" engine lathe. It's a

### CARROLL-JAMIESON Screw Cutting Lathe

It has double back gears, quick-change gears giving thirty-two changes of feed without removing a gear, nine spindle speeds,  $2\frac{1}{2}$ " belt drive from three-step cone.

Drop a line now for a set of specifications.

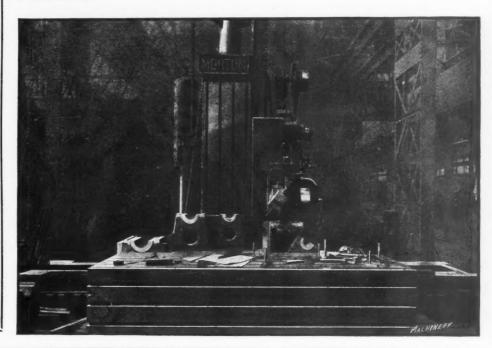
THE CARROLL-JAMIESON MACHINE TOOL CO., 257 Davis St., Batavia, Ohio

# The Morton Draw-Cut Traveling Head Planer

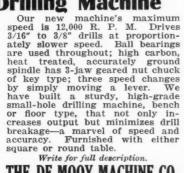
Unequaled for Manufacturing or General Shop Work

### MORTON MFG. COMPANY

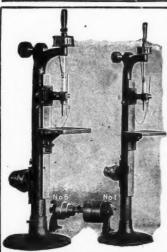
Muskegon Heights MICHIGAN THE remarkable adaptability of Morton Planers makes them profitable machines in any shop. Their range is practically unlimited. They are ideal for general requirements, and so simply designed and flexible that they can be readily adapted for any special work. Compared with the housed planer, the Morton requires but half the floor space and one-fourth the power, may be used either as a portable or a stationary machine, can be reversed into a push cut planer if desired, and handles all boring and milling easily and accurately regardless of the size of the piece. Convenient, powerful—and needed in most shops. Send for Bulletin 8D.



#### Demco High Speed Drilling Machine



THE DE MOOY MACHINE CO. 706 Frankfort Ave., Cleveland, O.



# No. 1 Drill—14" 265 lbs., Capacity ½" No. 5 Drill—16"

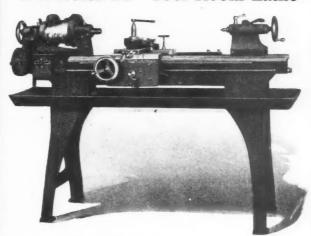
430 lbs., Capacity 3/4"

A splendid line of single spindledrillingmachines-

FRANCIS REED CO.

43 Hammond Street Worcester, Mass.

### Worcester 11" Tool Room Lathe



This simply designed, steady-going, efficient machine is built along the same general lines of our Standard 11" Lathe, with the addition of Steel Pan, Taper Attachment and Drawin-chuck. The Taper Attachment is graduated and can be easily set for turning; Drawin-chuck operates by means of a closer and split collet of tool steel, hardened and ground. The lathe swings 12\(^3\)\(^4\)" over bed, 8" over carriage, cuts threads from 2 to 40, takes turning tools \(^1\)\(^2\)" x 1". Write for further details.

#### WORCESTER LATHE COMPANY

68 Prescott St.

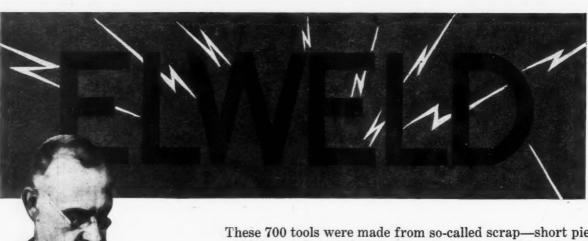
WORCESTER, MASS.

## 700 ELWELD TOOLS

For One Concern

That Would Indicate They Were Good Tools Wouldn't It?





These 700 tools were made from so-called scrap—short pieces of high speed steel that could no longer be used to advantage in the usual manner. We Elwelded these pieces to tool steel shanks, conforming to sizes designated, and 700 new high speed tools resulted at a fraction of their first cost. Compare this cost with that of new tools and it'll be an eye-opener.

And don't overlook the significance of the repeat orders we've had from these people. The fact that they've come back again and again for more Elweld tools surely proves that they're saving money and we're giving satisfaction.

Let us show you a sample of our work. We're increasing our capacity again and can give your specifications prompt attention. Any tools from  $1\frac{1}{2}$ " x  $2\frac{1}{2}$ " down to  $\frac{1}{2}$ " x 1".

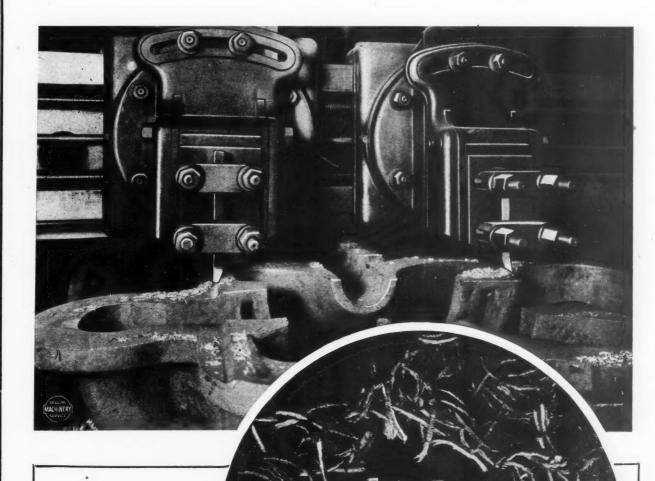
We do commercial butt welding also, large or small, and will be glad to figure with you.

# The Electric Welding Co.

(Superior Viaduct)

Cleveland

Ohio



These are

### High Speed Steel Tools

Would You Believe it?

This job is typical of some of the work put up to Uranium tools.

up to Uranium tools.

These two pump casing castings are made of acid-proof bronze, an exceptionally tough metal to cut; the chips shown are full size and indicate how short the metal flakes under the cutting action. Uranium steel tools are the only tools that stood up under this work.

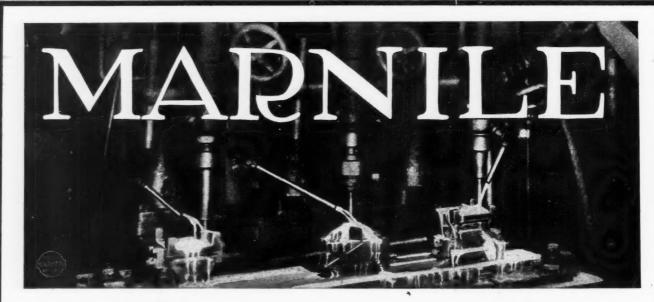
You, no doubt, often meet just such tough planing or turning propositions and then you need Uranium for best results.

Your own steel man can tell you about Uranium High Speed Steel; if not, consult us

Standard Alloys Company

Forbes & Meyran Avenues

PITTSBURGH, PA.



### A Good Compound for Tough Drilling

The machine is a Prentice Drill Press, the work is chromium high-carbon steel thrust bearing washers—"tough old birds," the operator said—but the cutting compound is Marnile. So the drills cut clean and cool, don't tear the holes, and stand up 25 per cent longer between grinds than when oil or soda water was used. Output is 25 per cent greater and lubricant bills are 75 per cent lower. Interesting and profitable results, aren't they?

Let us send a sample of Marnile to prove similar results on your work.

GEORGE A. HAWS, Inc., 135 Front St., New York, N. Y.

## Reducing the Thread Cutting Costs

The New NAMCO Positive Collapsing Tap offers an immediate solution to this high threading cost problem.

The NAMCO Tap differs from all other collapsible taps both in design and construction and features many advantages over the old style of tap, namely

-capacity for any depth hole.

-positive collapsing action.

—proper support for chasers while cutting.

—all operating mechanism within body.

The new catalog explaining in detail the reasons for the improvements claimed for NAMCO Collapsible Taps will be sent on request. Ask for NAMCO Tap Catalog "B."

(Capacities 14 inch up)

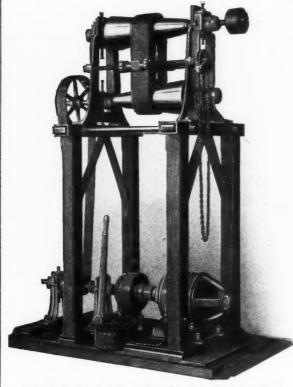
### THE NATIONAL ACME COMPANY, CLEVELAND, OHIO

New England Plant: Windsor, Vermont Canadian Plant: Montreal, P. Q.

BRANCH OFFICES-NEW YORK BOSTON CHICAGO DETROIT
ATLANTA, SAN FRANCISCO. REPRESENTATIVES IN FOREIGN COUNTRIES

Makers of Gridley Single and Multiple Spindle Automatics at Windsor, Vermont; and Acms Automatics, Threading Dies, and Screw Machine Products at Cleveland, Ohio





Constant Speed Alternating Current Electric Motor, combined with Moore & White Speed Change giving variable speed, and Moore & White High-Speed Friction Clutch for starting under load.

### Speed Regulation with Alternating Current Motors

The Moore & White Speed Change permits the drive from an A.C. motor to be varied in speed as freely as when D.C. motors are used.

By its use, lathes, boring machines, and machinery for pumping, conveying, bleaching, drying, textile manufacture, etc., can be made to operate at maximum efficiency all the time, thereby overcoming the chief drawback to the use of alternating current.

### MOORE & WHITE SPEED CHANGES

operate without frictional slip. Their special feature is the use of a pair of flexible "transformers," one on each cone, in which tapering strips build the cone up to cylindrical form. Each strip acts like part of the cones while in contact with it. It is not necessary to use a narrow belt.

Owing to the absence of slip, the speed control is very exact. Taken with the inherent steadiness of A.C. motors, this is a very valuable feature for many classes of work demanding accurate speed regulation.

We furnish the complete Speed Change in vertical and horizontal form in sizes from 1 to 200 H.P.

To manufacturers wishing to incorporate the Speed Change in their own machines we sell the patented transformers separately.

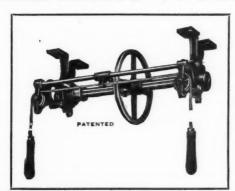
Write for booklet, "Speed Changes without Frictional Slip," giving full particulars of sizes and styles.

### THE MOORE & WHITE COMPANY, 2707 to 2737 N. 15th St. Philadelphia, PA.

Makers also of Moore & White Standard and High Speed Friction Clutches

NEW ENGLAND REPRESENTATIVE: Gilbert Howe Gleason, 141 Milk Street, Boston, Mass.

### COUNTERSHAFT GRINDER WORK



"DALTON" (Patented) Grinder Countershaft is designed for use on small lathes of all makes, using either internal or external grinding attachments.

The hangers are universal in adjustment for use upon either ceiling or wall.

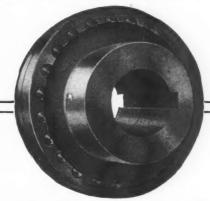
Manufactured only by the makers of the "DALTON SIX" Lathe.

Send for Bulletin.

Dalton Manufacturing Corporation 1911 PARK AVE, NEW YORK, U. S. A.

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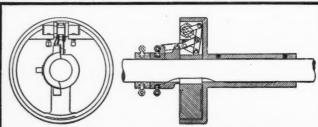


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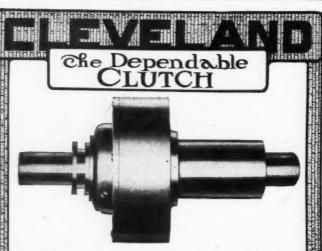
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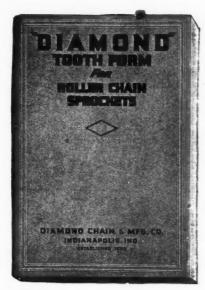
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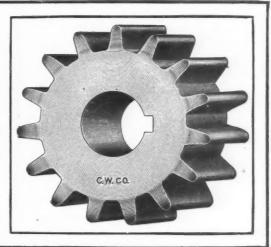
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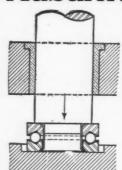
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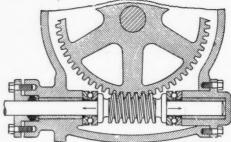
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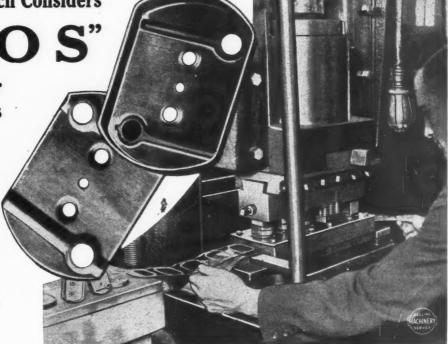
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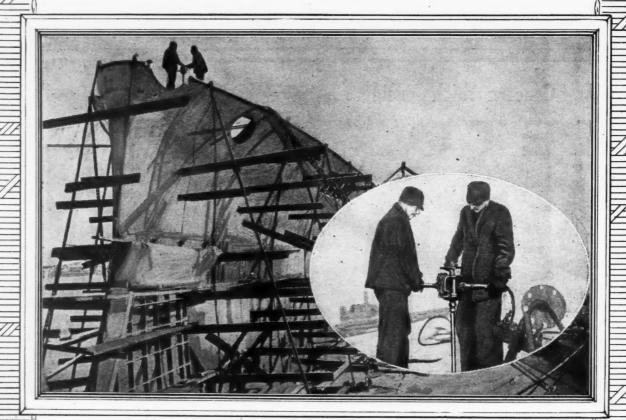
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The rough usage to which pneumatic tools are generally subjected makes staunchness and reliability essential qualities in every detail of construction.

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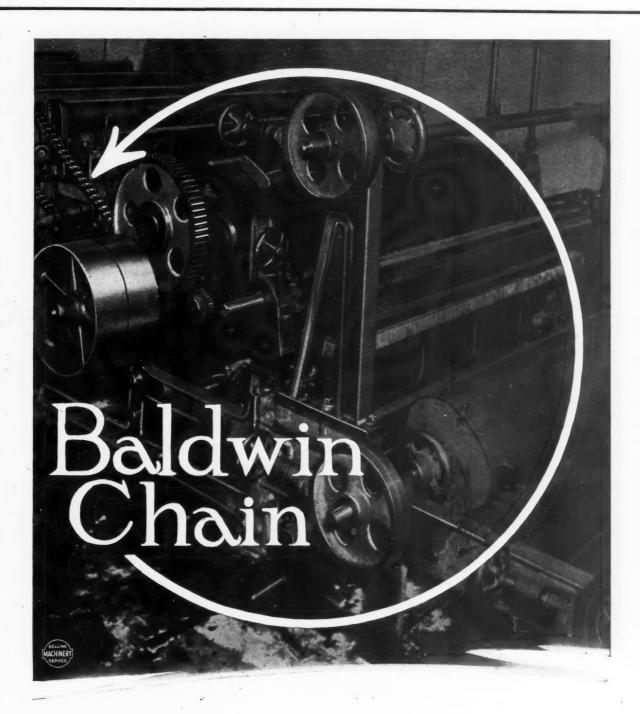
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The tide of her industrialism swells steadily.

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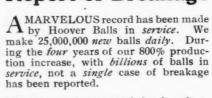


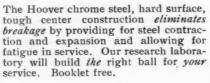




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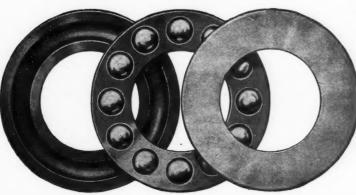
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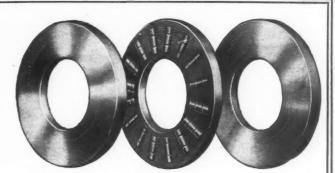
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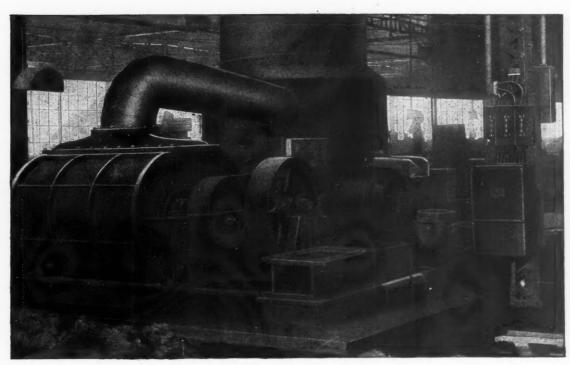
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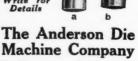
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ARE HANDY TO HAVE IN THE SHOP

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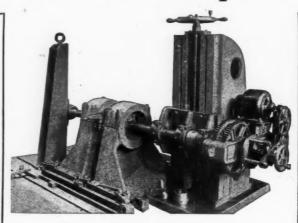
# The Pedrick Column Boring Machine Is Needed In Your Shops This Minute

Orders are coming in for this machine in groups—not singly. And as soon as its merits are generally appreciated larger numbers will be wanted.

Even a casual inspection will impress these facts:

Simplicity Range of Work Power Moderate Price

The unusual boring capabilities of the machine afford new methods of doing work. The boring bar may be passed through



Boring and Facing a Pair of Pedestals

# PEDRICK TOOL & MACHINE COMPANY

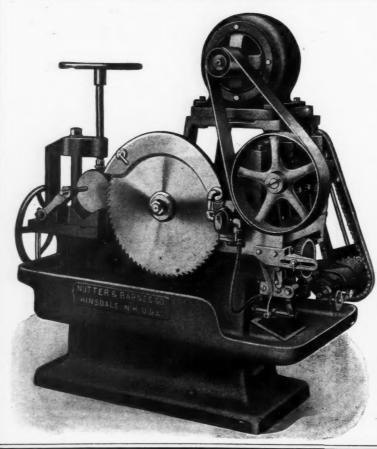
3639 North Lawrence Street PHILADELPHIA, PA.

Manufacturers of Portable Cylinder Boring Bars, Crank PinTurners, Pipe Benders, Portable Milling Machines, etc. the work with a cutter head traveling along the bar to do the boring, or the bar feeds in the regular manner with the cutter keyed fast or operating auxiliary boring bars. The machine may be set-up in a permanent position or it may be taken to the work.

If you need more boring machines these advantages must appeal to you. We have the machine; it has been tried out and is not an experiment.

Send for your circular now.

# Nutter and Barnes Cutting-Off Machines



Massiveness without clumsiness, convenience without superfluous parts, speed, accuracy and range—all combine to put these machines in a distinct class. Size of saw considered, their capacity is greater than any other cutting-off machine; their economy in blades and saw kerf is remarkably high, while their ability to stand hard, driving service is a factor that insures highest returns on the investment.

Complete Details in Catalog.

#### NUTTER @ BARNES CO.

The Metal Cutting-Off Machinery Specialists
HINSDALE - NEW HAMPSHIRE
13 South Clinton Street, Chicago

FOREIGN AGENTS: England, Alfred Herbert, Ltd., Coventry, England, Scandinavia, Wilh. Sonesson & Co., Ltd., Malmo, Sweden; Copenhagen, Denmark. Russia, C. Schinz, Petrograd. Allied Machinery Co. of America, 19 Rue de Rocroy, Paris, France; Via XX Settembre 12, Turin, Italy; 16 Seidengasse, Zurich, Switzerland; Ekaterininskaya 6, Petrograd, Russia; Malaya Lubianka 16, Moscow, Russia. Spain, Socieded General de Representaciones, Madrid. Australia, A. Asher Smith, Sydney. South America, A. G. Burbanks, Buenos Aires, A. R. DOMESTIO AGENTS: Swind Mchy. Co., Philadelphia, Pa. Patterson Tool & Supply Co., Dayton, Ohio.



# Grant Riveters

#### Help Make Good Shears

This little battery of eight bench type Grant Riveters rivets 240 gross scissors per

day for the Acme Shear Company, Bridgeport, Conn., without breaking a single casting. The Acme Company probably makes more scissors, shears, etc., than any one concern in the world. Considering the finish and durability of their product, their choice of Grant Riveters is significant.

Grant Machines rivet perfectly, noiselessly, economically and at record breaking speed
GIVE GRANT RIVETING A TRIAL

GRANT MANUFACTURING & MACHINE COMPANY N. W. STATION, BRIDGEPORT, CONN.

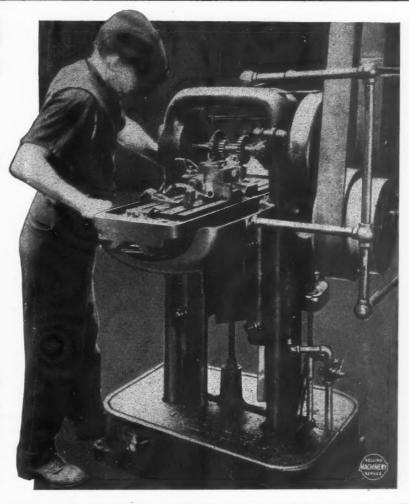
# BRIGGS MILLERS in the "Hudson" Plant

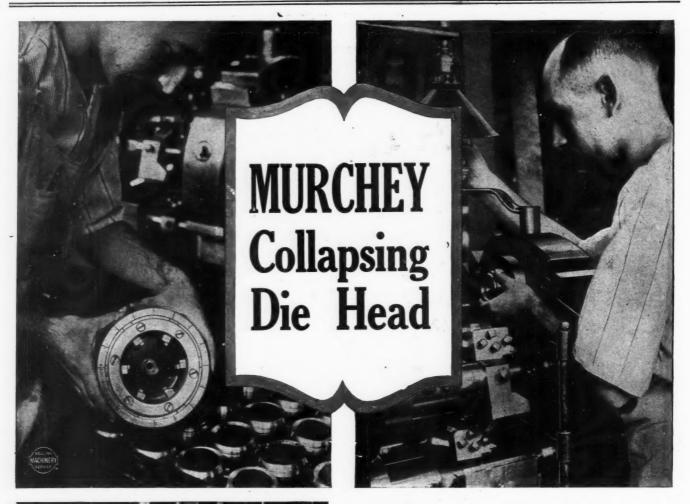
Many of the foremost manufacturing concerns of the country have learned that differentiating between milling and "Briggs" Milling is a profitable departure. They've found that over a wide range of application "Briggs" means better work and more of it, greater economy and longer service. In the Hudson Motor Car Co.'s plant, Detroit, Mich., "Briggs" Millers are making a particularly fine showing, being used exclusively on many operations requiring the closest limitations. It'll pay you to investigate "Briggs" possibilities on your work.

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DOMESTIC AGENTS: Chandler & Farquhar Co., Boston, Mass.; Vandyck Churchill Co., New York and New Haven; Swind Machinery Co., Philadelphia, Pa.; Syracuse Supply Co., Syracuse, N. Y.; O. R. Adams, Rochester, N. Y.; Brown & Zortman Machinery Co., Pittsburgh, Pa.; English & Miller Machinery Co., Detroit, Mich.; Federal Machinery Sales Co., Chicago, Ill.; Vonnegut Machinery Co., Indianapolis, Ind. FOREIGN AGENTS: Allied Machinery Co. of America, Paris, Turin, Zurich, Petrograd, Barcelons; Burton, Griffiths & Co., Ltd., London, Manchester and Glasgow; Andrews & George, Tokyo.







# 750 in 10 Hours

These pictures were secured recently from a western manufacturer who has a habit of short-cutting his way to results with the best equipment that can be bought.

They show Murchey Die Heads—12 of 'emoperated on 12 New Britain Automatics, cutting the threads in nose pieces for 3" shells. Thread is  $2\frac{1}{2}$ " diameter, 20 pitch Wentworth, 5 threads to the piece.

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Murchey Tools are high speed thread cutters. Their work is clean cut, accurate, finely finished and economically done. Practically every threading operation can be handled with taps and dies picked from the Murchey stock. If special tools are required we can furnish them in short order.

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W. L. BRUBAKER & BROTHERS

MILLERSBURG EASTERN REPRESENTATIVES: F. E. Harrison, 50 Church Street, New York. W. Searls Rose, 50 Church Street, New York. PA., U. S. A.



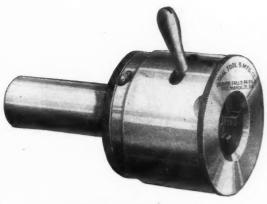
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Champion Expanding Mandrels hold securely because they expand uniformly and grip positively without distorting the work. One of the greatest economies you can make is to junk your whole stock of solid mandrels for Champion Expanding Mandrels.

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FOREIGN AGENTS: Alfred Herbert, Ltd., Great Britain, Italy, France, etc. V. Lowener, Copenhagen, Stockholm. Spliethoff, Beeuwkes & Co., Rotterdam. W. R. Grace & Co., Chili, Peru and Bolivia.



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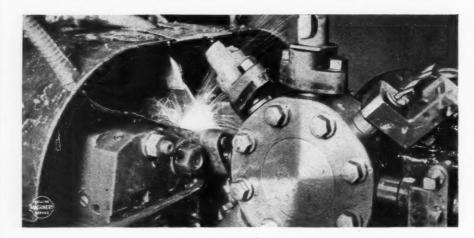
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CLIMAX Mineral Lard Oil is a scientific combination of the best fatty oils and has been used successfully for 40 years for all manner of cutting operations. It can be used as a base for many cutting oils or can be used straight, and if desired may be readily converted into a water solution by the addition of a small quantity of sal soda and water. It prolongs the life of tools and increases output; does not gum, separate or turn rancid; does not cause infection in open wounds. Truly, for many purposes Climax is without an equal.

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A thorough soaking in OAKITE Solution, then a simple steam wash, and waste is absolutely clean and a better absorbent than when new.

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With the Acme reamers you can get an expansion as fine as .0005 in a few seconds, and a maximum expansion of the blades of 1/8". When the blades are worn out they can be renewed.

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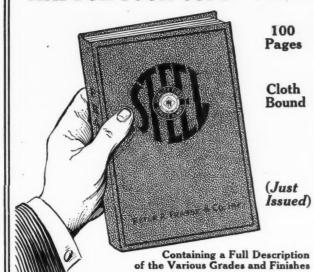
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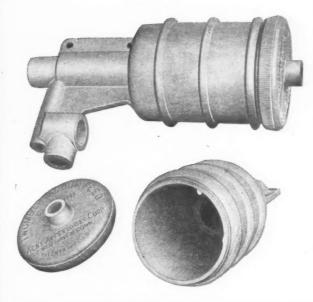
"We have a definite interest in the mechanisms for which we die-cast parts," says Mr. Micrometer.



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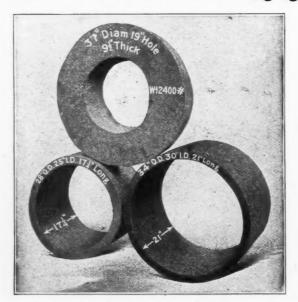
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For Supplying Lubricant to Machine Tool Cutters

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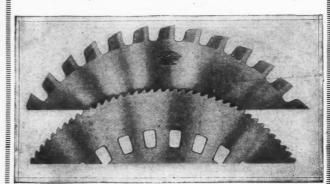
#### A" HARTFORD" Die Filing Machine

accomplishes many times more work than hand filing, at the same labor cost, and does it with greatest accuracy. More details on request.

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We make them for every purpose—hot or cold cutting, and for all makes of machines.

The economy of their use is worth your investigation.

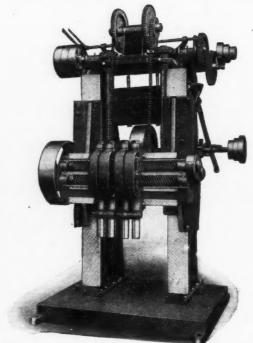
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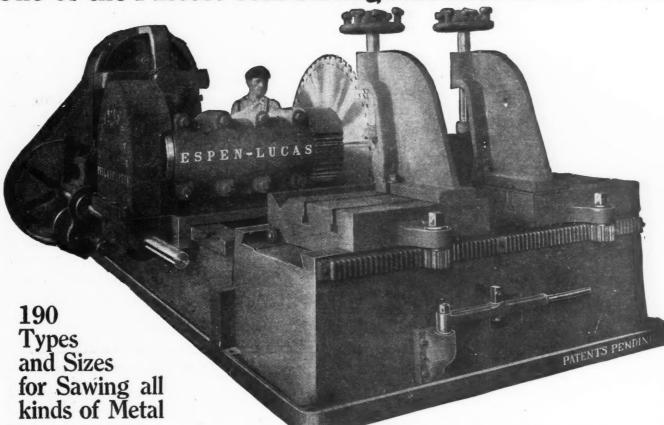


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13-Inch High Speed Drill

All bearings are bronze bushed and provided with ring oilers. The spindle has ball thrust bearings. The sleeve is graduated in inches.

> New lubrication features No leakage of oil

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Manufactured in sizes  $2\frac{1}{2}$ , 3,  $3\frac{1}{2}$  and 4 foot by

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A most practical machine for the purpose for which it was built—to drill 9/16" holes and under with speed and accuracy that make for greatest efficiency. The "Johnson" spindle and the other features of construction will interest you. Ask for details.

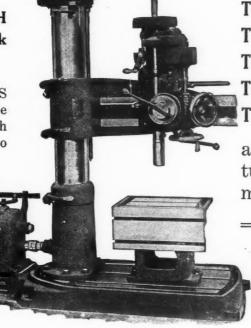
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1" Drill THROUGH Cast Iron 2" Thick in 7 4/5 Seconds.

OTHER RECORDS equally as remarkable in iron and steel with high speed drills up to  $2\frac{1}{2}$  inches.

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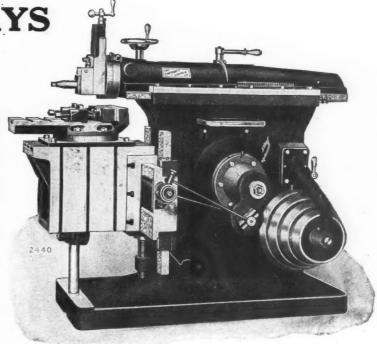
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This EXCLUSIVE feature, being used by us, together with SQUARE WAYS with SIGHT FEED OILERS and FULL LENGTH TAPER GIBS endwise adjustable by SINGLE SCREW for taking up wear, are a few of the characteristics that place CINCINNATI SHAPERS in a class by themselves.

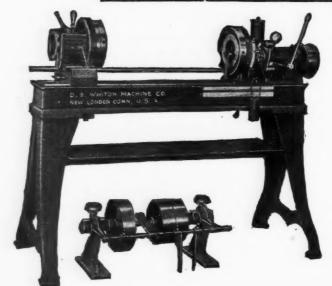
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THE CINCINNATI SHAPER COMPANY CINCINNATI, OHIO

# REVOLVING CENTERING MACHINE

FOR ACCURATELY CENTERING FINISHED SHAFTS

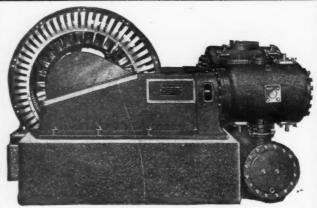


The cut shows new Revolving Centering Machine—a large size of the well-known machine of this type. It is heavier throughout and has capacity to center shafts up to 5 inches in diameter.

Constructed same as the smaller machine and embodies all the special features.

Circulars and prices sent upon application.

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Hand or Power Operated

THE MERRELL MFG. CO. 15 CURTIS STREET TOLEDO, OHIO

#### **ARMSTRONG**

Genuine Stocks and Dies



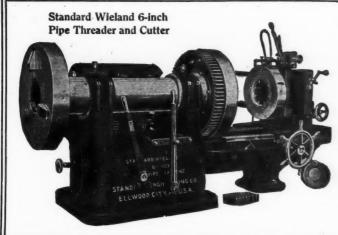
Pipe Threading and Cutting-Off Machines

Our dies can be adjusted to the variations in the size of fittings. They can be worked with less labor and the desired result accomplished in less time than with other dies. They are interchangeable in the stock, sharpened without drawing the temper, easily adjusted and kept in condition. Page 29 of our catalog gives you the details regarding our Pipe Threading and Cutting-off Machines. Sent on request.

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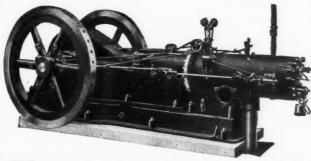
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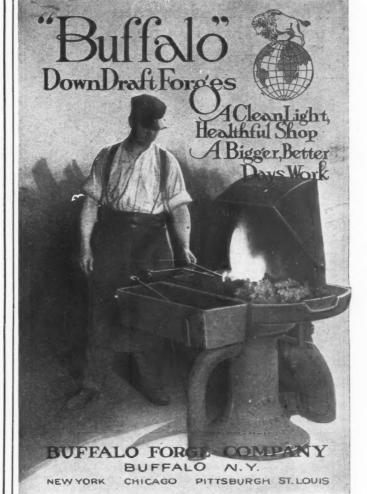
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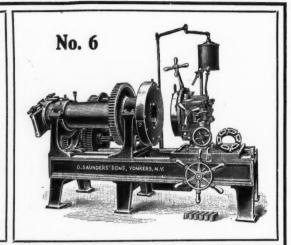
#### for Quick and Accurate Pipe Threading and Cutting

Saunders No. 6 is built for business and embodies every facility for quick and accurate service.

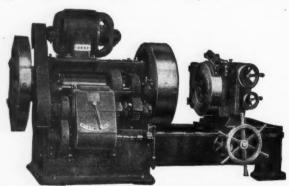
Special gearing gives ample power, without large pulleys and tight belts. Cone pulleys and interchangeable gearing—controlled by lever—vary speeds according to sizes to be cut. The adjustable die head—our patent—with interchangeable chasers, threads from 2½ to 8 inches and releases pipe without stopping or reversing the spindle. There are no complicated attachments—the whole mechanism is direct and easy to operate.

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Because a lot of time is wasted if the speed is not just right for every size and material of pipe.

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has a single-pulley drive with gear speed variation. This means that the belt speed is constant, not lowest when it should be highest. The belt tension is always proportional to the power transmitted—economy of power. The belt contact is constant and always adequate.

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TEN

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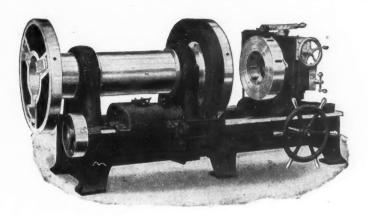
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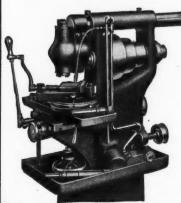


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For Shells and General Use.

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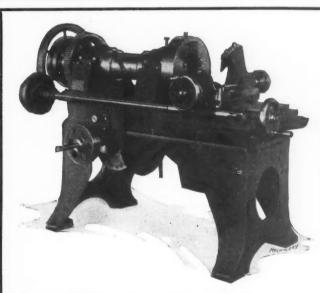
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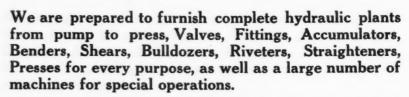
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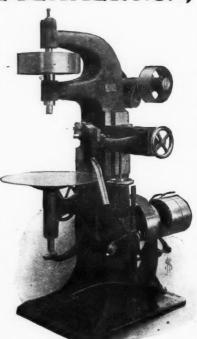
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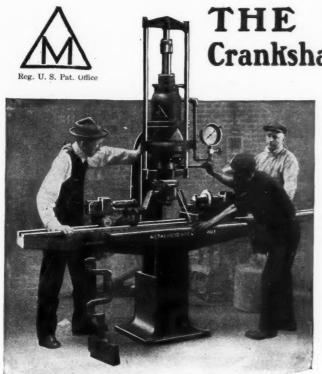
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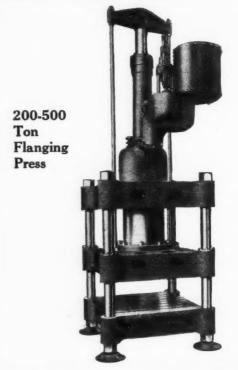
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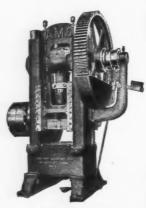
The Toledo Machine & Tool Co. TOLEDO, OHIO, U. S. A.



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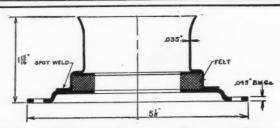
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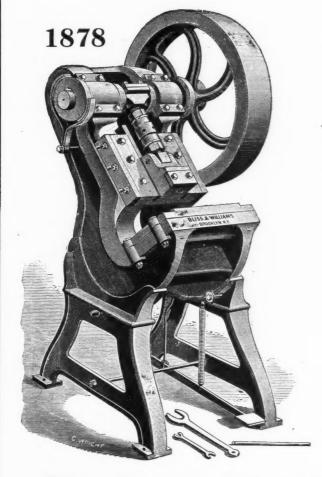


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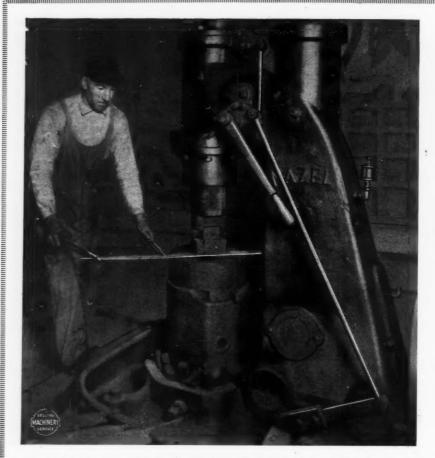
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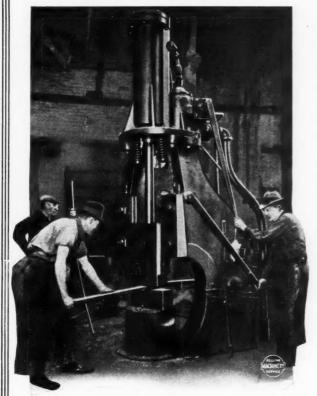
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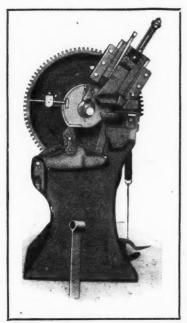


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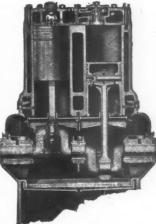
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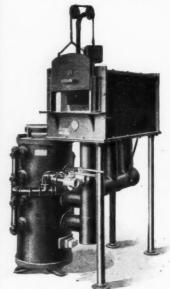
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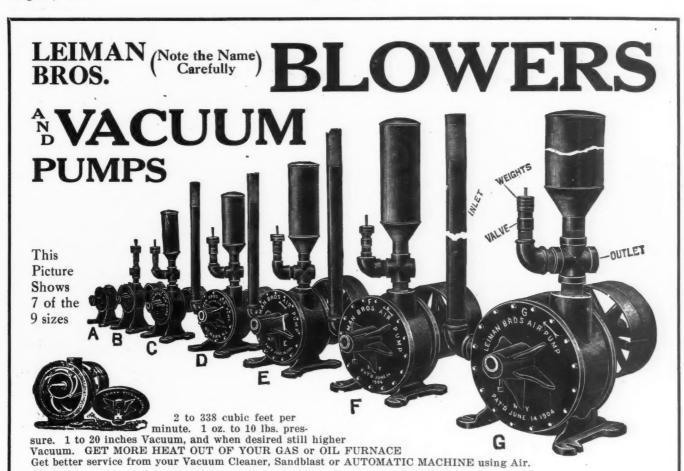
#### PHOENIX DIE CASTINGS



Finished Die Castings of high quality, good workmanship and perfectly compounded alloys. Let us send booklet and more details.

# PHOENIX DIE CASTING CO.

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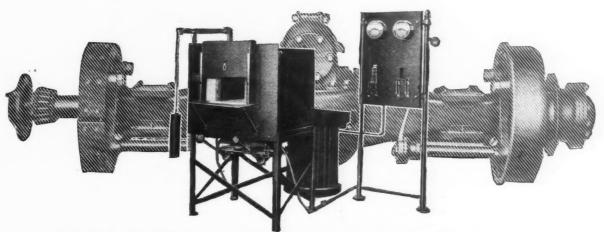


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# "The Control of Quality"





HOSKINS Electric Furnaces The leaders in the field control tool quality with Hoskins Furnaces—as does Timken.

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HIGH SPEED STEEL



APEX STEEL CORPORATION

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Do You Analyze Your Ferro-Tungsten? 

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The value of a product is largely controlled by the purity of the materials of which it is made.

We Guarantee -

Our Ferro-Tungsten to this analysis:

Tungsten 70	0 to 80%
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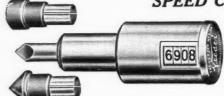
Our facilities are of the very best due to a strictly modern plant and equipment. We are able to offer quick deliveries. Write, Wive or Cable for prices.

THE VANADIUM-ALLOYS STEEL CO.

Makers of "Red Cut Superior" - A Quality High Speed Steel

Capacity speeds may be overreached - or full productive capacity never reached - unless you take count of revolutions-per-minute.





report speeds to a turn. Can be started or stopped at just the right moment by means of clutch which engages mechanism. Price, with two rubber tips, \$3.00. Circular gladly sent.

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Makers of Cyclometers, Odometers, Tachometers, Tachodometers, Counters and Die Castings



Right Where You Can
Put Your Hand on Them

is where your tools should be

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make tool cases with a place for every-thing. Tool cases that are not only convenient, but compact, strongly built and nicely finished. Shipped direct from factory; price reasonable.

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You are not put to the trouble of filing and fitting when you use our Finished Machine Key. We finish them *complete*—all ready to drive,



and you can always depend upon accurate machining and true size. We have special facilities for making Machine Keys any length, width, depth, style or taper. If your keys are costing too much—get our prices.

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STANDARD GAUGE STEEL COMPANY, Beaver Falls, Pa., U. S. A.

BRANCH OFFICES: Chicago, Ill., and Philadelphia, Pa. Pacific Tool and Supply Co., San Francisco, Cal. Dilworth Lockwood & Co., New York. R. B. Ridgley, Detroit, Mich. A. L. Maeder Co., Portland, Ore. Hall & Pickles, 64 Port St., Manchester, England.

100 per cent perfect water soluble—designed especially for the consumer who appreciates the highest standard of quality at a minimum cost.

Each of our products is backed by a reputation of 50 years in business.



Our business was founded qualitydeveloped on quality—a we will and we will continue to quality.

A scientifically treated lard oil. A base oil of quality equal to No. 1 lard oil. May be reduced with mineral oils for any machining operation. We will be glad to quote you or ship a barrel for test.

> Write for our book "Kleen Kut Facts"-This is a treatise on machine tool lubrication.

D. A. STUART & CO., Inc. CHICAGO, ILLINOIS 29 So. La Salle St.

FACTORY: 350-360 E. ILLINOIS STREET

**EDGEMONT Extended Sleeve Clutch** 

Designed to drive wood or steel pulwood or steel pul-leys, gears, drums, rope sheaves, sproc-ket wheels, etc., and adapted for continuous, heavy duty in any surroundings. It requires no oiling or attention on the fric-

tion mechanism: is powerful and long-lived. Catalog E for Details

The Edgemont Machine Co.

2700 National Avenue

DAYTON, OHIO, U. S. A.

# Power Transmitting Machinery



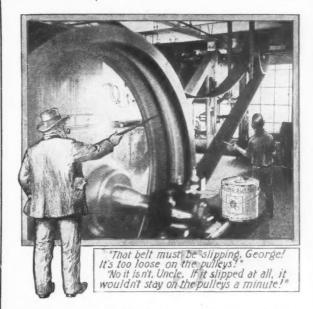
Heavy bearings, drop hangers and post hangers.

Machine moulded gears and pulleys.

Friction clutches, rope Heavy Pillow Block drives and chain drives.

#### H. W. CALDWELL & SON CO.

Elevating, Conveying and Power Transmitting Machinery 17th Street & Western Avenue, Chicago, Ill. 50 Church St., New York. 709 Main St., Dallas, Texas.



THE new Superintendent was different. For the first few days he just walked through the plant and looked at things. Down in the engine room he took the speed of the engine. Up in the shop he took the speed of the main shaft. Then he did some These are the figures.

Driving pulley 8 feet diameter. Speed 80 rev. per minute.
Driven pulley 4 feet diameter.
Speed should be 160 rev. per minute.
Speed actually 155 rev. per minute.

5 rev. per minute.

 $5 \div 160 = 3\%$  approximately.

8 feet  $\times$  3.1416  $\times$  80 rev. per minute = about 2000 feet per minute the belt travels. 3% of 2000 feet = 60 feet per minute LOST. Pulley centers at 20 feet, so belt length approx.

60 feet.

This meant that once every minute his belt was useless, for the loss in feet per minute due to slipping was more than the length of the belt itself!

In a ten-hour day this loss would be 36,000 feet, so that every day the engine had to give that belt a free ride of nearly 7 miles! And the firm paid the bills at the coal pile and machines, at the bearings, pulleys and in the belt itself. It didn't look right.

The plant had over one hundred belts. If they all slipped, the firm must be losing hundreds of dollars a year in power, time and equipment which might better be saved.

The new Superintendent never did things on impulse, or merely on someone else's say-so. Back in his experience he had used CLING-SURFACE, the treatment which PREVENTS SLIPPING, and allows the usual drive to be run easy or slack under full load. He knew that it makes constant tension unnecessary, preserves and makes the belts thoroughly pliable and waterproof; that it is not sticky, contains no rosin or anything harmful, and is safe, easy and economical to use

So he had every belt treated, and the effect was seen at once. His slipping stopped, he had more and steadier power, and not a belt has been taken up since that time.

This is fact; we can prove it on your drives to YOUR satisfaction. Just ask for THE PLAN 10,000 firms have found successful.

And remember, use CLING-SURFACE and you won't need belt dressings.



Cling-Surface Company 1018 Niagara St Buffalo N Y

New York Chicago Memphis Denver Boston St Louis Atlanta Toronto Etc

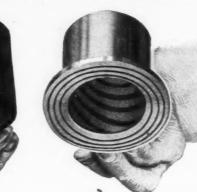
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# There Are Two Different Kinds of Genuine Graphited Oil-Less Bushings

#### **NIGRUM**

(Impregnated Hard Wood) Oil-Less Bushings are made of se-lected hard wood, thor-oughly seasoned and then thoroughly impregnated with our special lubricating com-pound.

This bushing not only runs efficiently and lasts indefinitely without oiling or any attention whatever, but it is light in weight, small in bulk and has the additional advantage of absorbing grit and dust without harm to itself, thus prolonging its own service life as well as that of the shafting.



#### **BOUND BROOK**

(Graphite-and-Bronze) Oil-Less Bushings are made of finest phosphor bearing of finest phosphor bearing bronze, so constructed as to retain a sufficient quantity of our specially prepared lubricating graphite to keep them lubricated in service, even if neglected.

They are used as an insurance against neglect of machine parts that are inaccessible and therefore difficult or impossible to keep properly lubricated.

Oiling will not hurt these troubleless bushings, but they will give efficient service even if overlooked, and as the life of a machine is no longer than the life of its bushings, the proper installation of BOUND BROOK Bushings gives assurance of long life and increased efficiency.

LEADING MANUFACTURERS throughout the country, as well as the U. S. and foreign governments, have endorsed these bushings by using them in hundreds of different kinds

We should be glad to advise with you concerning your own particular bushing problems

All Genuine Graphited Oil-Less Bushings Have Always Been Made at Bound Brook, U. S. A.

of machinery, from Armored Cars, Battleplanes and Naval Vessels to Mill and Factory Machinery, Windmills, Escalators, Gas Engines, Elevators, Mining Machinery, etc., etc.

TEN MILLION BUSHINGS per annum is the capacity of our plants at Bound Brook and Lincoln, New Jersey, where we have every facility for the manufacture of highest quality bushings in large quantities on short notice. Prompt, dependable deliveries are, therefore, assured.

#### BOUND BROOK OIL-LESS BEARING CO.

Specialists in the manufacture of Oil-Less Bushings for more than a Third of a Century

**BOUND BROOK** 

**NEW JERSEY** 

# No Power Swallowed Up In CHAPMAN BEARINGS

Every bit of power is directly available for the work, in shops where Chapman Bearings are used on shaft transmission. When we add that the average saving of power

reported is 20 per cent, you can get an idea how much your friction loss is—aside from the waste of time and oil for upkeep, eliminated along with the friction, if you are not using

#### CHAPMAN BEARINGS



We suggest that you write for our Bulletin No. 106, which explains the why and wherefore of Chapman saving.

#### TRANSMISSION BALL BEARING CO., Inc.

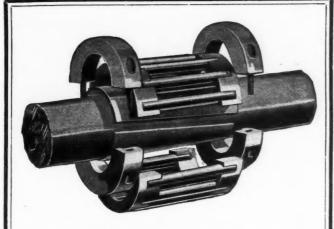
1050 Military Road

Buffalo, N. Y.

**BRANCH OFFICES** 

NEW YORK, Room 101, 30 Church Street PHILADELPHIA, Bourse Building TORONTO, ONT., Chapman Double Bearing Co., Ltd. 339-351 Sorauren Avenue





A letter is interesting to the extent that it either says something worth while or reflects personality—the personality of the writer.

A piece of machinery is serviceable to the extent to which it does something well—and is the embodiment of the character of the maker.

Conscientious workmanship and sound materials, as well as a regard for performance, efficiency and upkeep, are reflected in "Sells" Roller Bearings.

Take one point at a time—say the rollers. There is a lot of good judgment in the selection of rollers instead of balls. The greater bearing surface of the rollers will reduce the friction, lessen the amount of attention and lubrication required, and greatly decrease the wear on the shafting. Ball bearings wear grooves in the retainers, rollers do not, but as a further protection against wear in Sells Roller Bearings, there is a hard metal sleeve to protect the shaft.

These are the simple devices that help reduce the friction from 25 to 50 per cent over ordinary bearings. Just look at the picture. Did you ever see a better combination of common sense and mechanical simplicity?

Call me up or write to me and I'll explain the "Sells" principles as fully as you wish.

Yours for less friction,

John Seller Manager.

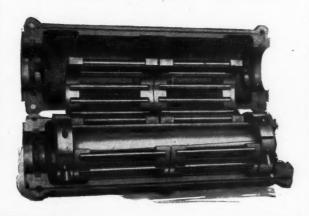
#### Royersford Foundry & Machine Co.

54 North Fifth Street

Philadelphia, Pa.

"Sells" Line Shaft Bearings, "Sells" Commercial Roller Bearings, Babbitted Ring Oil Bearings, Shaft Hangers, Collars and Couplings, Punches and Dies, Punching and Shearing Machines, Sensitive Drill Presses, Foot Presses, Grinding and Polishing Machines, Tumbling Barrels, "Rollerine"—the ball and roller bearing lubricant.

## Old Reliable "Sells"



# "NORMA" BALL BEARINGS

(Patented)

Bearing failure means machine failure. Resultant losses lie not alone in the cost of repairs, but in the interrupted service, the loss of output—and the loss of your prestige as a manufacturer of a dependable machine. Can you afford to risk these losses by using any but bearings of proved reliability?



We will welcome an opportunity to explain to you the factors which lie at the root of "NORMA" dependability—the open type and separable construction—the rigid mounting of both races—the unequaled precision—the silent-running, vibrationless qualities. We can probably help you to better bearing service, higher bearing serviceability. Then—

Let it be said of your machine, "It is "NORMA" equipped."

#### THE NORMA COMPANY OF AMERICA

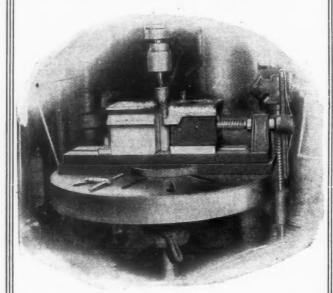
1790 BROADWAY

NEW YORK

Ball, Roller, Thrust, Combination Bearings

# SAVE

Those 30 Minutes That Your Men Waste Daily In Setting Up Work



WITH THE

On any machine with a horizontal table, such as a On any machine with a horizontal table, such as a drill press, miller or shaper, this vise clamps instantly work of any shape, and in any position desired. No parallel strips, V-blocks, clamps or other similar pieces are needed. The revolving four-sided rear jaw adapts itself to any form or position of set-up, vertical, horizontal or at odd angles. Irregular shapes are gripped with the same speed by means of auxiliary jaws means of auxiliary jaws.

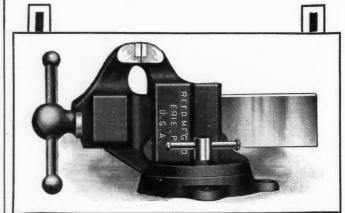
That's why the Utility TIME-SAVING Vise will save all the time your machinists waste in hunting for, and adjusting the many clamps and fixtures ordinarily required for setting up—why it will get 30 to 60 more minutes of *production* out of those men and their machines every working day.

On the machine that must handle a variety of work, the Utility TIME-SAVING Vise will pay back its cost in a few weeks. You can prove that fact in your own shop at our expense. The coupon will bring full details of our FREE TRIAL OFFER. Clip and mail the coupon-now.

THE BROWN ENGINEERING CO., 133 N. Third St., Reading, Pa.

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#### Choosing A Vise

Here are some practical hints valuable to vise purchasers. Get one size larger vise than would ordinarily be required for the work, as the larger vise will not spring away from a blow heavy enough to work the material.

#### REED VISES

should invariably be chosen, as they have a "limit gage" accuracy, are machine fin-ished and have wide bearing surfaces offering greater wearing resistance. When buying vises use our Catalogue H

as a reference book.

### Reed Manufacturing Co.

ERIE, PENNSYLVANIA, U. S. A.

W & B TOOL Cases Prolong TOOL Life Tool life is short at best—good care pro-longs it. We have done our bit for your tools in providing a good case reasonable figure. Write for catalog today **WEDELL & BOERS** 157 Jefferson Ave. Michigan Detroit,



First-class Tools and Prompt Deliveries

REIFF & NESTOR, Lykens, Pa.

#### Quick Operating Lever Vise

This Vise is well adapted ing or drilling is short and a large number of pieces are to be handled quickly.

Send for Circular.

The Carter &

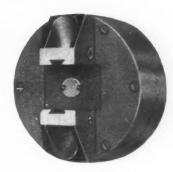
Hakes Company Sterling Pl., Winsted, Ct.



# AIR CHUCKS? FINE!

This operator enthusiastically reports a 25 per cent increase in production since she has had the "Hannifin." Other reports vary from 20 to 100 per cent, but all agree that Hannifin

Air Chucks are fine—easy to operate, thoroughly reliable, simple and durable.



The best test is a tryout. Send for one on trial.

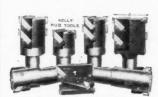
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#### KELLY PRODUCTION TOOLS



FOR CYLINDERS CRANKCASES, CONNECTING RODS, AUTO PARTS, ETC.

They "ADJUST"

We make DELIVERIES in 1 to 10 days Write for the catalog G-3

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KELLY 'Multiple' Operations

# TRADE \*PRODUCTION

MARK

Swivel Milling Vise (Graduated)

Width of Jaw..5 in. Depth of Jaw.1% in. Vise opens....3 in. Weight......45 lbs.

\$22.00

**NEW JERSEY MACHINERY EXCHANGE** NEWARK, N. J.

#### Save Your Taps with the

"WEAR-EVER" TAP CHUCK

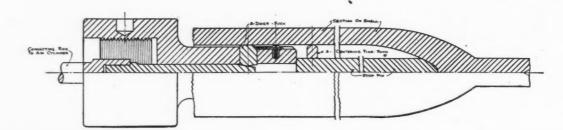
> With the Wear-Ever Tap Chuck the tap runs true and breakage is reduced to a minimum. Use it like a socket and stick it in the spindle like a drill. It takes but a mo-

ment to change taps-no expert required, no screws to adjust, no setting for various size taps—just a single piece of metal, hardened, but it-will outwear any number of friction taps and—the price is low. Try it and prove it.

SCULLY-JONES & CO.

647 Railway Exchange Bldg.

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# **AMERICAN SHELLS**

ARE NOW BEING MADE BY

# M. E. C. Short Expanding Mandrels

AIR-OPERATED

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# Manufacturers Equipment Co.

175-179 N. Jefferson St., Chicago, U. S. A.

AGENT FOR CENTRAL AND EASTERN STATES AND CANADA:
J. R. Stone Tool & Supply Co., Goebel Bldg., Detroit, Mich.
FOREIGN AGENTS: Burton, Griffiths & Co., Ltd., Ludgate, Ludgate,
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Hundreds of makers of American shells have found M.E.C. Mandrels reliable, durable and efficient. They are particularly adapted for rough and finish turning. Compensating mandrel furnished for cutting rough shell forgings to length and for centering.

In the past three years M.E.C. Chucks and Mandrels have been extensively and profitably used not only in munition work, but in automobile and gas engine manufactories as well.

If you are in the market for labor-saving devices of this kind, by all means get in touch with us. Tell us your problems. We know we can help you. Write today for our latest catalog describing M.E.C. Labor Saving Devices.



### Again the Woodstock Tapping Chuck "Brings Home the Bacon"

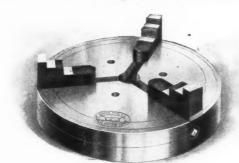
The Philadelphia Scoop Co. never knew trouble-proof tapping until they tried the "Woodstock." Now any tapping job is plain sailing, with broken taps as scarce as they formerly were numerous. Tapping scale pans is the job, the operator using a ¼ inch and a ¾ inch chuck for the work. The "Woodstock" is a fixture in this plant because of its speed, accuracy and economy—and we could tell you of hundreds of other shops where this same experience applies. The shop that uses the Woodstock Tapping Chuck knows tapping satisfaction. Why not yours?

Try one for 30 days free and see what it can do.

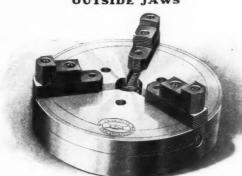
PETER BROTHERS MFG. CO., 135 Railroad Ave., Algonquin, Ill.

# UNION

Makers of a Complete Line of Chucks



OUTSIDE JAWS



REVERSIBLE JAWS

# **Combination Lathe Chucks**

-PINION SCREW TYPE-

UNIVERSAL
INDEPENDENT
ECCENTRIC
CONCENTRIC

The Union Combination Chuck as illustrated is made with solid or reversible jaws, also with four jaws. This type (Pinion Screw) of chuck makes a very accurate and quick acting chuck. Especially adapted for tool room, fine manufacturing, or experimental work.

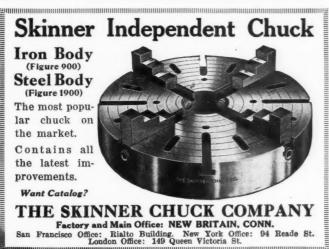
## UNION MANUFACTURING CO.

**NEW BRITAIN** 

CONN., U.S. A.

NEW YORK OFFICE: 26 CORTLANDT STREET







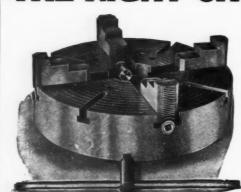
# For Rapid Grinding Use "D & W" Magnetic Chucks

In fact, for planing, shaping and milling as well; the "D & W" Magnetic Chuck lends itself most profitably to a wide range of uses. No clamping or bolting—place the work in position, throw on the switch and go ahead. When the job is finished, another turn of the switch releases the work

Ask for Bulletin 10-M

D & W FUSE COMPANY PROVIDENCE, R. I.

### THE RIGHT CHUCK FOR HEAVY TURNING



This Horton All-Steel Heavy Duty Chuck, made with extra large screw, double thrust bearings and long, wide jaws, possesses strength, power and endurance equal to the heaviest demands. In its thoroughness of construction it's a typical example of Horton standards and a true representative of a specialized line that provides a chuck for every purpose. Use Hortons in your plant and you'll be sure of chuck service par excellence.

Catalog lists entire line.

THE E. HORTON & SON CO. WINDSOR LOCKS



the Tool-Steel Bearing

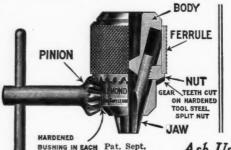


The Chuck That
Never Slips.

The More
You Crowd it,
The Tighter
It Grips.

NARRAGANSETT MACHINE CO. PROVIDENCE, R. I., U. S. A.

#### **ALMOND CHUCKS**



POWERFUL ACCURATE DURABLE

COST LESS TO MAINTAIN

Ask Us Why

T. R. ALMOND MANUFACTURING CO.
2 MAPLE AVENUE
LONDON OFFICE: 8 White Street, Moorfields, London, E. C.

#### TIME TO LOOSEN UP

A chuck must grip tight, up to the limit of its driving capacity; but when the tool binds or strikes bottom is the time to loosen up. The Bicknell-Thomas Friction Chuck does this automatically—that is why there are no broken taps where Bicknell-Thomas Chucks are used. It is especially adapted for blind tapping and on machines having relatively small center distance between holes.

5 Sizes
From ½" to 1"
Capacity



Write for details.



#### Another Tap PING! Broken-**Another Casting**



And the operator must get a new tap from the toolroom before the old one is worn out.

Scrapped

TAKE THE PING out of TAPPING with the

# "Double-Gripp" Tapping Chuck

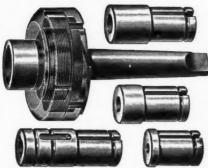
The SAFETY FRICTION does it. Only the "DOUBLE-GRIPP" has it.

Write for our new circular to-day. It's a yard long and tells all about the Safety Friction and the jaws that made the "Double-Gripp" famous.

WM. L. PROCUNIER

CHICAGO, U.S.A. 549 Washington Blvd.,

# The Safety Drill and Tap Holder



is the only attachment for the pur-pose that gives universal satisfaction and is un-equaled in efficiency, conveni-ence, rapidity, accuracy and simplicity. Nothing to break or get out of order. Made in 4 sizes, covering from 0 to 2½ inches diameter.

The Beaman & Smith Co. PROVIDENCE Rhode Island



#### Flynn Offset Boring Heads

This chuck, which has a micrometer adjustment and large range, is strong, durable and easily operated.

Write for free circular

J. M. WATERSTON, 77 Woodward Ave., DETROIT, MICH.

#### 1874 TRUMP DRILL CHUCK 1917



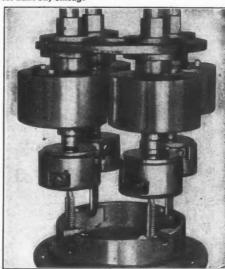
We have been making it for 43 years; it is still the BIG Chuck at the SMALL price; for Straight or Taper Shank Drills.

No. 1 0 to 1/8" No. 3 0 to %" No. 2 0 to 1/4 Write for prices and particulars TRUMP BROS. MACHINE CO. Wilmington, Del.

# LABORATORY

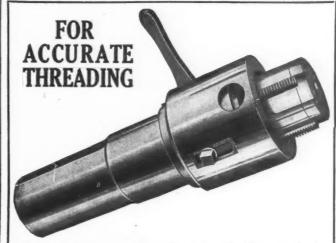
39 Cortlandt St., New York 136 West Lake St., Chicago

# ERRINGTON MULTIPLE



ERRINGTON TAPPERS reduce tapping the minimum, insure exact duplication of work, are simple, compact and long wearing. Taps up to 5%" can be used with only 2¼" between centers, and larger sizes are proportionately compact. In the job shown in the engraving 2560 3%" holes were drilled and tapped in malleable iron gear cases in eight hours. Let us figure on your line of terming in eight hours. Let us figure on your line of tapping.

Errington Opening Die Heads; Collapsing Taps; Opening Stud-Setters; Friction, Stud, Nut and Screw Setters, etc.



On tapping operations in general, the greatest damper on accurate production is the slow, uncertain backing out of the tap. Use

and tapping can be made your most productive operation. Never any spoiled threads, and the work is done in half the time required by solid taps. Victor Taps are adjustable for size and spring tension, will cut large and small threads, and stand the strains of heavy cutting. Sizes from 1 to 12 inches, either straight or tapered shank. Circular?

#### VICTOR TOOL CO.

WAYNESBORO, PA.



# Quick Control of a Giant Grip

Experienced men readily see that only the combination of these two things-easy control and strong grip—can bring chucking to a maximum point of profit. An immovable grip to assure accuracy; quick control to utilize the operator's time.

# **SWEETLAND** Lathe Chucks

hold work against all the power that any machine can deliver, and avoid the fractures, distortion and other inaccuracies that lead to the scrap pile.

With this gripping power easily exerted and controlled—with the quick and ready adaptability to work of differing shapes and requirements, Sweetland Chucks are a means of satisfactory chucking that shows on the profit sheets.

The special features that bring about these and other individual advantages are shown in detail in the booklet, "Chucking for Profit." Ask for it.

## HOGGSON & PETTIS MFG. CO.

**NEW HAVEN** 

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# **Drill Chucks** Lathe Chucks **Centering Chucks Portable** Face Plate Jaws

Steel Bodies Iron Bodies

Many Styles and Sizes. All Designed for Hard and Exacting Service.

Catalog Free

**HARTFORD** CONN., U. S. A.

#### If You want the best Lathe or Drill Chucks—buy Westcott's

Little Giant Auxiliary Screw Drill Chucks, Little Giant Double Grip Drill Chucks, Little Giant Improved Drill Chucks, Oneida Drill Chucks, Spur Geared Scroll Combination Lathe Chucks, Scroll Combination Lathe Chucks, Spur Geared Scroll Universal Lathe Chucks Little Little Chucks Little Little Chucks Little Ch

Chucks, IXL Independent Lathe Chucks, Cutting-off

Strongest Grip, Greatest Capacity Great Durability and Accuracy WESTCOTT CHUCK CO.

ONEIDA, N. Y., U. S. A. Ask for catalogue



Spur Geared Scroll Combination Lathe Chuck

**Solid Steel Rings** Reinforce these Independent Lathe Chucks

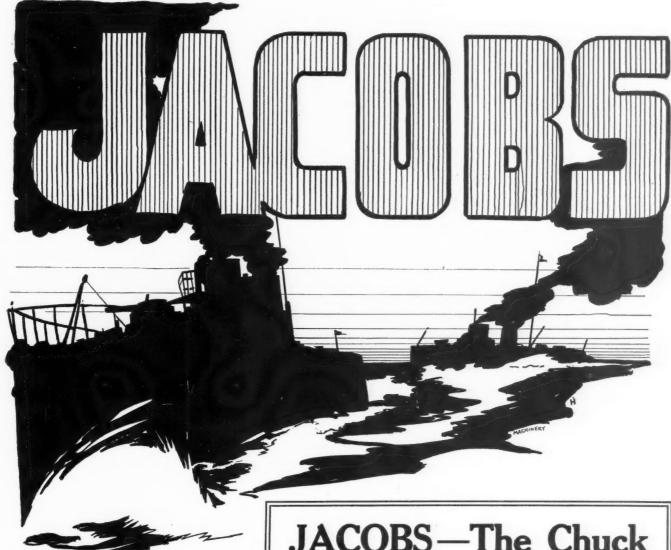


making themstrong where other chucks are weak, providing for tensile stresses and screw thrusts, insuring greater durability and better service.



Made with three distinct grips which can be applied at the same time when necessary—a positive gripping chuck—all sizes up to 2 inches. Catalog?

Oneida National Chuck Co. N. Y., U. S. A. ONEIDA



#### **FIVE SIZES**

No. 1—0 to 13-64" No. 2—0 to 21-64" No. 3—0 to 17-32" No. 4—1-16" to 3-4" No. 5—3-8" to 1"

# JACOBS—The Chuck

Ever since the Jacobs Improved Drill Chuck was first marketed, in 1902, it has held its place as the leader in this field. Thousands have been sold—all over the world. And this chuck is more popular today—selling in greater numbers—than ever before.

The Jacobs Improved Chuck combines convenience, efficiency, accuracy and durability. What more can you ask?





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#### Instead of a Handful Count a Thousand

THAT is what it means to have your counting done with a

# NATIONAL COUNTING MACHINE

T gives you a mechanically accurate count—not a brain-wearied result which may or may not be right-usually not.

The human brain cannot compete either in speed or accuracy with the National Counting Machine, because the machine doesn't get tired-the brain does.

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Distributors for the National Scale Co.

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need open the drawer and Made of plain or quartered oak or leatherette covered. Highly finished. Specially designed drawers, strong and perfectly fitted, some with felt. Drawer pulls—specially designed, practical and efficient. Space saving flush-ring. Every chest quaranteed to give perfect satisfaction to meet with your entire approval or money back. Write for our Catalog and Prices of Nineteen Styles and Sizes. If there isn t a "Union Dealer near you, get our Special Offer.



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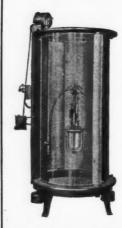
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For Eye Protection of All Those who do Work that Might Cause Eye Injuries.

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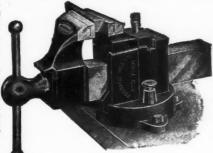
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with self-adjusting jaw that is as strong and durable as any solid jaw, and a Swivel Bottom that gives any desired adjustment to right or left, and is solid and firm at any angle. We make all sorts of good vises, and have been leaders in this line for forty years.



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though he bends close over his work. He has no fear that flying dust or bits of a brasive will lodge in his eyes, so he keeps them at a normal focus and centers all his attention on the task in hand.

The UNIVERSAL EYE GUARD insures this freedom, and it costs his employers only \$2.00—money well invested.

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IN order to illustrate the effective use of the pencil as a medium of expression for engineering and technical work we shall offer \$100 for the best drawings or designs.

First prize \$50 Second prize \$20 Third prize \$10

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A special box of VENUS Drawing Pencils will be sent to all contestants awarded honorable mention.

#### CONDITIONS:

- 1. The drawing submitted must illustrate pencil work.
- Name and degree of whatever pencil is utilized, and name and address of sender must be written on the back of the drawing.
- All drawings submitted are to become the property of the American Lead Pencil Co. and none will be returned.
- 4. Contest closes Sept. 10, 1917.
- 5. Important—The drawing must relate to some one of the following branches of engineering: (a) mechanical, (b) electrical, (c) civil, (d) automotive, (e) military, (f) marine or naval.

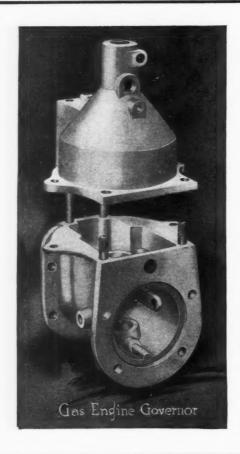
Mr. H. E. Cleland, Manager of the Service Department of the McGraw-Hill Publishing Co., has kindly consented to act as judge in this contest.

Awards will be based on originality, attractiveness and strength of design. In case of a tie, prizes will be duplicated.

This offer is made by the manufacturers of VENUS PERFECT PENCILS, which pencils are available in 17 degrees from 6B softest to 9H hardest, and also hard and medium copying. The winners' names will be published in a later issue of this publication.

Send drawings to

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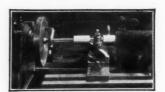
#### Accuracy Guaranteed

The Gas Engine Governor parts shown above are difficult die-castings. Their production in quantities strictly in accordance with specifications requires skill, experience and careful supervision and inspection. The parts must be solid and extremely accurate at a number of points—the finish must be perfect. We cite this merely as an example out of many hundreds of jobs we are turning out with complete satisfaction to our customers.

Acme Die-Casting Service is thoroughly dependable, the workmanship and materials measure up fully to the exacting standards of manufacturers of high grade products. This service awaits your order.



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are marshalled the machines of production, straining to speed up their output.

Every minute that can be saved adds to the total supplies which can be turned out. If 2 to 10 minutes could be clipped off, every time the job on a lathe is changed, from two hours to a full day would be added to the output of each lathe each week.

How many lathes have you? Even two hours a week totals nearly two working weeks in a year.

Nicholson Expanding Mandrels are *instantly* adaptable to any sized hole from ½" to 7", round or square, even or tapered. They can be centered immediately and quickly removed. The outstanding time saver of the machine shop.

This is a backed-up statement. We will lend you one for thirty days' test without any obligation. The full charges will be ours.

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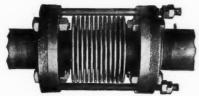
#### Nicholson Expanding M



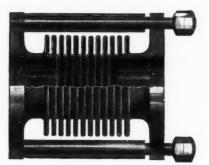
ANDREL

# The Nuttall

One Piece Expansion Joint



View of Joint Installed



Cross Sectional View

Here is the solution for pipe line expansion difficulties.

The Nuttall Expansion Joint is made in one piece, machined to extremely close dimensions from a solid, hammer-forged steel blank, then oil treated. Note the illustration showing the interior construction.

The joint is strong, non-leaking and bolts solidly into the line. Breakage from extreme expansion or contraction is cared for by an arrangement of limiting bolts equipped with sleeves. A sliding sleeve on the inside minimizes friction and helps support internal strain. In actual tests it proved itself fifty times more durable than ordinary expansion joints. It is made for all standard sizes of pipe and to accommodate high and low pressures, allowing a total movement of  $2^{\prime\prime}$  on the high and  $5/8^{\prime\prime}$  on the low pressure.

It retains all desirable features of other expansion joints but eliminates the objectionable points.

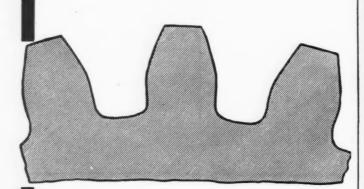
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# NUTTAL

#### "Can't Afford" to Make Their Own **Gray & Prior Universal Joints** Are Both Better and Cheaper That's the verdict of the manager of Deck Bros., Buffalo, N. Y., manufacturers of polishing machines. This concern used to make their own universal joints for transmitting power from the lineshaft to the machine. But that was before they knew of Gray & Prior Universal Joints. Once they tried G & P Joints they discontinued manufacturing their own. Today they have over 4000 G & P Joints in use and not a single case of trouble has developed. G & P Universal Joint parts are strong drop forgings with wearing surfaces carefully casehardened. No play to col-lect dirt, generate friction and absorb power. Can you afford to make your own universal joints? We doubt it. Write for descriptive literature The GRAY & PRIOR MACHINE COMPANY 38 SUFFIELD ST. HARTFORD, CONN.

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is the result of specialized knowledge and specialized equipment such as is used in the production of





We furnish complete gears designed to give maximum service under your particular conditions or we cut your blanks

20 years of experience in the manufacturing of better gearing exclusively has placed us in a position to give you positively the best gearing service to be found in the industry.

according to your specifications.

Ask our Engineering Department for suggestions as to your gearing.

# THE VAN DORN & DURYON COMPANY

Gear Specialists

Cleveland

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# Don't Waste Your Men's Energy

THE hum of the shop is music in the ears of a good mechanic—but the jarring clash of metal on metal gears soon tires his nerves.

Controlling tired nerves consumes a lot of energy that would otherwise go to the work, and the quality and quantity of production suffers proportionately.

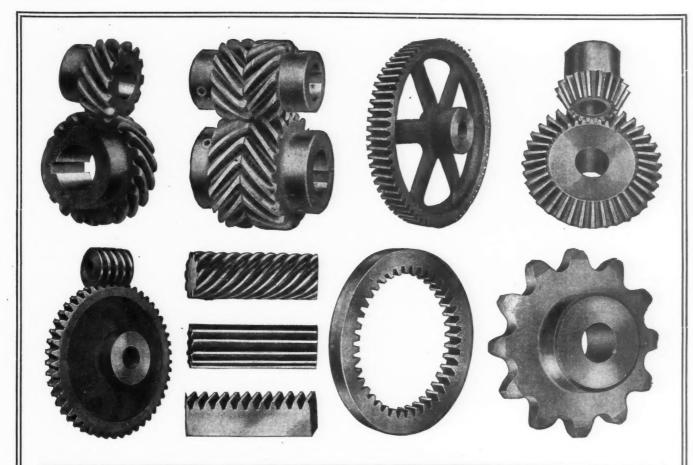
# PEERLESS RAWHIDE GEARS AND PINIONS

increase the output at least 10 per cent on this count alone, mesh perfectly with metal gears and wear well under any service.

We cut gears of all kinds. Send us your specifications.

THE HORSBURGH & SCOTT CO.
CLEVELAND OHIO, U.S. A





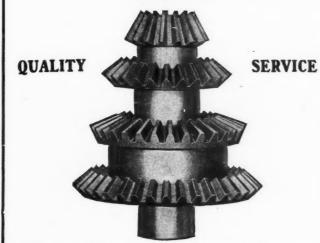
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BOSTON GEAR WORKS, NORFOLK DOWNS (Quincy) MASS.

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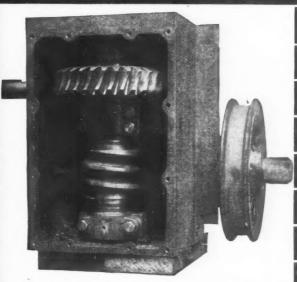
May we have an opportunity to quote on your gear requirements?

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INCORPORATED

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# HINDLEY WORM GEARS



Where gearing of close accuracy or great power—or both—is required, discriminating engineers specify Hindley Gears. Adapted for ignition mechanisms, mine haulage, driving automobile trucks—for any service where safety and efficiency depend on reliable gearing. Try us on your next order.

HINDLEY GEAR COMPANY

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LL gears wear out eventually. Economically speaking, therefore, the vital consideration in buying gears is to buy gears that will give the longest service.

Grant Gears are durable even under severe usage. They are made from selected materials in a plant equipped to turn out quality gears. Grant carries in stock Iron Cut Gears, Brass Cut Gears, Cast Gears, and makes gears to order, all sizes from 1/4" to 6' diameter, any face. from 1/4" Reasonable prices, prompt deliveries and gears you can depend upon.

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#### Equipped to Handle All Kinds of Special Machine Work

We make the unusual machinery that other shops are not now equipped to handle.

> Nothing too large for our equipment

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Special facilities for cutting Worm, Spiral, Miter, Internal and Elliptical Gear Wheels

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#### ONE OF OUR GREAT SPECIALTIES HEAVY DUTY HARDENED GEARS

For General Use Our Before

Tractor Truck and Auto Drives For Transmissions and Differentials

The IXL

#### FOOTE BROS. GEAR & MACHINE CO.

Manufacturers of all kinds of Cut Gears
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Gear Service You Can Depend On

Complete satisfaction in any gearing emergency is the service we give —perfect gears of enduring quality in minimum t im e. Our whole organization is keyed to this form of service. Send your next gearing S.O.S. to us and watch the clock.





SPROCKETS WORMS, ETC. manufactured true to

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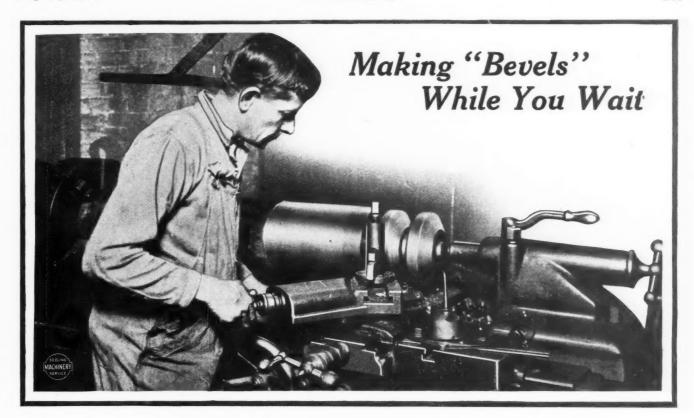
We have a modern shop equipped with modern automatic machinery especially suitable for making gears, etc., complete, or cutting the teeth in your blanks. We have had years of experience in this line of work, and can fill your orders promptly, accurately and at the right price.

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We Urgently Request You to Give Us a Trial

WOBURN GEAR WORKS, Woburn, Mass.





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"Every Second Counts"

Put Your Gear Troubles up to "Phillie Gear."

# PHILADELPHIA GEARS

The reason that "Phillie Gear" can turn out an order of bevel gears in such short time is due not only to shop organization, good equipment and well-trained men, but also to the stocking of a great many sizes of the finest of forged steel bars. This stock is conveniently arranged and the first procedure in putting through a batch of "bevels" is to pick out a forged bar the size required, deliver it quickly to the machine room, and presto, it takes the form of bevel gear blanks before your very eyes.

It is doing the desired thing just a little better and in better time than the other fellow that has given "Phillie Gear" and his organization their present reputation. Why not try Philadelphia Gear Service?



# **NEW PROCESS GEARS**

#### Use Them Anywhere

When you want gears that are absolutely dependable, that are uniformly good, that will stand up to severe service without fail, choose NEW PROCESS GEARS and you can't go wrong.

We make them in all styles—spur, bevel and spiral, in steel, iron or brass, large or small—and will supply any quantity, one gear or ten thousand.

Send us your blueprints for quotation, and you'll wonder why you have been cutting your own gears for so long.



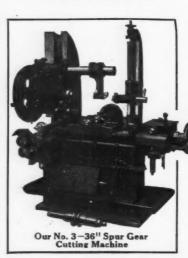
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We not only make good gears, but we make good gears at low cost. One trial order is all we ask.

# NEWARK

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Accurate, productive, durable machines; built by skilled labor; materials carefully selected; automatic in operation.

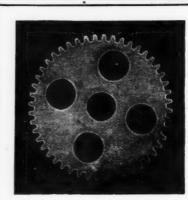
Buy them for gear cutting, for cutting sprockets, ratchet wheels, circular saw teeth and other similar work. Write for Catalog.

#### NEWARK GEAR CUTTING MACHINE CO.

Gear Specialists

69 Prospect St.

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in our

Gear Cutting Department

(Cut is full size)

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of every description in any material SPUR, SPIRAL, HELICAL, INTERNAL, WORM

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High-speed, motor-driven shears, presses, punches, etc., demand extraordinary service from the gears used with them. Aside from the wear induced by high-speed operation itself, the intermittent work such machines perform—running free one moment and laboring under full load the next—reacts violently and destructively on the gear teeth and unless provided against rapidly leads to wear and in many cases to costly breakage of the gears.

# NEW PROCESS NOISELESS PINIONS

used in such service offer an ideal remedy to both these conditions.

Cut from rawhide, especially cured by exclusive process for gear requirements, NEW PROCESS NOISELESS PINIONS have a resiliency in service that metal gears, no matter how well oiled, greased or lubricated, can never acquire. This characteristic resiliency acts as a cushion to absorb the sudden shocks of heavy service and will protect the whole gear train against crystallization and tooth fracture.

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They are cut to suit every motor drive requirement. Ask for our booklet—*Noiseless Gear Driving*. It is worth a thorough reading.





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gears of the highest grade at prices as low as quality permits.

It also guarantees prompt delivery. We furnish gears for driving all manner of delicate mechanisms, and for hard, heavy service in the industrial field. We have never lost a customer. Let us show you why.

Try us also for Automatic Screw Machine products up to 51/2" diameter.

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Made from open-hearth steel of any carbon, nickel steel, chrome-nickel steel and chrome vanadium—any size, any amount.

Blanks that will enable you to guarantee, absolutely, gear quality in any machine you make. We've been forging gear blanks for a long time and have saved money for concerns the country over. Let us show you what we can do for you.

Send your specifications today.

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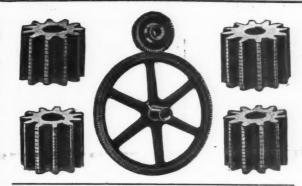
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Good gears—either metal or rawhide; gears absolutely as per specifications—material, workmanship, delivery; gears of standard quality—for uniform service—made by

STAHL



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Metal Gears—Spurs up to 60" dia., 2 D. P.; Bevels up to 24" dia., 13/4 D. P.; Spirals and Herringbone gears up to 19" dia., 3 D. P.; Worms up to 18" dia., 3 D.P.; Racks 8' long, 4 D. P. Rawhide Gears—any requirement up to 15" dia., 2 D. P.

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Good tools are essential regardless of the skill of the machinist. With Union Tools every element of guesswork can be eliminated, less work will be spoiled, production naturally can be greatly increased. Union Tools brace up standards unconsciously—and the line is complete; good tools for every purpose. Send for particulars.

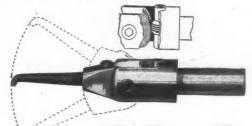
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Complete drives with housing ready for power

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For milling and boring you need accurate Spacing Washers and the E-Z-Set Boring Tool.

We have both—the Washers three, four, five and six thousandths thick, \$3.00 per 100 (25 of each). The E-Z-Set Boring Tool in three standard sizes, with provision for rigid clamping and worm actuated adjustment to secure fine variations. Adapted for screw machines, lathes, drill presses, etc., a time saver on tool work and in general manufacturing.

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There are two ways to select tools—try them, or buy from a house of established reputation. Our reputation is second to none. We carry in stock a complete line of Taps, Dies and Screw Plates, and our name on a tool is sufficient guarantee for anyone who knows us. We guarantee our tools and our tools guarantee repeat orders. Send us your next. Complete catalog on request.





BAY STATE TAP & DIE COMPANY MANSFIELD MASSACHUSETTS, U. S. A.

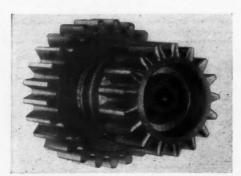
REPRESENTATIVES FOR ENGLAND: Geo. W. Goodchild & Macnab, 56-58 Eagle St., Southampton Row, London, W. C. REPRESENTATIVES FOR SCANDINAVIA: Wilh. Sonesson & Co., Ltd., Malmo, Sweden.





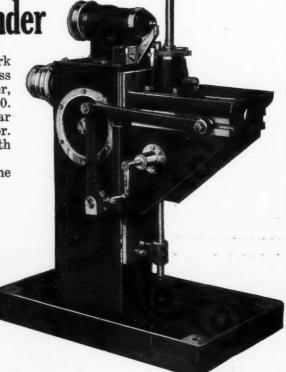
The Cross Gear Tooth Rounder

Rounds the teeth of sliding meshing gears; does its work accurately and sets a fast pace for speed. The Cross Tooth Rounder handles spur gears up to 30" diameter, any pitch from 2 to 20, any number of teeth from 8 to 50. It rounded the 5 pitch, 17 tooth chrome nickel steel gear we are showing in one minute ten seconds, floor to floor. If you make sliding gears you need the Cross Tooth Rounding Machine to give them the finishing touch. The machine has other uses-removes burrs left by the cutter, takes off sharp corners left by the hob.



Bulletin is interesting.

Tell us where to send it.



CHARLES H. WALKER, Detroit, Michigan Corner 14th and Grand River Avenues

Alfred Herbert, Inc., 30 Church St., New York City, Sales Agents for the Eastern States. Alfred Herbert, Inc., Coventry, England, Sales Agents for Great Britain, Allied Machinery Co. of America, Turin, Paria, Zurich, Petrograd, Sales Agents for Europe.

# BRONZE WORM GEARS

# For Severe Service and High Efficiency

Gear blanks must be of a uniform hardness throughout, not only around the periphery, but also through the section of the teeth. Although the finished blank is of quite uniform cross section, the cast in the mold is not so, because of the heavy headers used.

At these points a much heavier cross section sets up a very much more open grain when sand cast in the regular way, hence when the blanks are hobbed the softer portion causes a different pitch to be generated. Furthermore, these heavy worm gear sections set up a very much coarser grain in the center near the root of the tooth, athough the metal at the tip of the tooth is a very fine grain.

It has always been recognized that a spur gear was improved by casting the teeth in since the "skin" was deep enough to leave a fine uniform grain around the tooth sides after cutting. This fine grain therefore has always been recognized as an improvement. However, on worm gears it is not common to cast the teeth in, hence we have to carry the chilling effect deeper than sand will do ordinarily.

Our chill cast gear blanks have this fine grain carried well past the root of the teeth of even the largest worm wheels.

The beneficial results of the chilling process very largely contributed to the recent success of worm gearing of high efficiency.

A very uniform gear can be generated which is much more quiet and which, since the compressive strength is also increased, will retain its original tooth form.

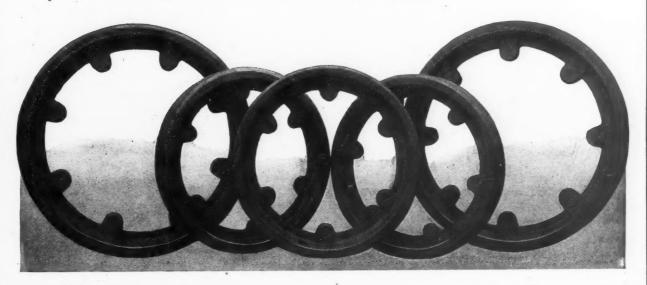
The machining qualities are improved by our chilling process which does not give an objectionably hard skin, but is a process of cooling the mass of metal quickly and evenly throughout, producing a fine uniform grain to the desired depth.

We have carefully studied the English as well as the American practice in worm gearing, and are familiar with the alloys giving satisfaction.

This is a specialty which we have developed to a very high degree. We would be glad to study your worm gear conditions and submit our recommendations as to the proper alloy for your use.

# TITANIUM ALLOY MFG. CO. WORKS: NIAGARA FALLS, N. Y., U. S. A.

BRONZE SALES DEPARTMENT 504 MARINE BANK BLDG., BUFFALO, N. Y.

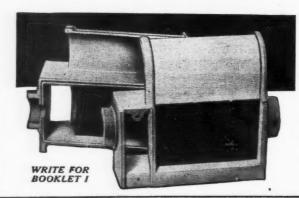


XPERIMENT & FINISHED PRODUCT



#### The Franklin Die-Casting Process is the Direct Way to Results

The advantages of die-casting over the usual forms of machining have become a recognized fact. A die once constructed insures for all time a degree of accuracy and uniformity difficult to secure except through expensive machine operations, at the same time eliminating the necessity of costly machine equipment. This is of special advantage in the development of new inventions. special advantage in the development of new inventions or the meeting of rapidly increasing demands.



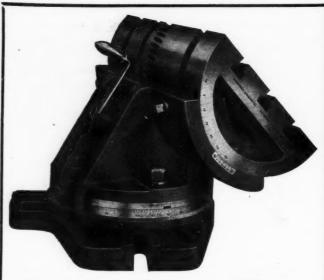
#### FRANKLIN MANUFACTURING CO.

SYRACUSE

738 Gifford Street

NEWYORK





# **Universal Angle Plate**

A little device for shop use that has practically unlimited possibilities of application on lathes, planers, milling machines, shapers, drill presses and grinders. Capable of movement through 360° horizontally and 90° vertically; a thoroughly practical tool that will give quick adjustment to any angle without disturbing the work. Its usefulness will be apparent to every wide-awake owner who appreciates the difficulty of getting accurate results from makeshift, inaccurate devices.

Detailed Information on Request

BOSTON SCALE & MACHINE COMPANY 381-389 Congress Street BOSTON, MASS.

#### "NEW BRITAIN" DROP-HEAD POLISHING MACHINE



DRIVE from below makes this an all-around safe machine. The belt is entirely enclosed— the operator is safe from the belt and the belt is safe from dust, oil and grit. Countershafts, loose pulleys.
idlers and overhead belts are
eliminated and the spindle is pulled down into solid part of box— all of which makes the machine smooth running, convenient and productive.

Write for complete description



The New Britain Machine Company NEW BRITAIN, CONN., U. S. A.

# BARKER

Wrenchless Chucks Increase Output on Any Work, Any Machine, Under Any Condition

A big claim to make for any chuck; but the "Barker" has proved its case by what it has actually done and is doing.

Barker Chucks have been skeptically received in more than one plant where they have later been retained as regular equipment. A Barker Chuck increased average daily output on differential cages from 45 to 64 for a motor car company that thought 45 per day remarkably good. In a plant where brass ties were turned out at the rate of 375 per day, another "Barker" ran the figures up to 625 per day—a 66.6 per cent increase. So it goes through a long list.

The Barker Chuck is a self-contained unit, practical in design, accurately constructed, a universally efficient and economical chuck.

Complete description on request.

We'll be glad to tell in detail the special advantages of Barker Chuck construction.
Write us.

Thomas Elevator Company
22 SOUTH HOYNE AVE, CHICAGO ILLINOIS

### In Selecting Stamping Dies Examine the Bevel



The life of Steel Marking Dies is largely determined by the bevel. A long, narrow bevel requires only a light blow—but it soon wears down and must be discarded.

## MATTHEWS STEEL CUT DIES

are the short, "stubby" kind. They need a forceful blow—but will outwear a dozen of the others.

An uneven bevel brings too much pressure on one side and the figure soon breaks down—often at the first blow.

Matthews Dies are hand cut from the best Pittsburgh steel. They are absolutely uniform and Matthews guarantees them for long and satisfactory service.

All Kinds of Marking Devices
Send for Catalog



Jas. H. Matthews & Co., Inc.

Established 1850

3946 Forbes Field, PITTSBURGH, PA.

Canadian Distributors-Canadian Fairbanks-Morse Co., Ltd.



# Carpenter

Look for the name when you buy taps and dies. It means investing in 47 years of tap and die experience.

### CARPENTER TAPS

cut true threads and retain a lasting cutting efficiency even under the harshest conditions. If there's need for better thread cutting in your work, try "Carpenter" next time. You'll remember the name, but it is just as well to keep a catalog on file.

The
J. M. Carpenter
Tap and Die
Company





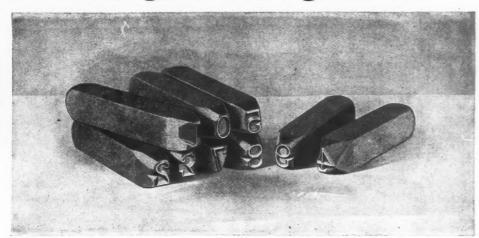
We Can Make
Early Deliveries
Fine files for toolmaking or
manufacturing purposes, accurately cut, uniform in quality.
Considerable quantity and various sizes on hand from which
we can make prompt deliveries.

T. P. WALLS TOOL CO.

SOLE AGENTS
75-77 Walker St., NEW YORK

### For Clear Markings and Long Service

# PANNIER BEVEL STAMPS

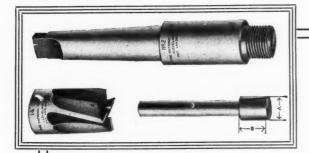


Prompt Shipments

Our Advisory and Consulting Service are yours for the asking. Catalogue on Request. Pannier Steel Bevel Stamps are designed by men who know the exact mathematical degree of balance between maximum efficiency and maximum wear—who turn out stamps that cut a clean, deep impression, and are still strong enough to stand up under hard work. Pannier Stamps are made of best grade tool steel, from blanks sawed from cold bars just as they come from the mill. They receive only one heating—that in the tempering furnace. Grinding, cutting, tempering are done by expert steel workers.

We guarantee every Pannier Stamp against defect in material or workmanship

PANNIER BROS. STAMP CO., Inc. PITTSBURGH, U. S. A.



## Reducing Your Tool Bill with the NATIONAL Counterbore

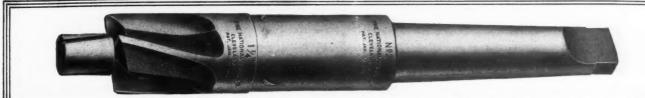
The price of tool steel is soaring—there's no telling where it will stop. You can't do without it—the best you can do is to use no more than you need.

THE NATIONAL PATENT INTERCHANGEABLE COUNTERBORE demonstrates the value of this practice applied to tool making. Of the three interchangeable parts, only the cutter is high speed steel. The pilot and shank are made of strong, durable, but less expensive steel—saving No. 1. The cutter is always the part that wears. If it's a "National," only the cutter need be renewed—saving No. 2.

If you are interested in reducing your tool bill, write for circular.

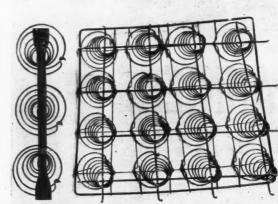
MANUFACTURED BY

THE NATIONAL TOOL CO., Cleveland, Ohio





# S P R I



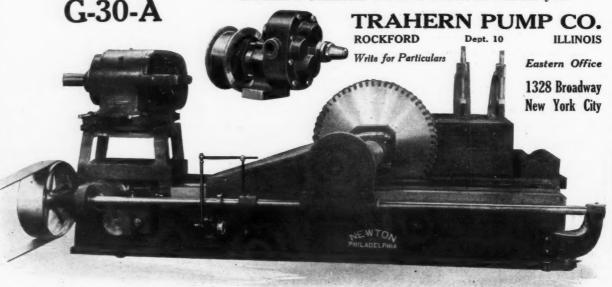
# Coil Springs of Every Kind

Prices Right Superior Service Exceptional Facilities Send us your blue prints or samples for estimates.

# Kokomo Spring Company

Kokomo, Indiana, U.S.A.

ATrahern Cools this Saw that Cuts Bethlehem G-30-A This machine is designed to cut a beam 30 inches deep, weighing 200 pounds to the foot, and having a cutting area of 58.85 square inches. The manufacturers, the Newton Machine Tool Works, Inc., say: "The fact that it supplies enough lubricant to carry off the heat generated by such a large blade, testifies to the practicability and capacity of the mechanism of the pump." TRAHERN ROTARY GEARED PUMPS will do as well for you.



# A Cold Drink for the Industrial Army

There's a great deal of sympathy extended to the men in the trenches who suffer from thirst; but little if any goes to the men in the rank and file of manufacturing—the trench workers of the nation's industries. Shop work is hot and tiresome—a cold drink now and then sets a man up amazingly.

"Meeco" Bubbling Ice Water Fountains are as necessary to maintain uniform production in your plant as your lighting, ventilating and transportation systems. Take care of your men and they will take care of the work.

For attachment to municipal water supply. Holds 75 pounds of ice.  $15\frac{1}{2}$  coils of  $\frac{1}{2}$ " seamless brass tubing. Serves 150 persons.

Our Lines Include: Sanitary Wash Bowls (in Batteries), Bubbling Fountains (Plain and Ice Cooled), Metal Lockers, Metal Stock and Pattern Storage Racks, Metal Shelving, Metal Cabinets, Vault Fixtures, Soda Kettles (40 and 60 Gallons), Metal Stools and Chairs, Water Mixers, Work Benches, Bench Legs, Full Line of Plumbing Fixtures, Etc.

# Manufacturing Equipment & Engineering Company

Works and Mail Address: FRAMINGHAM, MASS.

Office and Showrooms: BOSTON, MASS.





CUT HANDLING COSTS
One man can do the work of
five—if you give him a Stuebing
Lift Truck.

Get the benefit of the experience of such concerns as Goodyear Tire and Rubber Co.,
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Firestone Tire and Rubber Co.,
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Machine Co., Linderman Machine Co., Continental Motors
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U. S. Government, and hundreds
of others who have selected
Stuebing Trucks.

Ease of operation—high lift—
steel construction—positive hydraulic check—make them "The
Choice."

Free trial in your own plant.
Get our book "SYSTEM IN
TRUCKING."

Write now!

THE STUEBING TRUCK CO.

CINCINNATI

OHIO, U.S.A.

Men Who Plan and Design Must Preserve Their Physical Endurance. Avoid Unsteady Tables, Haphazard Filing and Use the Economy Way.

Economy is Harmony

Standard Sizes: 26 x 38-32 x 44 Inches



### **ECONOMY DRAWING TABLE CO.**

Drawing Tables and Filing Cases in Steel and Wood

**TOLEDO** 

OHIO



The Cincinnati Screw Company (Cincinnati Suburb) **TWIGHTWEE** 

SPEED

Trade Mari

C HIP high-speed your steel scrap to us. We'll grade it; remelt it; forge it to the size bars you needadding any Tungsten or other material needed to raise it to the high standard of

### UNDADAGA PROCESS

High Speed Steel. Every bar trade marked as above; the best high speed steel you ever

Write for more information.

DADADAGA STEEL COMPANY INC. SYRACUSE, N.Y.

### STEEL BEARING BALLS

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THE ABBOTT BALL CO. Elmwood Hartford, Conn.

### For Heavy Cuts in Tough Stock



you can be sure of tool stamina if you use service-guaranteed

### Windau Tools

Speed Spiral Milling Cutters, Form Milling Cutters,

Circular Tools and Special Small Tools.

Write for Quotations

WINDAU TOOL 1318 ADDISON ROAD

**COMPANY** CLEVELAND, OHIO



Testing a die for Hardness (Scleroscope on Swing Arm)

### Have You a Scleroscope to Test Your Metals?

For Softness, Hardness or Strength
Can be operated by non-technical help. The majority of manufacturers are thus ordering their material to specifications, as to quality and fitness, meaning that the minority who have not a scleroscope to inspect their material may have to accept the discard of their more up-to-date competitors. It shows if you are getting what you pay for out of your tool steels. Send for our 80-page booklet. Free.

### THE PYROSCOPE PYROMETER

If your heat troubles are still unsolved, investigate the pyroscope, the one common-sense instrument that makes straight for results without fuss. Extreme simplicity—constancy—always ready. Pamphlet on request.

SHORE INSTRUMENT & MFG. CO., Inc., 555-557 W. 22nd St., New York FOREIGN AGENTS: Agent for Great Britain and Colonies, Coats Mch. Tool Co., Ltd., Caxton House, London, S. W.; Glasgow; Newcastle-on-Tyne. Schuchardt & Schutte, Tokyo, Japan. Iznosskoff & Co., Petrograd, Russia. Aux Forges de Vulcain, Paris, France. R. S. Stokvis & Zonen, Ltd., Belgium and Holland.



SECTIONAL
STEEL
SHELVING



THIS vessel, which has served as Headquarters for Vice Admiral Sims and Mother Ship of the Destroyer Fleet now operating in European waters as submarine chasers, went abroad equipped with "Multi-Unit" Steel Shelving for the storage of repair materials, etc., needed by the fleet.

"A Place
For
Everything
And
Everything
In Its
Place"

Super-strength, standardized steel units which can be quickly assembled into stacks of plain shelves or bin compartments of various dimensions.

Construction:—Extra heavy sheet steel with strengthening tubular edges of pleasing design.

Finish:—Furnished in plain steel for rough storage or in olive green, dark green or black enamels for offices, stores, warerooms or storerooms where handsome appearance is a factor.

First cost is the last cost. "Multi-Unit" is the economical, efficient shelving.

"Multi-Unit" Bulletin MD and prices sent on request.



Showing the Method of Assembling Units

### NATIONAL SCALE CO.

(Standard Steel Shelving Division)

8 Mechanic St., Chicopee Falls, Mass.

Manufacturers of National Counting Machines and National-Chapman Elevating Trucks

FOREIGN REPRESENTATIVES: 8.
Haug Ellingsen & Co., Christiania,
Norway. Burton, Griffiths Co., Ltd.,
London, England. H. Brenneisen & Co.,
5 Jules Ferry Boulevard, Paris, France.



Not Bric-a-brac. Built for hard service. Use it like a ladder to reach the top-most bin.

# Don't Experiment with Wrenches-Buy "Coes"





A "Coes" Wrench never slips—never rounds the corners of a nut—never jams the thread. You can depend on a "Coes"; it is stronger by 30 per cent than any similar wrench on the market; it is the choice of experienced mechanics all over the world. "Coes" Wrenches are made in five styles and a wide range of sizes—order by name from your dealer. "Coes" Steel Handle Model, 4" to 21" sizes; Knife Handle, the general utility "Coes," 6" to 21" sizes; Key Model "Coes," 28", 36", 48" and 72" sizes.



COES WRENCH COMPANY, Worcester, Mass., U. S. A.

AGENTS: J. C. McCARTY & CO., 29 Murray Street, New York. 438 Market Street, San Francisco, Cal. 1515 Lorimer Street, Denver, Colo.

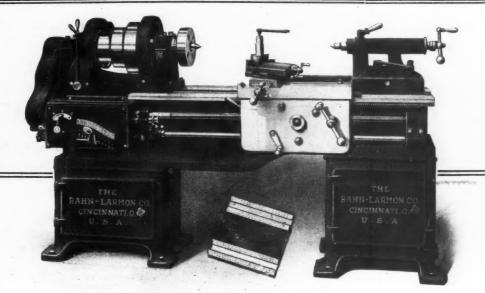
AGENTS: JOHN H. GRAHAM & CO., 113 Chambers Street, New York. London, E. C., 118-122 Holborn, for Great Britain and Continental Europe.







ROCKFORD TOOL COMPANY, Harrison Avenue Rockford, Illinois



# ATTENTION GAP LATHES for SHIP YARD WORK

20/26" x 8"

Swings over V's . . . 21 inches Swings over Gap . . . 27 inches Width of Gap . . . 14 inches

THREE STEP CONE DOUBLE BACK GEAR QUICK CHANGE GEAR

THE RAHN-LARMON COMPANY, Cincinnati, Ohio, U.S.A.

## What Threads or Worms Do You Cut?

The Automatic Threading Lathe does not compete with dies or thread millers in their range of work. Rather, it outclasses both, handling that fine, exact work—threads of every character, particularly those of large diameter—that

can be cut satisfactorily only on a lathe.

It triples output and lowers costs because it does automatically what must be done by the operator on any engine lathe, and one man can attend a battery.

Information?



### AUTOMATIC MACHINE COMPANY, Bridgeport, Conn.

AGENTS: Burton, Griffiths & Co., Ltd., of London, England. Marshall & Huschart Machinery Co. of Chicago, Ill. Motch & Merryweather Machinery Co. of Cleveland, O., and Vandyck Churchill Co. of New York.



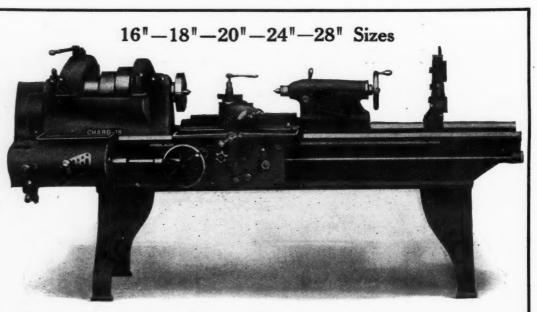
BRANCH OFFICES-NEW YORK **BOSTON** CHICAGO ATLANTA SAN FRANCISCO. REPRESENTATIVES IN FOREIGN COUNTRIES

Makers of Gridley Single and Multiple Spindle Automatics at Windsor, Vermont; and Acme Automatics, Threading Dies, and Screw Machine Products at Cleveland, Ohio

There's an Acme for every kind of screw cutting work up to  $3\frac{3}{4}$  diameter.

Catalog Acme Method "B"?

**Exceptional** Lathe Value



A Chard Lathe is 100 per cent quality. For an example of its thoroughness of construction, study the value put into the spindle. This is made of a special analysis steel, machined from forgings which are hammered down from 6-inch billets. The steel is thoroughly annealed, reheated to between 1525 degrees and 1550 degrees F., quenched, then reannealed at a temperature of from 1225 to 1250 degrees F. Every detail of construction is just as highly specialized—with factors for convenience and safety worked out to a perfect balance.

Write for complete description

### CHARD LATHE COMPANY, Newcastle, Ind., U.S.A.

GENTS: Vonnegut Machinery Co., Indianapolis, Ind. English and Miller Machinery Co., Detroit, Mich. The W. M. Pattison Supply Co., Cleveland, Ohio. Ill, Clarke & Co., Chicago, Ill. Odgen R. Adams, Rochester, N. Y. The F. O. Stallman Supply Co., San Francisco, Cal. J, S. Miller Machinery Company, Ittsburgh, Pa. Monarch Machinery Company, Philadelphia, Pa. Patterson Tool & Supply Company, Dayton, Ohio.

# BICKETT EFFICIENCY

If you have a BICKETT MILLER in your factory you know it is always in use.

If you have not as yet bought one you are minus a good tool.

Not CHEAP, but ECONOMICAL.

Not EXPENSIVE, but EFFICIENT.

Fifteen different styles and sizes, both horizontal and vertical.

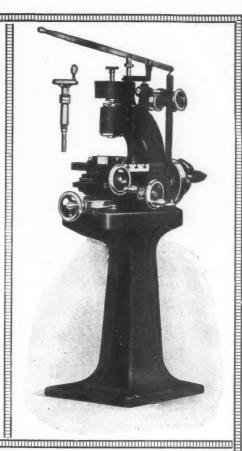
This illustration shows

# The BICKETT No. 0 Vertical Milling and Profiling Machine

with spring lever attachment.

Particularly useful for profiling, routing, and letter cutting.

This machine can also be furnished with foot treadle attachment.



# THE BICKETT MACHINE & MFG. COMPANY 1118 Richmond Street CINCINNATI, OHIO, U. S. A.

EUROPEAN AGENTS: The Selson Engineering Co., 83-85 Queen Victoria St., London, England.

# Gray's Sheet Metal Cutter Saves a Lot of Metal

Steel is high and going higher—so is your scrap heap unless you are using a Gray Metal Cutting Machine for cutting gauge blanks, templates, gaskets, gear covers, jigs, etc.

Designs may be laid out close together on a large sheet—conserving every ounce of metal. The Gray Machine cuts a clean, smooth, accurate slot—without the spring and buckled edges of the shearing cut. This is double economy.

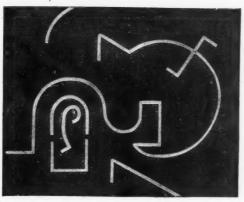
Capacity includes metal 3/16 inch thick in which 30 inches a minute can be accurately cut—the stock is automatic-

ally fed in by rollers above and below while the operator follows the design and controls the cutter.

Complete description in Bulletin. Write for it.



PATENTE



Steel Plate, 10" x 18", 3/16" thick, finished by the Gray in 10½ minutes.

W. J. SAVAGE COMPANY, Inc. KNOXVILLE TENN., U. S. A.

# Hercules

Turret Lathe

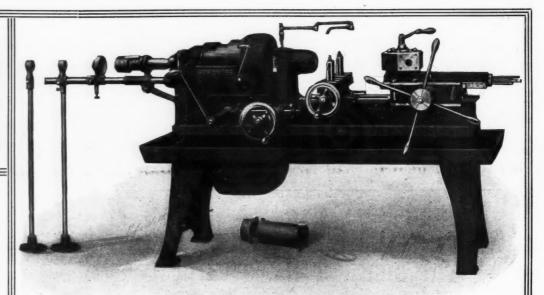
**Screw Machine** 

Glad to Send Detailed Description on Request.



45 Mills St., ASTORIA In the City of New York

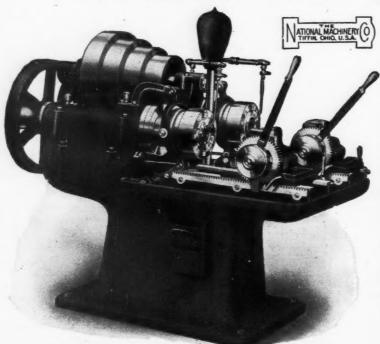
Sales Office: 50 Church St., New York



HIS machine is designed for working bar stock, for producing work that requires turning and threading at one setting, and for machining castings, forgings and second operation work. It is strong and rigid; bed is well braced; head and bed in one-piece; bearings all of phosphor bronze and lubricated automatically by a chain-oiling system. Machine is regularly equipped with automatic chuck and bar feed; but can be furnished without these attachments if desired. It is an accurate worker, operates smoothly, has provision for taking up wear.

# A National Bolt Cutter

For Good Threads and Big Productions



About 70 per cent of all screw threads are cut on Bolt Cutters and a large percentage of this production is turned out by "Nationals." No matter what the threading problem, there is a "National" to meet it, which will give you accurate threads, along with the largest possible production.

The National Die Head has a positive lock which makes it as rigid as a solid die, and insures absolute accuracy in threading. This accuracy continues throughout the life of the machine, as there is no friction or wear that can affect the threading.

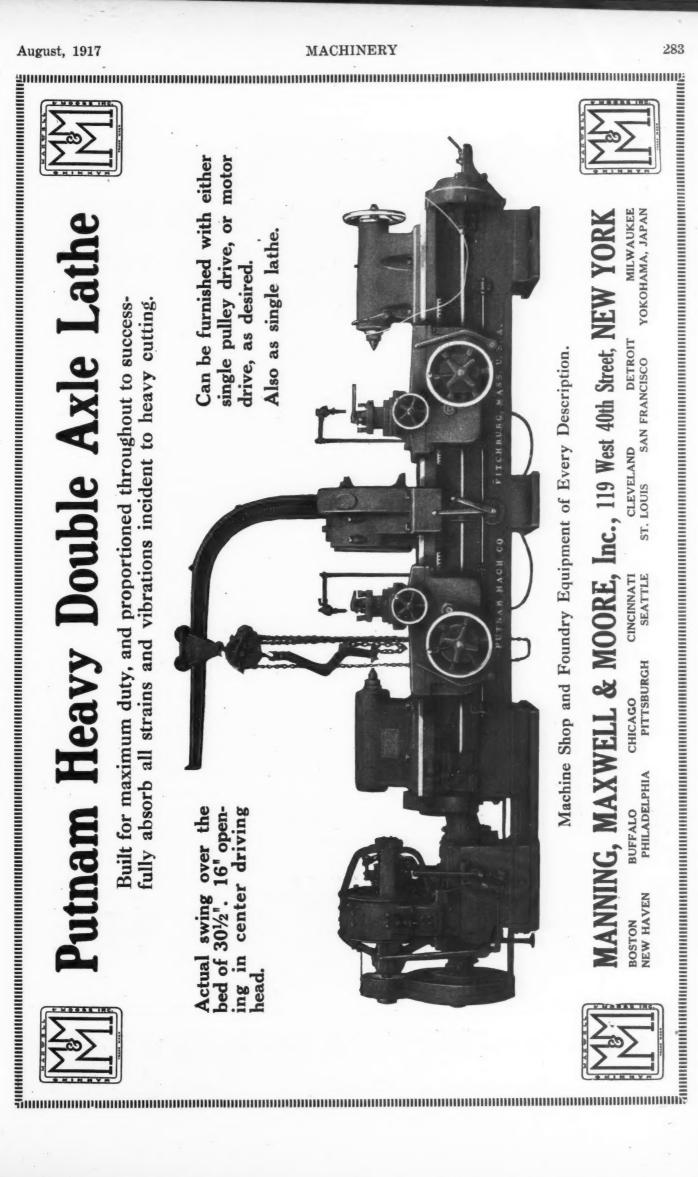
The National Die Head is simple, hence easy to adjust and operate; and can be run at the highest cutting speeds.

Tell us your threading problems and let us give you our recommendation.

THE NATIONAL MACHINERY CO., Tiffin, Ohio

Originators of Modern Bolt, Nut and Forging Machinery

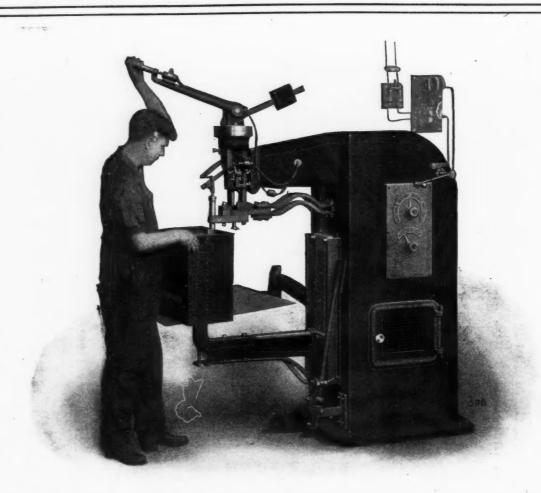












# Reduce Riveting Costs 60 to 90%

How? By Spot Welding

One boy and a Thompson Spot Welding Machine can do as much work as five men by the old fashioned method. In spot welding there are no holes to punch, no rivets used, and the result is a stronger and better finished job. Thomson Spot Welders in operation show a saving of from 60 to 90 per cent. Send us samples of your work. We will weld them and return them with figures of surprisingly high speed and low cost.

If you are riveting work that should be welded you're wasting good money

Write Us



Ask for Bulletin S-2

THOMSON SPOT WELDER CO.

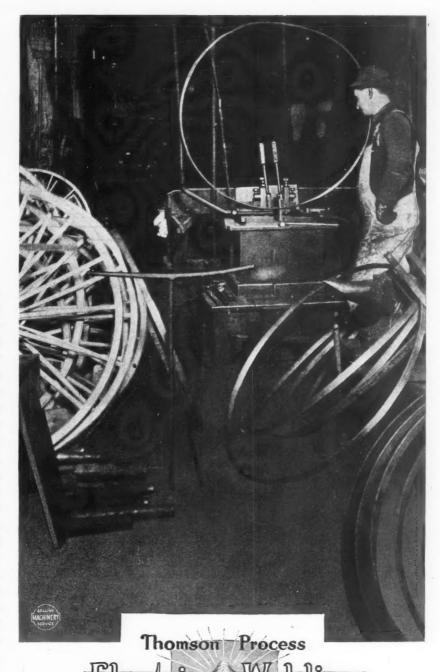
84 State St., Boston

SO E. 42 = St. New York City

602 Finance Bidg. Phila

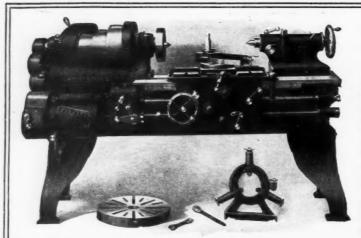
# The **Proper** Way to Weld Tires

The proper way, according to the Martin Carriage Works operators, at York, Pa., is the Thomson way. For eighteen years this Thomson Electric Welding Machine has been welding carriage tires. Two minutes per tire completes the job. All the operator does is clamp the work in the welder, bring the ends together and turn on the current. Output has ranged from 15,000 to 18,000 tires per year. The Martin people are going into automobile work, which means just a change of line for the Thomson, since Thomson Electric Welders have made some of their best records in the automobile industry.



The important point is that no matter where Thomson Welders work, or how hard they work, they wear well. They are long service machines, high-grade to the smallest detail. We'll be glad to show you before-and-after production figures from concerns now welding with Thomson machines—we'd rather show Thomson advantages on your own product, however. No charge or obligation for demonstration. Ask for particulars and Bulletin B-2.

1127 Majestic Bldg., Detroit 323 N.Sheldon St., Chicago. III.



### 16" Lehmann Lathe Swings 181/4"

Built for Heavy Duty and Accuracy

3-STEP CONE for 3" belt, DOUBLE BACK GEARS, CHILLED BED, HIGH CARBON STEEL SPINDLE, PHOSPHOR BRONZE BEARINGS, DOUBLE PLATE APRON, STEEL GEARING, BALL THRUST BEARING for lead screw, cuts threads 2 to 112 to the inch without change of gears, GEARED FEEDS from .007 to .4. 9' bed takes 5' between centers, net weight 3020 lbs.

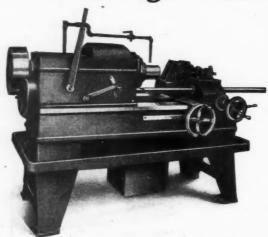
Write for circular illustrating NEW and INTERESTING FEATURES of these lathes.

### LEHMANN MACHINE CO.

606 to 612 South Broadway

ST. LOUIS. MO.

# Thurlow Waving and Undercutting Machine



Designed to cut, groove, undercut and wave shells simultaneously and at a single operation. Its adoption in any plant never fails to reduce costs and increase production, and in addition, it releases for other operations the lathes now tied up on this work. The Thurlow is made in three sizes to take shells from 3 inches to 9 inches; is strongly built and easy to operate.

Full details on request.

Thurlow Steel Works, Inc. 1418 Walnut St. PHILADELPHIA, PA.

# STEPTOE Milling Machines and Shapers

Set Free Your Large Millers and Planers for Heavier Work



quickly than a large mill-

ing machine.

The same is true in regard

to a shaper as compared to a

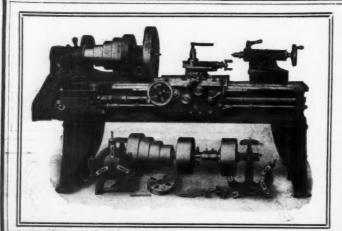
heavy planer.

Co.
Brighton
Cincinnati, Ohio\*



Steptoe Milling Machines and Shapers will enable you to get economy and efficiency in production by the proper distribution of work.

The best possible evidence of their reliability, accuracy and economy is the fact that thousands of them are in worldwide use today.



# **Champion Lathes**

Built to Turn Out Accurate Work Fast

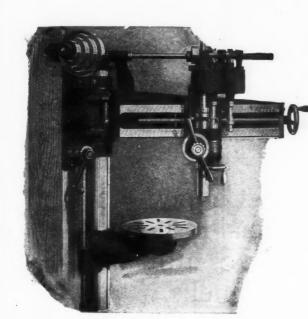
Champion Lathes are solidly constructed 12-, 14-, 16- and 18-inch machines. Metal is distributed to give each machine maximum rigidity and strength; power is provided to handle heaviest cuts within range; convenient arrangement of operating parts assures speed. The "Champion" is an A-1 tool room or manufacturing lathe. General Catalog on request.

### CHAMPION TOOL WORKS CO.

2422 SPRING GROVE AVE., CINCINNATI, OHIO, U.S.A.

# Canedy-Otto Wall Type Radial No. 51

Every Shop Needs It—Every Shop Owner Can Afford It



For the garage, the machine shop or other plant where a low cost "Radial" is needed. Adapted for a wide range of work, absolutely reliable in every respect. Equipped with automatic cut-off, four instantaneous speed changes, and quick return lever serving as pilot to move spindle. Well built throughout, rapid, accurate. Furnished with  $2\frac{1}{2}$  or  $3\frac{1}{2}$  foot arms, drills up to  $1\frac{1}{4}$ ".

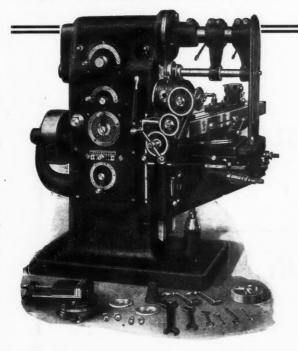
### PRICES

No. 51—2½ Foot Arm . . \$237.50 Net No. 51—3½ Foot Arm . . \$250.00 Net F. O. B. Chicago Heights

Carried in stock by leading jobbers and machinery dealers everywhere. Ask for circular and name of our dealer in your locality.

CANEDY-OTTO MANUFACTURING CO. CHICAGO HEIGHTS, ILL.

# The Rockford No. 2 is a Well Balanced Machine



Extra reinforcement at every point of strain, arm braced to withstand vibration, and smoothly running mechanism insure the uniform, powerful service which only a well balanced machine can give.

Fourteen changes of feed, eighteen speed changes—ranging from 13 to 350 R. P. M.—and simple, instant control with accurate adjustment, equip the "Rockford" to handle any piece of work its ample table will accommodate.

These twin qualities, perfect balance and sturdy rigidity, make it possible for the NO. 2 ROCKFORD MILLING MACHINE to take heavier cuts without chatter than any similar machine of its size.

Complete specifications on request.

ROCKFORD MILLING MACHINE CO., Rockford, Illinois

# IMMEDIATE DELIVERY

From Stock

Complete Line Calipers and Gauges and Official Inspecting Apparatus for 75 mm and 155 mm Shells

Including Shells, Cases, Sockets, Fuses, Etc.

Stamped with the Approval of the French Technical Artillery Section

Also Full Stock
Caliper Gauges, and Thread Gauges
for

# **Aviation Motors**

Hispano-Suiza — Clerget — Rhone — Gnome

# LA PRECISION MECANIQUE

11, Rue Vergniaud

PARIS, FRANCE

Manufacturer of Caliper Gauges-Established 1912

Telegraphic Address: CALIBRE, PARIS





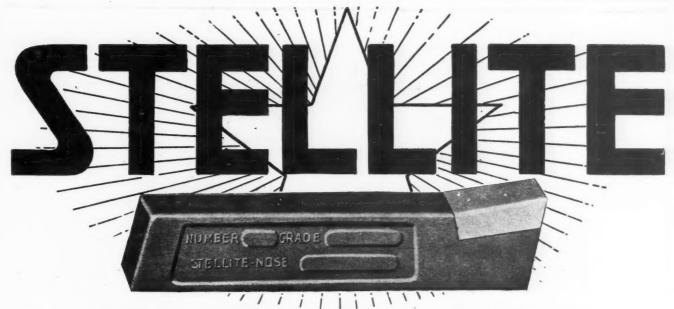
# Bunting's Bronze Bushings and Bearings

"Selling" the purchasing agents of million-dollar corporations is a man-size job. These gentlemen know a "good buy" when they see one, but you have to show them every inch of the way. Good salesmanship is not enough—a good product must back it up.

The fact that 51 concerns rated at \$1,000,000 and over, in addition to 175 more rated at from \$200,000 to \$1,000,000, order Bunting's Bronze Bushings and Bearings is sound evidence of a thoroughly satisfactory product. If million-dollar corporations, with their complete and modern equipment, find it more profitable to buy bushings and bearings completely machined and ready for assembly there's something worth while for you in Bunting's service. They find it cheaper and better or they would not buy. Think that over and send for price list G.

### THE BUNTING BRASS & BRONZE CO.





# ARC WELDE



Jobs like the one that produced this chip throw Stellite superiority into bold relief. The chip was turned off a 11/2" bar of 50 carbon steel by a Stellite Arc Welded Tool at such a high turning speed and with such a coarse feed that the end of the chip was fused, and the floor was scorched where the chip dropped upon it.

Stellite "stacks" up against some mighty tough turning propositions, but the harder they are the greater are Stellite advantages. Any steel tool will stand the ordinary job; but it takes Stellite for the "heartbreakers."

We'll gladly tell you all about it, if you'll write.

### THE HAYNES ITE COMPANY

HOME OFFICE AND PLANT

KOKOMO, INDIANA, U.S.A.

BRANCH OFFICES:

1829 Lytton Bidg., Chicago, III.

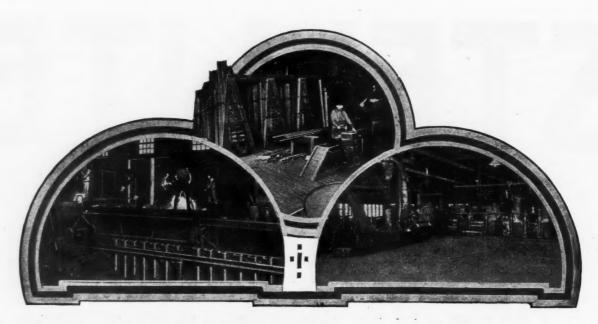
2402 Union Central Bidg., Cincinnati, O.

1370 Penobscot Bidg., Detroit, Mich.

2220 Farmers' Bank Bidg., Pittsburgh, Pa.

also sold by
THE MIDVALE STEEL COMPANY
OFFICES: Philadelphia, Boston, New York, Cleveland, Chicago, San Francisco.

Licensed Canadian Manufacturer
DELORO SMELTING AND REFINING COMPANY
Deloro and Montreal, Canada.



# Why WOLFRAM is a Standard Tungsten High Speed Steel

Heat Resisting

Wolfram is Carbon Steel without Tungsten will harden at 1400 degrees F. and will coarsen at 1500 degrees F. The same steel containing 18 per cent Tungsten will not coarsen even at 2350 degrees F.

> Tungsten is the only alloy of which as high as 18 per cent may be used beneficially in tool steel, and the heat resisting power of the steel is increased in proportion to the Tungsten contained.

Wolfram is Uniform The nature of the alloying element must be such that the commercial product will be uniform and reliable. One heat must be very similar to another, one bar to another, and each bar must be the same throughout its entirety.

Wolfram is Unchanging

Again, the steel must stand the test of time. It must stand repeated redressing, hardening and use, without breakage or loss of cutting power. And TUNGSTEN is the most stable alloy.

WOLFRAM is of uniform high quality, and may be worked down to the last ounce without variation.

### VULCAN CRUCIBLE STEEL COMPANY

**ALIQUIPPA** 

ESTABLISHED 1900

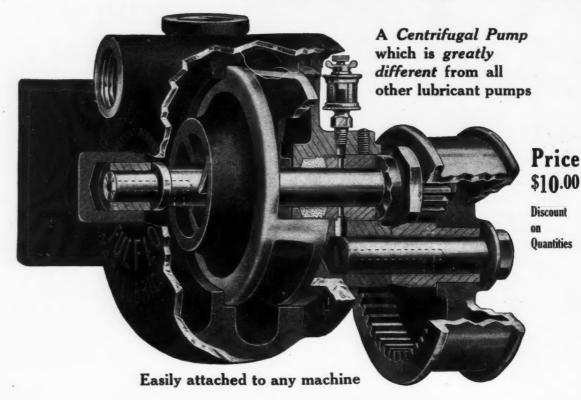
PA., U.S.A.

BRANCHES:





# FULF The Lubricant Pump You've Looked For



THE ONLY LUBRICANT PUMP FOR WHICH THESE CLAIMS CAN BE TRUTHFULLY MADE

"The Trouble-proof Pump"

- 1 Greatest Capacity. 50 per cent more volume than any other pump its size. 1 to 20 gallons per minute, according to speed.
- **2** Cannot Lose Its Prime. Water has to run uphill before the Fulflo can lose its prime. All other pumps depend on valves to hold their prime.
- 3 Longest Life. There is but one pumping part—the impellor—and it touches nothing but the liquid, therefore retains its pumping efficiency indefinitely.
- 4 Won't Clog. Anything that can get in will go right through without injury to the pump. No passage smaller than intake, which is 3/4 inch.

Are you going to continue to put up with lubricant pump troubles which have heretofore been necessary evils, or are you going to improve this feature of your manufacturing methods as you have all others, now that it is possible for you to do so?

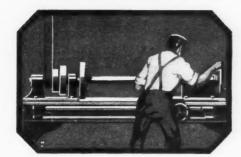


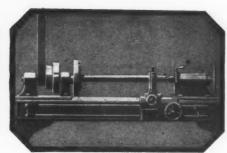
# THE FULFLO PUMP COMPANY

129 Opera Place CINCINNATI, OHIO, U.S.A.



# The Machine Without a Man





NE of the chief causes of delay in all forms of manufacturing is the machine without a man—the machine that is momentarily idle.

When a workman has to shut down his lathe to look for the bolt he is to turn, when he has to stop work to sharpen or find his tools, his machine is not producing and a decrease in output results.

Of all the causes which make it necessary for an operative to leave his machine, poor light is the most common— and the most unnecessary.

Even if the window to which a workman must step in order to adjust his micrometer or examine his calipers is but a few feet distant, a certain amount of time is lost. Insignificant as these seconds may seem in each individual instance, the total amount of time wasted by all operatives in similarly unproductive movements is far from negligible.

Every machine in your plant should be so well lighted that no workman need ever step away from it in order to see more clearly. The lamp that makes it unnecessary for him to walk to the window will soon pay for itself.

Adequate illumination will remove one of the chief causes of delay. It will enable you to speed up production by keeping your machine running all the time, and it will also improve the quality of your output.

By suggesting improvements and alterations to your lighting system our Engineering Department is ready to help you remove the most unnecessary cause of delay. This service is free and obligates you in no way.

"Increasing and Improving Production" is the title of a new book we have just published. The wide experience of the author, Mr. R. T. Kent, in industrial plant operation has enabled him to discuss the problems of factory management from the standpoint of practice rather than theory.

A copy of this book will be sent upon request to any industrial plant manager.

# Westinghouse Lamp Company 165 Broadway, New York

Sales Offices and Warehouses Throughout the Country



GUARANTEED BY THE NAME

# GOODSILIGIO GOOD TOOLS

# IMMEDIATE DELIVERY

on Goodell-Pratt and Greenfield Drill Chucks



Goodell-Pratt Drill Chuck



Goodell-Pratt Drill Chuck Morse Taper Shank



Goodell-Pratt Drill Chuck Bit Brace Shank



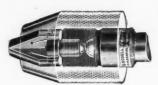
Goodell-Pratt Drill Chuck Shank Fitting No. 2 Ratchet

At the present time we have in stock, or can assemble within a very short time, all styles and sizes of Goodell-Pratt and Greenfield Drill Chucks.

These chucks are made entirely of steel, are very simple in construction, but will be found equal in accuracy and durability to many that are very much more expensive.

We make such extraordinarily large quantities of these chucks for use on our various drilling devices that we are able to sell them at remarkably low prices.

These chucks are regularly made in four different capacities up to ½ inch. They can be furnished with ½ inch, 41/64 inch, bit brace, or Morse taper and other shanks; or without shanks if desired.



Greenfield Drill Chuck Sectional View



Greenfield Drill Chuck Morse Taper Shank



Greenfield Drill Chuck Taper Hole



Greenfield Drill Chuck Bit Brace Shank

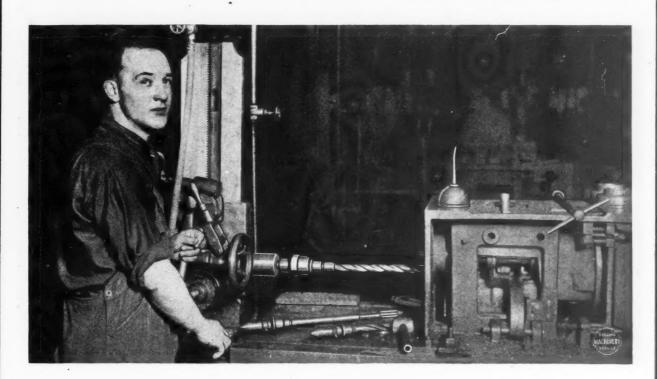
**GOODELL-PRATT COMPANY** 

**GREENFIELD** 



MASS., U. S. A.

# WIZARD CHUCKS AND COLLETS



# Equally Satisfactory on Either Horizontal or Vertical Spindles

At the Morrow Mfg. Co.'s plant, Elmira, N. Y., time is money; every second is made to count. If work calls for boring, drilling, reaming, tapping, etc., whether on boring machines, lathe or drill press, about the first move the operator makes is to reach for his Wizard Chuck and Collets. He can make tool changes with a Wizard outfit without stopping the spindle; he lowers non-productive time to the minimum, and incidentally he makes an A-1 record for himself and his machine.

WIZARD Chucks have a sure grip. They hold big tools in heavy cuts regardless of spindle position. They have been part of the Morrow regular shop equipment for five years. To operate a Wizard Chuck you grasp the chuck in one hand and the tool in the other and the trick is done.

Can you afford to change tools the old fashioned way? Order a "Wizard" on trial and find out.

Write us about it.



## THE McCROSKY REAMER CO.

MEADVILLE, PA., U. S. A.

EXPORT AGENT: Benjamin Whittaker, 21 State St., New York, N. Y.

DIRECT REPRESENTATIVES: Young, Corley & Dolan, Inc., 115 Broadway, New York City. J. R. Stone Tool and Supply Co., 24 Goebel Bldg., Detroit, Mich. R. E. Ellis Engineering Co., 549 Washington Blvd., Chicago, Ill.





# DURABILITY and QUALITY

Are Always Found Together

Send for Catalogue

NAPIER SAW WORKS, Inc.

SPRINGFIELD MASS.

# HUTHER High Speed Inserted Tooth Saw (Patented Oct. 29, 1907 Jan. 19, 1915)

### The User Says:-

"It has done everything put up to it and shows greater efficiency than solid blades."

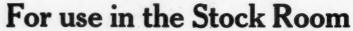
And the man who tells the story has used this Huther Blade for three years, on miscellaneous work of all kinds.

Let us tell you more about Huther Saws-show you why they are efficient, economical saws.

Huther Brothers Saw Manufacturing Co. Rochester, N. Y., U. S. A.

1108 University Avenue

# LEA-SIMPLEX SAWS

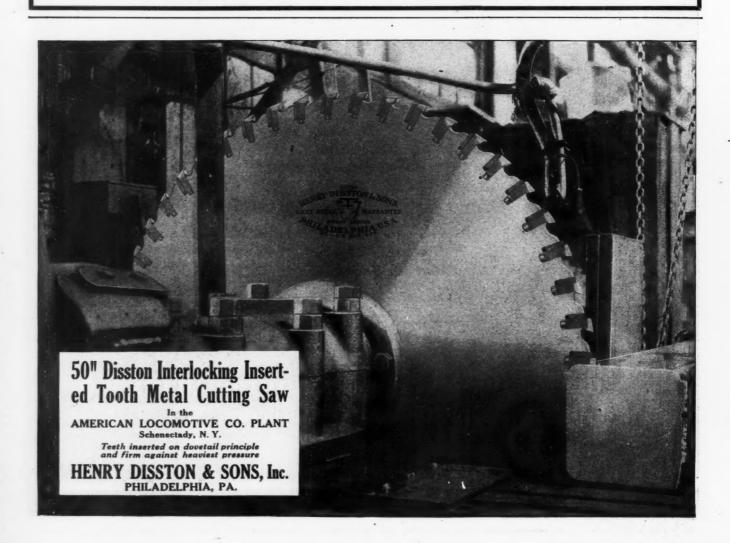


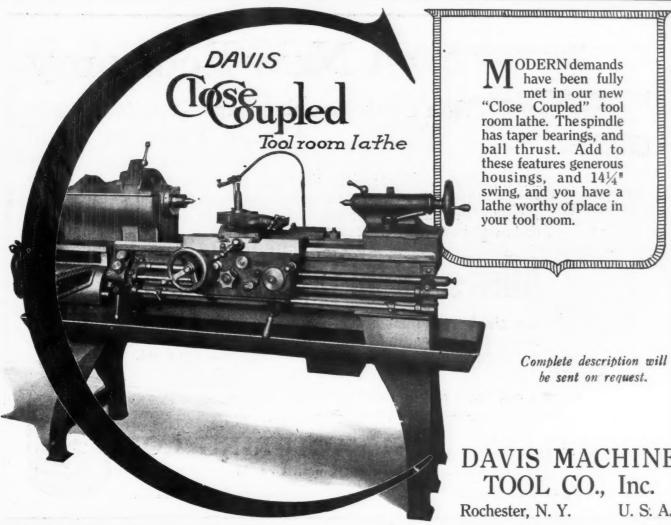


A group of Lea-Simplex Cold Saws, represented by this No. 15 machine, has earned the good word of the Buffalo Forge Company, Buffalo, N. Y. The Buffalo Forge people have worked these machines for eight years—worked them hard—and found them satisfactory in every way. They are still doing most of the stock cutting, and have every appearance of being good for a long busy future.

Lea-Simplex Cold Saws are simple, powerful, dependable machines with special reasons—the sprocket drive, for one—for remarkable performance. Write for particulars.

# EARLE GEAR & MACHINE COMPANY 4705 STENTON AVENUE PHILADELPHIA, PA.



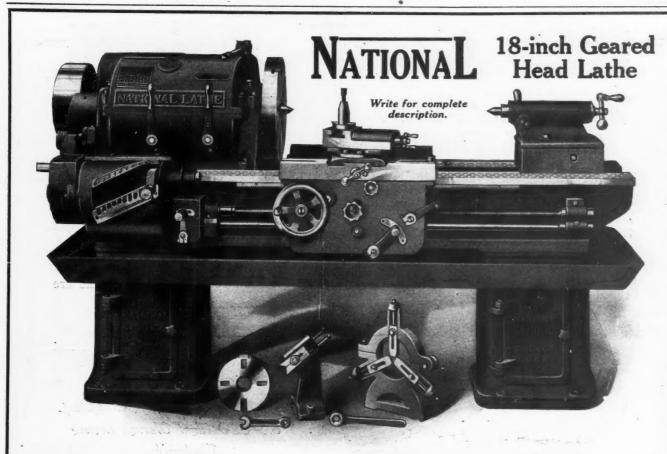


**ODERN** demands have been fully met in our new "Close Coupled" tool room lathe. The spindle has taper bearings, and ball thrust. Add to these features generous housings, and 141/4" swing, and you have a lathe worthy of place in your tool room.

> Complete description will be sent on request.

DAVIS MACHINE TOOL CO., Inc.

U. S. A. Rochester, N. Y.



THE NATIONAL LATHE COMPANY

Established 1912

15 West Second St., Cincinnati, Ohio, U.S.A.





Allen Patent Tap Extensions eliminate the necessity of keeping taps with extra long shanks on hand, in case you ...may need them—and prevent delay when you do need them and have none in your equipment.

# Allen's Patent Tap Extensions

used singly or in combination—add from  $1\frac{1}{2}$  to 11 inches to the effective length of your taps. Fit the shanks of all standard makes—easily ground to fit others—try a set.

We also make a full line of Safety Set Screws Many styles and sizes.

### THE ALLEN MANUFACTURING CO.

135 Sheldon Street, Hartford, Conn., U.S.A.

People's Life Insurance Bldg., Chicago, Illinois

173 Princess Street, Manchester, England



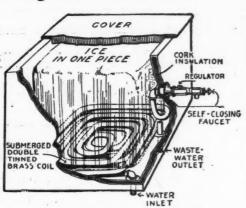


# ALLEN Instantaneous Water coolers

Did you ever notice how much better a man works after he has taken a refreshing drink of water?

Attach to City Water Supply

Ice is Separated from Water



Sectional View Showing Construction of

"Dog Days" are coming but that's no reason why your workmen should lead a "dog's life" through this sweltering season. Give them plenty of good, cool water to drink, make them comfortable as possible, and production will not suffer. Allen Water Coolers do the trick. Stock sizes for 25, 50, 100 or 200 pounds of ice, fitted with self-closing faucets or bubblers, sanitary and economical.



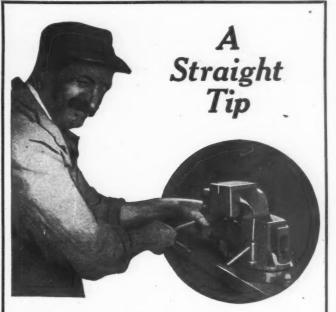
Notice Ice Goes in In One Piece-Lasts Longer

Our list of satisfied users includes many plants of national reputation, such as:

Studebaker Corporation. Peerless Motor Car Co., Chalmers Motor Co.. Wrigley Chewing Gum Co., Glidden Varnish Co., Western Union Telegraph Co., Curtiss Aeroplane Co., Cleveland Automatic Ma-chine Co., Chevrolet Motor Co. Carborundum Co., Kelsey Wheel Co., Standard Motor Construc-tion Co.. Remington Co., King Motor Co., John A. Roebling Sons Co., Electric Auto-Lite Co., Crocker-Wheeler Co., Hudson Motor Car Co.

Write for folder on
"Drinking Water Coolers that
Save Money."

The Allen Filter Company TOLEDO, OHIO, U.S.A.



# The Athol Vise is a Dependable Vise

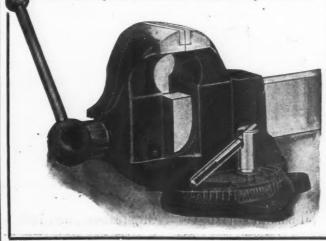
"Now it swivels and now it don't. Swing it round till you have it at just the handy angle, push down the lever—and get to work. The base is as solid as bed rock and will stay so until you release the bull-dog grip of the Starrett locking device. Don't forget to disengage the handle and drop it down out of the way. Your work can't slip, the buttress thread on the vise screw was specially designed to hold it—and the Athol hold is some grip."

A convenient, dependable vise is an important asset in a shop that does particular work.

Send for complete description and catalog of our machinery and high-grade tools.

### ATHOL MACHINE COMPANY

ATHOL, MASSACHUSETTS, U.S.A.





### O. K. TAPS AND DIES For Long and Faithful Service

Hammered from flat bar steel, specially heat treated, given ample chip clearance and means for lubrication, O. K. Taps and Dies are well adapted to survive a long period of active duty.

Accuracy and durability are standards that are never lost sight of in the manufacture of these tools. They are twin qualities that can be reckoned on by every user.

Complete list in Catalog 7A.

### F.E. WELLS & SON COMPANY

GREENFIELD, MASSACHUSETTS





### You Can Now Solder Aluminum Successfully

Send for Welded Sample



Makes joints that are stronger than the metal. No flux required. Used with gasoline torch,

### SAMPLE BAR \$1.00

Used and endorsed by U. S. Army and navy, and leading a mobile and aeroplane manufacturers. Send for booklet 200.

SO-LUMINUM MFG. CO., 1790 Broadway, New York

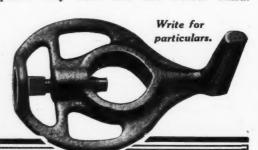
### **Protected Lathe Dogs** SAFE --- RELIABLE



We carry a full stock of standard crucible cast steel, protected lathe dogs-strong, durable, dependable We are regularly lathe dogs. supplying concerns whose policy is to surround their workers with the most reliable safeguards they can find. We shall be glad

to go into the question of lathe dog equipment with you and explain why ours are the better kind.

Straight or **Bent Tail** Lathe Dogs any size, any form.



The West Steel Casting Co. CLEVELAND

### Oil Pan Logic

Sheet Steel Oil Pans weigh less, cost less and wear longer than any other kind and fulfill every requirement.

Incorporated when assembling or easily attached to machines already on the floor.

### LATHE PANS SPLASH GUARDS GEAR

**GUARDS** 

Littleford Sheet Steel Oil Pans

are the logical pans for your equipment. Send for details, prices, etc.



354 E. Pearl Street

CINCINNATI, OHIO



# Mystic Cutting Compound-

When your work is coming fast, and production is needed badly, you will appreciate the speed increasing qualities of Mystic Cutting Compound. Mystic keeps tools cool and cutting edges in good trim. The leading lubricant for turrets, automatic bolt cutters, drilling and milling machines.

Let us send you a barrel on 30 days' approval, and convince you.

# Cataract Refining & Manufacturing Co.

General Offices: Marine National Bank Building, Buffalo, N. Y.

PLANTS: BUFFALO—CHICAGO

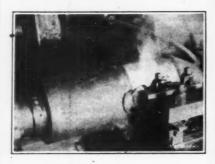
Eastern Department, 17 Battery Place, New York City. Western Department, 3

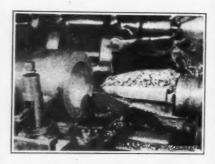
Warehouses: Detroit, Boston, New York, San Francisco, Toronto, London, Eng. Western Department, 327 So. LaSalle St., Chicago, Ill.















# MACHI

Showing clearly and vividly every High-Explosive

HIS extraordinary motion picture continues MACHINERY'S "bit," which began with the remarkable treatise on Shrapnel Shell Manufacture printed more than three years ago, and has furnished the government as well as engineers and manufacturers a mass of definite specific information on mechanical methods and processes in the making of Shrapnel, High-Explosive Shells, Rifles, Gauges, and other devices of the utmost importance to a modern nation engaged in or preparing for war. MACHINERY was the first journal in the world to cover these subjects and did it long before Uncle Sam found it necessary to join the Allies. It was a work of preparedness. was read and studied by the whole engineering world—and it served in good time.

MACHINERY'S motion picture was arranged, made, and produced by MACHINERY'S Staff, and shows in detail every operation from the rough forging of the shell to the final inspection and packing for shipment. As a movie it is different. You see exactly what the cutting tool is doing and you see each test clearly made. Detail drawings flashed upon the screen between the operations show exactly what each step in the process means.

MACHINERY, 140-48

# NERY'S PICTURE

detail in the machining of a 9.2" Howitzer Shell

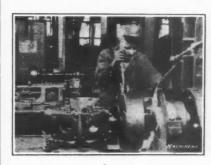
HE picture has been shown with great success at the Cincinnati Convention of the American Society of Mechanical Engineers and the National Machine Tool Builders' Association, and before Engineering Societies, Superintendents' and Foremen's Clubs, Employers' Associations, and other industrial gatherings in Cleveland, Buffalo, Rochester, Syracuse, Fitchburg, Worcester, and elsewhere.

MACHINERY is arranging an itinerary to show this interesting film in all the leading industrial centers and will be glad to hear from mechanical societies, engineering schools, manufacturers and others interested. This is not a money making proposition and there is no charge for showing the picture or for the use of the film. All that is necessary is to provide the auditorium and the simple facilities required. Mr. Lucas of MACHINERY'S Staff gives a concise explanation of the operations as they are shown. Total time required is about thirty minutes. It is a real picture of actual operations in logical order and was taken in the High-Explosive Shell Department of the A. P. Smith Mfg. Co., East Orange, N. J.

Write MACHINERY Now about your Dates for the Fall.

Lafayette St., New York

















We'll be glad to show you why your portable drills, reamers, grinders, etc., should be picked from the STANDARD Line.

Catalogue on request.

# PAY A GREATER RETURN THAN EVER BEFORE

Today is the day of intensive production—of crowding every hour full of productive activity. It's the day of the ever ready, easy to handle, universally useful, time-saving portable tool. Standard Portable "Electrics" are working where the drive is thickest—in machine tool and automobile plants, air-plane factories, railroad shops, etc., working hard and working profitably. They lead the field for accuracy, speed, power and endurance, and they are notably economical to use.

The list of Standard users reads like an industrial directory. It includes the U.S. Government and many of the largest manufacturers in the country.

# STANDARD ELECTRIC TOOL COMPANY

CINCINNATI

OHIO, U. S. A.







# Pawling & Harnischfeger Co. No. 52 Heavy Duty Vertical Drill

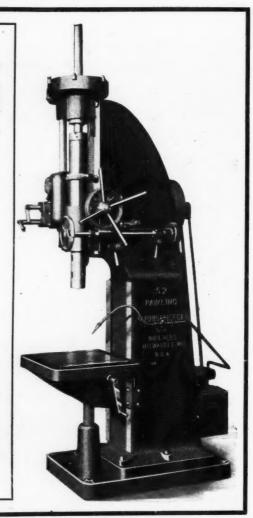
This P & H machine is of rugged construction throughout and is designed for the heaviest duty that may be required of a drill of this size.

A machine of this kind, which is master of its class, should surely have your attention long enough to convince you that it is an efficient and economical tool for your work.

Let us send complete description of the Drilling and Boring Machine suited to your work. Eleven sizes—all high grade, well built, widerange machines.

# DALE-BREWSTER MACHINERY CO., Inc.

545-547 West Washington Blvd., CHICAGO, ILLINOIS 30 Church St., NEW YORK





Milling Machine A simple machine—operator has absolutely no thinking to dolevers to pull, that's all. Semiperation. Exautomatic in A big pro-to 3½" ditremely accuraco. ducer. Capacity ameter, internal thread.

Let us send complete description.

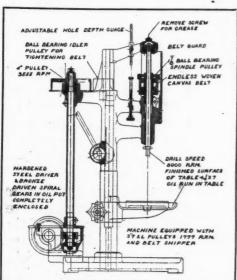


. Manufacturing Co.

# THE LANGELIER

No. 1 High Speed Ball Bearing Drill, Eight Thousand R. P. M.

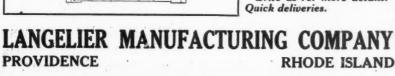
This high-speed ball bearing sensitive drill is built expressly for drilling holes up to 7/32" diameter, developing full cutting efficiency of the drills. It takes up to 6" in height and drills to 3" from edge. Table working surface,  $4\frac{1}{4}$ " by 7". Total spindle feed 2". The spindle is hardened



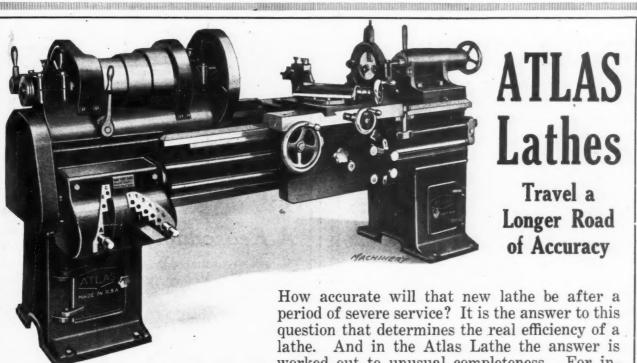
steel ground to size; it is doublesplined to provide perfect bal-ance at high speed. Upper end runs in imported high-grade ball bearings; lower end runs in phosphor bronze bearings. Machines have fine threaded depth gauge. Spindle driving belt is endless and without quarter turns. Tightener provided. Tension of belt does not affect sensitiveness of spindle speed.

Machines also made in No. 2 size for drills up to 3/8". Both sizes in bench or floor types and either in single spindle or gang models as desired.

These are remarkable tools—write us for more details.
Quick deliveries.







Travel a Longer Road of Accuracy

How accurate will that new lathe be after a period of severe service? It is the answer to this question that determines the real efficiency of a lathe. And in the Atlas Lathe the answer is worked out to unusual completeness. For in-

stance, 20 per cent steel mixture in the "V" bearings provides a harder metal on the shears than in the carriage. Thus most of the wear is confined to the carriage and accuracy of alignment is preserved. There are other reasons why Atlas Lathes "travel a longer road of accuracy." Ask for details.

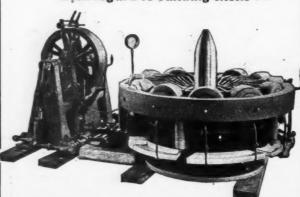
HE TAYLOR MACHINE CO., Cleveland, Ohio

**Manufacturers of ATLAS Machine Tools** 



# The U. S. GOVERNMENT

has made strict regulations with regard to banding shells.



HIS Hydraulic Banding Machine meets all requirements, and bands any size shell from 151/2" down.

The machine is also well adapted for general banding work of all kinds. It is a fast worker and built for hard service. A special feature holds bands in place as they enter the grooves and prevents shearing—an appreciable advantage.

Details on request.

The West Tire Setter Company ROCHESTER, N. Y.



# A Reasonable Price

We offer reasonable price and early delivery as two very good reasons why you should buy G. M. Engine Lathes. They are good lathes mechanically—well built, tested, swing 16 inches, with single back gears, provided with ample oiling facilities, etc.

# **G-M Engine Lathes**

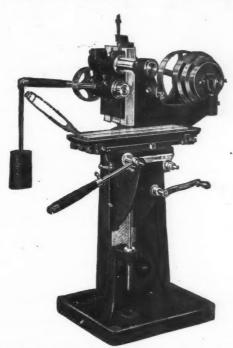
Eight-foot bed only. Can be furnished with taper attachment if required. They are all you can require in a lathe this size.

Let us send full particulars.

W. H. BOSWORTH, Cleveland, Ohio COMMERCIAL BANK BUILDING

# "WHITNEY"

HAND MILLING MACHINE
THOUSANDS IN USE



# PROMPT DELIVERIES

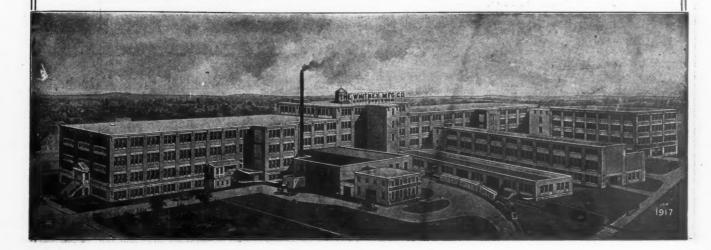
Owing to the increased demand for WHITNEY products we have recently completed another large addition to our factory. We have increased our production and are now prepared to make prompt deliveries on our Hand Milling Machine.

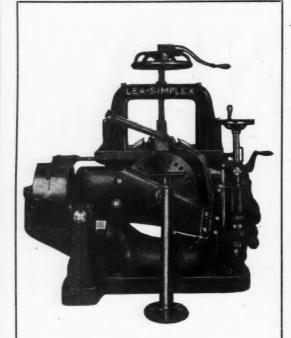
## NOTE THE SLIDING HEAD

The handiest machine for light milling, keyseating, profiling, die sinking, gear cutting, etc. Powerful and simple in operation. Simply send for Catalog D.

THE WHITNEY MFG. CO., Hartford, Conn. KEYS HAND MILLING MACHINES

FOREIGN AGENTS: Burton, Griffiths & Co., Ltd., London. Fenwick Freres & Co., Paris.





Price \$450 F. O. B. DAYTON

# FOR SALE

# No. 18 Lea-Simplex Cold Metal Saw

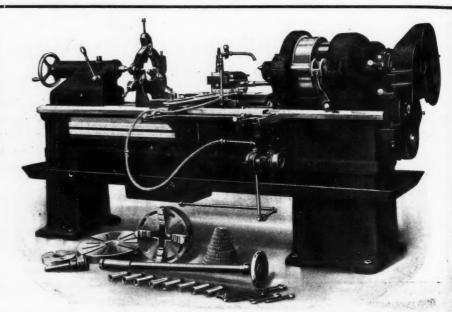
Manufactured by The Earle Gear and Machine Company, Philadelphia, Pa., complete with extra swivel block. Capacity 5" to 7" rounds and 6½" squares; an extra circular saw, type "BB"; serial number 1-46-11; perfect working order, practically good as new; belt driven.

For Sale by

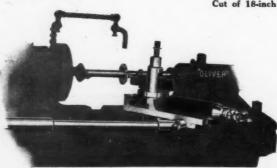
The Patterson Tool & Supply Co. Dealers in Machinery, Tools and Supplies DAYTON, OHIO, U. S. A.

# OLIVER ENGINE LATHES

Built for your work, arranged with various Tool Room Attachments, Belt or Motor Drive, with or without Chip and Oil Pan Pump, etc. Any length of bed to suit your particular needs.



Cut of 18-inch Tool Room Lathe Equipped with Taper, Draw-in and Relieving Attachments



Relieving Attachment Doing Busines

Engine Lathes—26-inch, 18-inch, 16-inch. Turret Lathes—16-inch. Screw Machines—2½-inch. Speed Lathes—12-inch.

OLIVER MACHINERY CO.
No 7 Coldbrook St. GRAND RAPIDS, MICH.

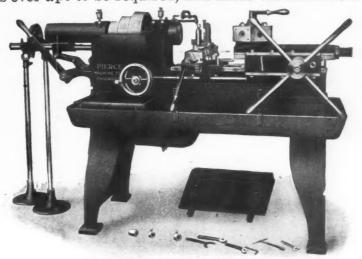
# Accuracy, Speed, and Unusual Range

The Pierce Turret Screw Machine in operation is one of the speediest and most convenient machines of its kind on the market. We have made the "Pierce" rigid and strong, provided more power than is ever apt to be required, and made the machine a

joy for the operator to handle. Spindle is carefully machined and hardened, has minimum overhang and is free from vibration regardless of speeds or class of work. Turret is rigidly constructed and automatically locked, directly under the cutting tool, when indexed.

Actual capacity is 1 1/16" x 8". In every important detail the "Pierce" is of greater dimensions than any other machine of similar capacity.

Complete description on request.

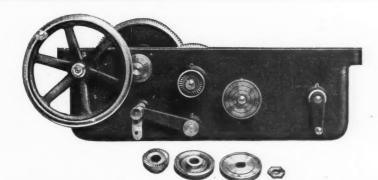


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ACHINE

Chicago, Ill., U.S.A.

HIGH GRADE TURRET MACHINER



to Feed the Carriage Against Heavy Cuts is Provided in Our Large Lathes

The above front view of apron partly dismantled shows construction of positive, toothed clutch (no frictions employed). The arrangement of the discs which carry the shearing pin is also shown. This shearing pin will break before the all-steel gearing will give way.



LARGE SWING LATHES BUILT IN 30", 36" 42", 48", 54" AND 60" SIZES

THE HOUSTON, STANWOOD & GAMBLE COMPANY CINCINNATI, U. S. A.

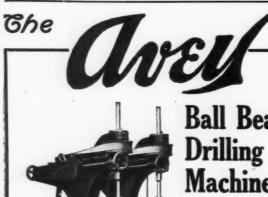
Hill, Clarke & Co., Inc., Boston Sherritt & Stoer Co., Philadelphia William K. Stamets, Pittsburgh

The Vonnegut Machinery Co., Indianapolis
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# S-T-E-R-L-I-N-G



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Sizes, Speeds, Capacities to suit each specific job

> High Speeds Clean Holes

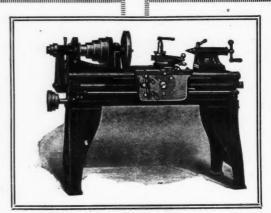
Our No. 3 Machine provides maximum speeds for work up to 1½-inch.

Our No. 1/2 machine for light work may be run at 12,000 r. p. m.

Other Sizes for Intermediate Work

Real manufacturing means specializing. Get the right machine.

The Cincinnati Pulley Machinery Co. CINCINNATI



S IMPLICITY in construction yet embodying all necessary features and backed up by perfect workmanship is what we offer in a

13-14-15-INCH SWING

You Need One in Your Shop for Certain Jobs

The Sebastian Lathe Co.

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# NO ADJUSTMENT

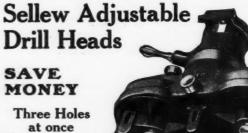


Ask for the circular

Manufactured by

ROCKFORD TOOL CO.

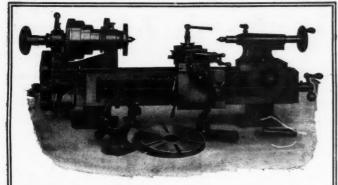
Rockford III.



instead of one.

Write for details

SELLEW MACHINE TOOL CO. Pawtucket, R. I., U. S. A.



# Wade 8" Precision Lathe

This lathe is designed for tool room, experimental and scientific work-for use wherever close accuracy is of prime importance. Nothing but the best in design and construction; only honest values go-for the Wade is built to take a permanent place in the machine tool field.

A strong feature is the quick change gear mechanism which provides for any thread from 12 to 120 per inch. Other features include a set of eleven spring chucks, two face plates, ground tool-steel bearings and draw-in type spindle, covered gears, etc.

Complete description on request

# WALTER H. WADE

Boston, Mass.

AGENTS: T. Crowther & Co., Boston, Mass. L. R. Meisenhelter Machinery Co., Philadelphia, Pa. E. A. Kinsey Co., Cincinnati, Ohio. International Commercial Co., New York, for Russia. Alfred Herbert, Ltd., Corentry, England. Charles Churchill & Co., Ltd., London, Eng.

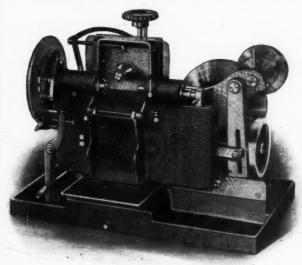
# **BLOMQUIST-ECK**



AGENTS: Northern Mchy. Co., Minnea Minn. Strong, Carlisle & Hammond Co., C land, Ohio. Essley Mchy. Co., Chicago, Ill.

203 St.ClairAve., N.E. CLEVELAND, OHIO

# The Waltham 4" **Precision Gear Cutter**



A profitable little machine for the shop that makes small gears and fine pitch pinions. The "Waltham" is automatic in operation, has all working parts protected and is a speedy producer of accurate work. When cutter slide is in cutting position and cut in progress, it is tightly clamped; clamp is released on return stroke so slide may be lifted for indexing.

Complete description on request.

#### Waltham Machine Works **Newton Street** WALTHAM, MASS.

Small Thread Millers, Gear Cutters and other small Automatic Machines



# **Burnishing Up-to-Date**

The modern idea of burnishing small metal parts—the most in the shortest time—is developed to the last notch by the Abbott Tumbling Barrel process. Hand polishing turns out one piece at a time, Abbott polishing—hundreds. Finish is perfectly clean and uniform, secured without injury to the work. And it's particularly cheap in labor—one operator handling four or five machines.



We'll gladly burnish samples of your work free and estimate on costs.

THE ABBOTT BALL COMPANY (ELMWOOD)

ARTFORD CONN.

# SecondHand

# Machinery, Tools and Accessories

NEW, REBUILT AND



USED MACHINERY

# USED MACHINERY

#### BORING MACHINES

No. 1 Beaman & Smith hor., double head. 2 spindle Beaman & Smith hor. 24" Bullard vert., 2 heads. 30" Bullard vert., 1 head.

#### DRILLS

4" Henry & Wright, B.B., sensitive. spindle Foote-Burt, P.F. spindle Gardam sensitive. spindle Barr sensitive. spindle Gardam. 6 spindle Gardam. 28" Blaisdell sliding head. 36" Prentice Bros., upright. 36" Blckford sliding head. 4' Blckford plain radial. 4' Blckford full universal radial.

#### GRINDERS

No. 6 Bryant, internal.
No. 1 Norton univ., C.&T.
No. 4 Springfield planer type surface.
No. 5 Rivett, on stand.
No. 200 Heald ring.
No. 3½ Van Norman radial.
No. 4—12 x 60 Landis universal.
No. 2 Garvin hole.
12 x 60 Diamond Surface. No. 2 Garvin hole. 12 x 60 Diamond Surface. 12 x 30 Landis plain.

#### LATHES

15 x 8 Hamilton, plain rest, T.A. 16 x 8 Porter C.R., P.C.F. 16 x 6 Automatic threading. 18 x 6 Reed C.R., P.C.F. 18 x 8 Lodge & Shipley C.R., P.C.F. 18 x 8 American C.R., Q.C.T.A.

18 x 8 Rahn-Mayer C.R., P.C.F., chuck. 20—18 x 8 L. & S. 3-step, Q.C.

26 x 14 Gleason C.R., P.C.F. 5-22 x 10 L. & S. selective head. 30 x 10 Gleason, swivel rest. 36 x 14 Pond, C.R., P.C.F.

11 x 5 Barnes, C.R., P.C.F.

-42 x 12 F. & S. gap, motor drive.

#### MILLERS

No. 3 Reed plain. No. 13 Brainerd universal. No. 2 Garvin universal . No. 31/2 Garvin plain. 25 Lincoln pattern, assorted. Nos. 1 and 2 P. & W. hand. No. 12 B. & S. plain, belt feed. Grant Mfg. Miller.

#### PLANERS

24 x 24 x 6 Wheeler. 26 x 26 x 5 Pond.

#### SCREW MACHINES

21" Gisholt Turret Lathe. 21" Gisholt Turret Lathe.

18 x 7 Fay & Scott universal turret.

1" Smurr & Kamen, wire feed.

3—2 x 24 Jones & Lamson.

2—24" Gisholt, turret lathe.

3/4" Rivett, collet chucking attachme.

1/2" National Acme automatic.

1/2" P. & W. automatic.

3/4" Cleveland automatic.

20" J. & L. geared head.

20—2" Cleveland automatics. attachment.

#### MISCELLANEOUS

No. 1 Baker Bros. Keyseater.
30 ton Watson-Stillman bending mch.
675 lb. P. & W. board drop hammer.
14" Steptoe shaper.
16" Rochester shaper.
24" Hendey shaper.
4" Espen-Lucas saw.
26 x 10 Cincinnati gear cutter.
2—No. 1 Slate pinion cutters.

# HENRY PRENTISS & COMPANY, Inc.

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ROCHESTER, N. Y.

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Warehouse: 439 Communipaw Avenue, Jersey City, N. J.

# Second-Hand Tools

1—3/8 Cleveland Automatic. 4—5/8 Automatic Screw Machines.

3—3/4 Hartford Automatics. 5—13/8 Hartford Automatics. 5—2" Cleveland Automatics. 2—2" Davis & Egan Automatics.

-21/4 Gridley Automatic M.D. -11/2 x 6 Gray Screw Ma-

chines. -24 x 24 x 6 American Planer.

1-32 x 32 x 8 S. H. New Haven Planer.

-40 x 36 x 10 S. H. New Haven Planer.

x 42 x 16 D. H. Gray Planer.

1—Grindstone and Frame.

# The Cincinnati Planer Co.

CINCINNATI, OHIO

## FOR SALE

-3' Pratt & Whitney Vertical Sur-face Grinder with magnetic chuck. -5" x 48" P. & W. Plain Cylindrical Grinder.

-No. 2 Bath Universal Grinder. -12" x 36" Landis Plain Grinders. -No. 13 B. & S. Automatic Gear

No. 13 B. Cutter.
No. 3 B. & S. Automatic Gear

-No. 3 B. & S. Cutter. -30" Eberhardt Bros. Automatic Gear Cutter.
30" Old Style Brainers Automatic

Gear Cutter. 12" Gleason Single Tool Gear Gen-

-12" Gleason Single Tool Gear Generators.
-Lees Bradner Thread Millers.
-Reed Plain Milling Machines.
-No. 3 Brown & Sharpe Plain Milling Machine.
-No. 4-B Becker Vertical Millers, new.
-No. 3 Bristol Vertical Millers, new.
-14" x 5' Reed Engine Lathes,

-14" x 5' Reed Engine Lathes, R. & F. -14" x 6' Rockford Engine Lathe. -14" x 6' Flather Engine Lathes,

14" x 6' Flather Engine Lathe, new.
16" x 7' Oliver Engine Lathe, new.
16" x 8' CISCO Engine Lathe, new.
18" x 8' Davis Engine Lathe, new.
D.B.G.
20" x 6' Florence T

20" X 6 Florence Full State Lathe.
-20" X 8' Bullard Chucking Lathe.
-20" Cincinnati Type "B" Double Head Traverse Head Shaper, 10', new. -15" x 30" Cincinnati Open Side Shaper, new.

BROWNELL MACHINERY CO. PROVIDENCE, R. I.

## For Sale, Immediately, Electrical Equipment

2 Elevators, complete, two and three ton capacity, with 20 and 30 H.P. Crocker-Wheeler motors.
2 Switches, various sizes.
12 Lighting Transformers.
2 Remek Transformers.
3 Type "f" Auto Transformers.
14 Current Transformers.
6 Conduit Series Transformers.
10 Miscellaneous Transformers.
10 Miscellaneous Transformers.
10 Marble Slabs.
10 Slateries of Conduit Oil Switches, three and six units.
11 Meters—Watt Meters—Volt Meters—Watt Hour Meters, etc.

and six units.

17 Meters—Watt Meters—Volt Meters—
Hour Meters, etc.
Numerous other items in electrical equipment.
Want to sell in one lot—write at once for complete list if interested.

The Goodyear Tire & Rubber Co., Akron, Ohio

# FOR SALE **Shell Making Machines**

For Immediate Delivery

64-6" Shell Making Machines, with all attachments.

25-9.2 and 12" Shell Making Machines, some arranged for motor drive, and others for belted drive.

For further particulars inquire of

The Cleveland Machinery & Supply Co. CLEVELAND, OHIO



# The Only Re-Manufacturing Plant in the World, 55,000 Sq. Ft. of floor space

TURRETS—Latest M	lodels	S
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- 25—21" Gisholts, 2-step, 5" belt,  $3\frac{1}{2}$ " hole.
  25—21" Gisholts, motor arrangement,  $3\frac{1}{2}$ " hole.
  15—24" Gisholts, 3-step, 4" belt,  $4\frac{1}{4}$ " hole.
  40—24" Gisholts, 2-step, 6" belt, 6" hole.
  42—24" Gisholts, motor arrangement, 6" hole.
  4—3-A Warner & Swasey.

## ENGINE LATHES—Latest Models

- 24—22" x 8' Hamilton, D.B.G., C.R., Semi-Q.C.G. 5—22" x 8' Hamilton, D.B.G., turret tool post. 7—22" x 10' Hamilton, D.B.G., C.R., Semi-Q.C.G. 2—22" x 10' Hamilton, D.B.G., turret tool post. 20—22" x 10' Davis, D.B.G., C.R., Q.C.G.

#### VERTICAL BORING MILLS

- 1—30" Baush. 1—32" Rogers.

- 1—36" Brown & Sharpe Chucking. 1—42" Colburn, 2 hds. 1—51" Baush, 2 hds.

## RADIALS

- -2½' Fosdick.
- 2—2½' Mueller. 1—2½' Dreses.
- Prentice.
- -3' Mueller.

#### 1-31/4' Gang.

- 1—4' Niles Full Universal. 3—5' Niles Semi-Universal.

### PLANERS

- 1—22" x 22" x 5' Flather. 1—22" x 22" x 6' American. 1—24" x 24" x 4' Gray.

# 1—24" x 24" x 4 Gray. 2—24" x 24" x 5' Gray. 1—24" x 24" x 6' Cincinnati. 1—24" x 24" x 10' Lodge & Davis. 1—26" x 26" x 6' American. 1—30" x 30" x 10' Powell, 4 hds. 1—32" x 32" x 8' Gray, 2 hds.

Your money back, if you Our Guarantee:return machine within 30 days from date of shipment, freight prepaid. No excuses necessary.

Our new "Green List" just out, describes the above machines and hundreds of others. Write for one.

HILL, CLARKE & CO. of CHICAGO 625 Washington Blvd. CHICAGO, ILL., U. S. A.

- 4—22" x 8' Davenport, D.B.G., turret tool post.
  8—24" x 10' Lodge & Shipley, D.B.G., C.R., Q.C.G.
  8—24" x 10' Lodge & Shipley, Selective Gd. Hd., C.R.
  11—26" x 10' American, D.B.G., C.R., Q.C.G.
  2—25" x 10' American, D.B.G., carriage turret.
  19—26" x 12' Putnam, carriage turret, Semi-Q.C.G.
  9—26" x 12' Putnam, C.R., Semi-Q.C.G.
  2—26" x 12' Wickes, D.B.G., ,C.R. Semi-Q.C.
  10—28" x 10' Niles, Bement, Pond, Q.C.G.
  4—28" x 14' Lodge & Shipley, Select. Gd. Hd., C.R., carriage turret.
- carriage turret.
- 3--30" x 16' Lodge & Shipley, Select. Gd. Hd., C.R., carriage turret.
- 11-40" x 18' Pittsburgh Triple Geared, Q.C.G.

  - 1—32" x 32" x 10' Gray, 2 hds. 1—76" x 48" x 18' Wood Woodward &

#### Powell, 4 hds. PRESSES

- 1-No. 30 Perkins Inclinable.
- 1—No. 5 Niagara Geared. 1—No. 5 Consolidated.

- 1—No. 20-U Ryerson Punch.
  3—No. 73½ Bliss S. S. Trimming.
  1—No. 23½-B Niagara Toggle.
  1—Long & Allstater Geared Punch.
  1—No. 17 Williams & White Double
- End Punch.

#### MILLERS

- 1-No. 3 Brainard Plain.
- 1-No. 20 Oesterlein Universal.
- 1-No. 11/2 Brown & Sharpe Universal.
- 1-No. 25 Becker Plain.
- 1-No. 2 Cincinnati Universal.
- 1-No. 5 Schuchardt & Schutte Plain.
- 1-No. 3 Hendey Plain.
- 1-60" x 48" x 8' Ingersoll Slab.
- 1-Beaman & Smith, 2 vert. hds., 1 horiz. hd.
- 1-No. 2 Beaman & Smith Combination.

#### GEAR CUTTERS

- 1-No. 1 S. & S. Hobber, spiral.
- 1—No. 12 B. & S., spur and bevel. 1—24" Fellows Gear Shaper.

- 2-No. 3-26" Cincinnati Spur.
- 1—36" Fellows. 1—36" Gleason Gleason Former, spur and bevel.
- 1-84"-96" Gleason Planer, spur and



# NEW AND USED MACHINE TOOLS

#### IN STOCK FOR IMMEDIATE DELIVERY

RADIAL DRILLS (Used) 1-3' Bickford Plain Radial, Gear Box Drive.

THREAD MILLER (Used) 1—No. 3 Lees-Bradner (used one month)
MILLING MACHINES (New)

—No. 3 Rockford Hand Miller.

—U. S. Plain Hand Millers (Whitney type).

—Standard Hand Millers (Whitney type).

MILLING MACHINES (Used)

2—No. 2 Garvin Hand Millers, Lincoln type.
3—No. 1 Steptoe Hand Millers with vise and arbor.
1—No. 3 Cincinnati Plain Miller.

SHAPERS (Used)
1—20" Queen City B.G. (like new).

SCREW MACHINES (New)

3—No. 0 Foster Plain Head, 9/16 wire feed capacity.

1—No. 2 Foster Plain Head, 11/16 wire feed capacity.

2—No. 4 Foster Geared Fr. Head, 19/16 wire feed capacity.

1—No. 6 Foster Geared Fr. Head, 21/16 wire feed capacity.

1—No. 140 Wells (7/8 capacity). 1—No. 2½ Garvin (17/16 capacity).

SCREW MACHINES (Used)

1—1/2 Pratt & Whitney Automatic Screw Machine. 1—Foster No. 4 Motor Driven Screw Machine. 1—No. 52 Acme 4-spindle, 3/4" capacity automatic.

GRINDERS (New)

-Capital Internal Grinder, capacity 3/16" to 2 x 2.
-Greenfield Universal Grinder.

-No. 1 Wilmarth & Morman Surface Grinder.

-Wilmarth & Morman No. 2 Full Automatic Surface. -No. 190 Wells Tool and Cutter Grinder.

-Dumore Portable Electric.

GRINDERS (Used)

No. 190 Wells.

1-No. 1 Landis Universal.

POWER SQUARING SHEAR (Used)

-60" Niagara Power Squaring Shear, capacity 1/8 stock.

BENCH LATHES (New)

2—No. 5½ Sloan & Chace, Comp. slide, 3 speed, c/s 10 col. 1—Ames Compound Slide, 3 speed, c/s 10 collets.

LATHES (New)

LATHES (New)
2—13 x 6 Worcester, P.C., C.R.
1—14 x 6 Hamilton, Q.C., C.R., Sgl. B.G.
3—16 x 8 Flather, Q.C., C.R., Dbl. B.G.
2—18 x 8 Hamilton, Q.C., C.R., Sgl. B.G.
1—20 x 6 Rahn-Larmon, Q.C., C.R., Dbl. B.G.
1—20 x 10 New Haven, P.C., C.R., Dbl. B.G.
1—26 x 10 Lodge & Shipley, Q.C., C.R., Dbl. B.G.

LATHES (Used)

1—12 x 5 Seneca Falls, P.C., C.R.

1—14 x 8 Davis, Q.C., C.R., with chuck.

1—18 x 8 Davis, Q.C., taper attachment, pan bed.

1—20 x 10 Jones & Lamson, P.C., C.R.

1—20 x 12 Greaves-Klusman, Q.C., C.R., taper attachment.

1—28 x 10 Hamilton, Q.C., C.R.

1-16 x 6 Lodge & Shipley Geared Head.

DRILL PRESSES (New)

-10" Sensitive Bench Drill Presses with chuck.

3—14"U. S. Sensitive Drills.
2—20" Buffalo B.G. self-feed automatic stop.
2—20" Barnes plain lever and worm feed.
2—20" Barnes B.G., self-feed automatic stop.
3—20" Champion B.G. self-feed automatic stop.

-2-spindle No. 32 A Reed Sensitive

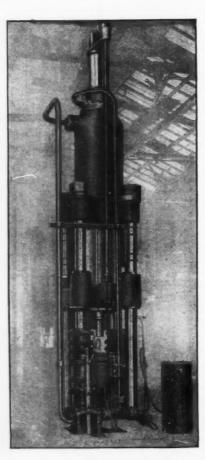
DRILL PRESSES (Used)

Sgl. Spindle Sipp High Speed.

-20" Excelsior B.G. Auto. Feed. -25" Hamilton B.G. Sliding Head. -23" Snyder B.G. Automatic Feed.

1-24" Barnes Sliding Head.

HOMER STRONG, Successor to Strong & Hery Company ROCHESTER, N. Y. U. S. A.



# FOR SALE

# Two350-TonVertical Hydraulic Presses

UP to 6" H. E. Shell Forgings PRODUCTION - - 5" Forgings, 3,000 in 20 hours

# Immediate Delivery

Including pumps, motors, accumulator, valves, underground and overhead piping, fittings, single and double holder die blocks, and all other accessories for completé units, ready for operation, except heating furnaces.

These units are two of four used for forging H. E. shell blanks. Operated less than six months. In firstclass condition.

Also offer for sale complete units for machine finishing 4.5", 5" and 6" H. E. shells.

For detailed description, price, term, etc., address

THE UNION SWITCH & SIGNAL CO. **SWISSVALE** PENNSYLVANIA, U.S.A.

# W. F. DAVIS MACHINE TOOL

CHICAGO, ILL., 549 W. Washington Blvd. CLEVELAND, O., 508 Leader News Bldg. CINCINNATI, OHIO, 1018 Union Central Life Bldg. NEW YORK CITY, Singer Bldg.

## BORING MACHINES-VERTICAL

1-30" Colburn, one turret head.
1-34" Rogers, one turret head, September de-

livery. -34" Gisholt, including motor. -36" N.-B.-P., one plain and one swivel head. -36" B. & S., one turret head. -New 42" Putnam, two heads, November de-

livery.
1—53° N.-B.-P., two swivel heads.
1—72° Niles, two swivel heads.
1—New 8' Bickford, December delivery.

#### BORING MACHINES-HORIZONTAL

1—Lucas, 2¾" bar.
1—Hoefer Horizontal Driller and Borer, with
111/16" spindle; vertical adjustment, 46";
horizontal adjustment, 46"; size of table,
33" x 48".
2-spindle Beaman & Smith, 3¾" bar. Page 48,
G. of G. 1907 Cat.

#### BULLDOZERS

1—New No. 4 Garrison (same as No. 4 Williams-White).

# White). 1-No. 7 Ajax, 20" stroke. 1-No. 7 High Speed Ajax, 16" stroke.

COMPRESSORS-AIR 1-8"  $\times$  8" Curtis, belt driven. 1-10"  $\times$  10"  $\times$  10" Single Cylinder Smith-Valle, 4—10" x 10" x 10" Single Cylinder Smith-Valle, steam driven.

1—10" x 12" Chicago Pneumatic, belt driven.

1—10 x 16½" x 13" Peerless, cross compound, steam driven.

1—22"—13" x 16" Ingersoll-Rand, motor driven.

1—Ingersoll-Sargent Duplex, 8 x 14½ x 8".

1—Ingersoll-Sargent, steam driven, 345 cu. ft.

1—Cincinnati, cross compound, two stage, 790 cu. ft.

#### CUTTING-OFF MACHINES

2-No. 00 Brown & Sharpe. 1-2" capacity Warner & Swasey. 4-3½" Hall. 10-4½" Williams. 3-4" Curtis & Curtis.

### DRILLING MACHINES-RADIAL

2—New No. 3 American, plain, cone drive. 3—New 3' Americans, sensitive tapping attachment.
7—New 3' Prentice, July delivery.
1—New 3' Mueller, plain, speed box drive.
1—New 3'/4' Mueller, cone drive, July delivery.
1—New 3'/4' Western Drill, 86" circle.
2—4' Mueller, plain, speed box drive.
1—3' Bickford, plain, speed box drive.
1—5' Bickford, gear drive.
1—5' American, plain, motor drive.
1—5' Spindle, arm does not raise and lower, hand feed.
1—5' Fosdick, plain, cone drive, tapping attachment.

## DRILLING MACHINES-HEAVY DUTY

tachment. 6' Baush, plain, cone driver.

Solid steel.

-No. 3 Colburn, plain, table.

-No. 3 Colburn, plain, table.

-No. 3 Foote-Burt, 44" swing, 3½" capacity in solid steel.

No. 310 Baker, single pulley drive, late type.

DRILLING MACHINES-MULTIPLE SPINDLE

holes, 30" circle.

1-No. 24 Baush, 12 spindle, capacity 1%"
holes, 30" circle.

1-No. 24 Baush, 12 spindles.

1-Gardam, 12 spindle, capacity 3%" holes, 14" square. 1—14-spindle Baush, capacity 1" holes, 36" circle. circle.

1—No. 11 Pratt-Whitney, 16-spindle, cap. 10 spindles, ¼" cap.

#### GEAR CUTTING MACHINES

1—New 6" Standard Gear Cutter, Spur.

1—12" G. & E. Gear Hobber.

1—12" Gleason Bevel Gear Planer.

1—16" Gleason Bevel Gear Planer.

1—16" Bilgram Bevel Gear Generator.

1—20" Grant-Lee Gear Hobber.

1—No. 1 20" Schuchardt & Schutte Gear Hobber. ber.

1-22 x 8 G. & E. Spur and Bevel Cutter.

1-24 Fellows Gear Shaper.

1-24 x 8 G. & E., for spur and bevel.

1-26 x 10 Cincinnati, spur gears only.

1-New 30 Flather, spur gears only.

3-36 Fellows Gear Shapers.

1-No. 3 Brown & Sharpe Auto. Gear Cutter, Spur.

Spur.

# GRINDERS—UNIVERSAL, FOR CUTTERS, DRILLS, REAMERS, ETC.

1—New Norton No. 1.

1—New Wilmarth & Morman, style B X.

1—No. 1 Cincinnati.

1—Now Walker No. 2, outfit K (capacity 9" x 26").

8—No. 180 Wells.

# GRINDING MACHINES—CYLINDRICAL—PLAIN

TRINDING MACHINES—UTRINDICAL—
PLAIN

1—No. 11 (6" x 36") Brown & Sharpe.

1—6" x 48" Pratt & Whitney.

1—New No. 12 (8" x 26") Brown & Sharpe.

1—10" x 50" Norton.

1—New 10 x 72 Norton, plain.

1—No. 16 (10" x 72") Brown & Sharpe.

20—12" x 24" Modern, self-contained.

6—12" x 36" Modern, self-contained, motor or belt driven.

6—12" x 48" Modern, self-contained, motor or belt driven.

1—16" x 46" Landis, with crank grinding.

1—12 x 33 Landis, rebuilt.

1—18" x 96" Brown & Sharpe.

1—New 10" x 36" Landis. Immediate.

# GRINDING MACHINES—CYLINDRICAL—UNIVERSAL

1-No. 1 Fraser, with surface grinding attach-1-No. 1 Fraser, with surface shaded ment.

1-No. 1½ (10" x 30") Landis.

1-No. 2½ (10" x 36") Bath.

1-No. 2 (9" x 20") Bath.

1-No. 2 New Walker, 9" x 26".

1-No. 2 New Walker, 9" x 26".

1-10" x 42" Modern.

1-No. 2 (12" x 30") Brown & Sharpe.

1-No. 2 (12" x 30") Brown & Sharpe.

1-New No. 2 Morse Cap. 12" x 30", universal, December delivery.

1-No. 3 (12" x 40") Brown & Sharpe.

1-12" x 42" Landis.

#### GRINDING MACHINES-INTERNAL

#### GRINDERS-CYLINDER

1-No. 27 Brown & Sharpe. 1-No. 60 Heald, single pulley drive.

#### GRINDERS-DISC

1-No. 14 Besly. 1-New No. 17 Gardner (Pattern Makers).

## GRINDING MACHINES-RING

1-No. 200 Heald. 1-No. 210 Heald.

## GRINDING MACHINES-EDGE

1-No. 374 Safety Emery Wheel Co.

GRINDING MACHINES-SURFACE U-No. 1 Diamond, capacity 12" x 12" x 24", automatic.

- New No. 2 Reid (same as B. & S.).

1-22" x 12" x 60" Springfield, planer type, automatic.

- New No. 1 Wilmarth & Morman.

#### GRINDING MACHINES-DUPLEX

1—No. 5 Bath, suitable for grinding cylinders, pistons, piston rings, etc., 16" feed, swivel table, water pump.

### GRINDING MACHINES-FACE

1-Diamond Face Grinder, 4' travel, 14" wheels.

#### HAMMERS-POWER, FORGING

1—40-lb. Bradley Helve. 1—150-lb. Bradley Helve, upright.

### HAMMERS-BOARD LIFT. DROP

1-400-lb. Billings & Spencer. 1-2000-lb. Chambersburg.

#### HAMMERS-STEAM, FORGING

1-New 600-lb. Bell. 1-New 3000-lb. Bell, September delivery.

#### \* KEYSEATERS

2-No. 0 Mitts & Merrill.
1-No. 2 Mitts & Merrill, motor driven.
1-60° stroke Compton-Knowles Broacher,
6-New 12 x 4 Shepard, reverse head.
8-New 12 x 5 Shepard, reverse head.
3-New 12 x 6 Shepard, reverse head.

#### LATHES-MANUFACTURING-NOT SCREW CUTTING

13—No. 3 X Reed-Prentice, semi-automatic.
14—Reed-Prentice Shell Lathes for 4" or 18-lb.
American shells.
60—14" x 6' Reed Stud and Bolt.
5—16' x 8' Fairbanks-Morse, heavy duty.
70—New Simplex, 16" x 8'.
14—16 x 8 Simplex, single pulley drive.
22—18" x 8' Battle Creek, heavy duty.
5—20" x 8' Merschon.
50—20" x 10' Hindman, high duty.
12—21" x 8' LeBlond, quick change, with attachment for grooving and facing both ends of shells, with air cylinders and mandrels for 5" shells.

#### LATHES-ENGINE

LATHES—ENGINE
6—New 12 x 4 Shepard reverse head.
8—New 12 x 5 Shepard reverse head.
3—New 12 x 6 Shepard reverse head.
1.—14" x 6' Bradford, taper attachment.
2.—16" x 6' LeBlond, pan bed, quick change gears, taper attachment.
1.—18" x 8' L. & S., geared head, taper.
1.—18 x 10 Hendey, quick change gear, 14" chuck.
3.—18" x 9' Chard.
1.—New 19" x 8' LeBlond, heavy duty.
22—20" x 8' Lodge & Shipley, quick change gear. 1—New 19" x 8' LeBlond, heavy duty.
22—20" x 8' Lodge & Shipley, quick change gear.
7—New 20" x 8' American, heavy duty.
9—22" x 10' Putnam, oil pan, turrets.
4—24" x 10' Reed.
2—24" x 12' S. & B.
1—24" x 14' Lodge & Shipley, patent head.
4—24" x 14' American, quick change.
3—New 28' x 12' Boye & Emmes.
1—26" x 24' New Haven.
4—New 28" x 12' Boye & Emmes.
1—28" x 18' S. & B.
5—New 30" x 14' Boye & Emmes.
1—36" x 15' Fifield, 36 x 16".
8—New 38" x 12' Pittsburgh pattern.
1—36" x 15' Fifield, 36 x 16".
8—New 36" x 24' Putnam, triple geared.
1—38 x 19' Steptoe, single back gear.
1—24" 48' x 22' McCabe, double spindle.
1—48 x 27' x 9" Betts, triple back gear.
1—New 66" x 30' Putnam, December delivery.

#### LATHES-TURRET

5—2 x 24 Jones & Lamson. 5—3 x 36 Jones & Lamson. 18—6A Potter & Johnson. 2—21 Gisholt.

# MILLING MACHINES—KNEE TYPE—UNIVERSAL

UNIVERSAL

1-New No. 1 Kempsmith.

1-No. 1½ Hendey-Norton.

1-No. 2 Kempsmith, back geared.

1-No. 2 New Cincinnati.

2-No. 2½ LeBlond, September delivery.

2-No. 3-H LeBlond, September delivery.

1-No. 3 Cincinnati, single pulley drive, high power, vertical attachment.

1-New No. 4 LeBlond Heavy Duty. Immediate.

#### MILLING MACHINES-KNEE TYPE-PLAIN

MILLING MACHINES—KNE
1—No. 0 Pratt & Whitney.
3—New No. 1 Rockford.
2—New No. 1 Kempsmith.
1—½ American.
1—Mew No. 2 Rockford.
1—No. 3 LeBlond.
1—No. 3 Cincinnati.
1—No. 4 Garvin.

#### MILLING MACHINES-VERTICAL

4—New No. 4 B Becker. 1—No. 2 New Cincinnati. 2—No. 5 Becker.

#### MILLING MACHINES-PLANER TYPE

1—No. 2 Beaman-Smith.
2—Ingersoll Slab Millers, working surface of table 60" x 20".
1—No. 4 Beaman & Smith, vertical spindle, open side, working surface of table 120" x 24", removable housing on one side.

#### PLANERS

PLANERS

1—24" x 24" x 6' Gray, one head on cross rail.

1—26" x 26" x 8' Gray, one head on cross rail.

1—30" x 30" x 8' Gale Planer, one head.

1—30" x 30" x 8' Whitcomb, one head.

1—30" x 30" x 12' Powell, high speed, one head.

1—36" x 36" x 12' Powell, high speed, one head.

1—36" x 36" x 12' New Haven, one head.

1—36" x 36" x 9' Sellers, four heads.

2—New 36" x 36" x 12' Woodward & Powell, two heads on cross rail, one side head, October delivery.

1—36" x 36" x 14' Sellers, four heads.

1—42" x 10' Hewes & Phillips, one head on rail, one side head.

1—42" x 10' Hewes & Phillips, one head on aid, one side head.

1—42" x 10' Hewes & Phillips, one head on aid, one side head.

1—42" x 10' Hewes & Phillips, one head on aid, two side heads.

1—50" x 14' Powell, one head.

1—72" x 72" x 26' motor drive, Betts, four heads.

## SCREW MACHINES AUTO.

3-No. 51 National Acme. 2-No. 52 National Acme. 2-No. 53 National Acme.

#### SHAPERS

1—New 16" Springfield.
1—16" Motor Driven, Rockford.
2—New 24" Milwaukee.
1—New Barker 24".
3—New 24" Steptoe. Back Gear.



# **Second Hand Machines**

Four and one-half inch bar horizontal boring machine. 20" Prentice Bros. lever feed drill. 24" Sibley, sliding head drill, B.G., P.F. 20" Hoefer three-spindle gang, B.G., P.F.

20" Barnes four-spindle gang, one B.G., three P.F., one tapping. No. 413 Baker Bros. heavy pattern fourspindle gang.

16" Brown & Sharpe spur and bevel gear

16" Brown & Sharpe spur and bevel gear cutter.
 26" Brown & Sharpe spur gear cutter.
 36" x 12" Gould & Eberhardt vertical cutting type spur gear cutter.
 12" x 24" Modern plain grinder, self-contained, fine condition.

Landis universal grinder (small).

No. 1 Baker Bros. keyseater. 16" x 8" Bradford lathe, compound rest. 21" x 10' Bradford lathe, compound rest.

x 10' LeBlond lathe, compound rest, turret on carriage. x 56" x 26' Bement planer, four 56"

1—1/2" x 9" Acme wire feed screw machine, power feed turret.
34" Lodge & Davis shaper.

# Marshall & Huschart Machinery Co.

17 S. Jefferson St. CHICAGO, ILL.

915 Chemical Bldg. ST. LOUIS, MO.

# **Immediate Delivery**

24" x 10' Springfield Engine Lathe.

24" x 10' Springfield Engine Lathe.
9" x 4' Star Engine Lathe.
No. ½ AVEY High-speed Ball-Bearing Sens. Drills.
No. 1 BAKER BROS. High-Speed Drill.
12" x 32" LANDIS Plain Grinder.
No. 3 GARVIN Cutter and Surface Grinder. No. 3 GARVIN Cutter and S Grinder. 10" x 50" Norton Plain Grinder.

10" x 50" Norton Plain Grinder.
36" Bickford Plain Radial.
3" Stover Pipe Machine.
21/4" x 24" WARNER & SWASEY Hollow Hexagon Turret Lathe.
No. 6 Warner & Swasey Turret Screw Machines.
31/2' Prentice Bros. Plain Radial.
4' Mueller Plain Radial.
7' OHL Bending Brake.
No. 2 BATH Linyersal Grinder 9" x

No. 2 BATH Universal Grinder, 9" x 20".

2 COCHRANE-BLY Die Filing

Machine.

8" FOSTER-KIMBALL Plain Head Screw Machine.

No. 11½ HIGLEY Cold Saw.

16" Barker Crank Shaper.

No. 3 Barber-Colman Gear Hobbing Machine.

58" CLEVELAND Automatic Screw Machines (2).

# THE E.L. ESSLEY MACHINERY CO.

551-557 West Washington Boulevard CHICAGO, ILLINOIS

# Factory and Mill Supply Co.

137 Oliver Street, BOSTON, MASS.

One Baush Plain Radial Drill, 6' arm, cone

One Bickford Radial Drill, with tapping at-tachment. 3' arm, single pulley drive.

Two Pratt & Whitney Plain Cylindrical Grinders, capacity 6"x 48", in excellent condition. ers, capacity 6"x 48", in excellent condition.

One Springfield Machine Tool Co., Cylindrical Grinder, capacity 12" x 96".

One Flather Automatic Spur Gear Cutter, capacity 26" x 8", excellent condition.

One Brown & Sharpe, ditto.

One 8" x 18" Modern Tool Co., Grinder, new.

One Diamond Machine Co., Roll Grinder, capacity 8" x 26".

pacity 8" x 26". One No. 5 Becker Vertical Milling Machine. One Kempsmith No. 1 Universal Milling Ma-

One No. 3 Cincinnati Plain Milling Machine.
One 26" x 7' Niles Planer, parallel drive, one head.

head.
One Wheeler Planer, 24" x 24" x 6' in excellent condition.

One Whitcomb Crank Planer, used less than two years, excellent condition.

One Hendey 28" Friction Shaper, motor driven, complete with motor, practically new,

One 2"x 24" Jones & Lamson Geared Head Turret Lathe, with bar and chucking equip-

One 2" x 24" Jones & Lamson Geared Head Turret Lathe, flat, two spindle, with com-plete chucking equipment, latest model, in excellent condition.

We also carry a large line of Shapers, Tur-et Lathes, Hand Screw Machines, Engine athes, Upright Drills, etc. Send us your equiries.

## WANTED AT ONCE

the following machines for export to Japan. Must be in first-class condition apan. Must be in first-class condition and subject to acceptance after inspec-

10-Radial Drills, 5' or over. Give reach

10—Radial Drills, 5' or over. Give reach of arm.
6—Slotters over 18".
4—Horizontal Borers.
8—Planers 48 × 48 or over. Give length of bed.
30—Lathes, 48" or over. Give length of bed.
3—Lathes, 60" or over.
20—Upright Drills, 2" capacity.
5—Boring Mills over 7'.
1—Boring Mill, 10'.
1—Boring Mill, 12'.
1—Boring Mill, 42".
1—Bending Roll for 1-½" material 13' wide.

wide. Bending Roll for 1-1/2" material 8' wide. -Straightening Roll for 1-1/2" material

1—Punch and Shear for punching 1-34" hole in material, 1-1/2" thick,

1-3/" hole in material, 1-1/2" thick, 36" gap.

1-Manhole Flanging Press for 1-1/2" material.

1-2000-ton Steam Hydraulic Press.

3-6' Universal Radial Drills.

PAYMENT CASH AGAINST SHIP-PING DOCUMENTS—STATE FULLY MAKE, AGE AND CONDITION.

ALSO—6 Miles 40-lb. Rails and 5 Miles 30-lb. Rails, complete with splice bars and boits. Second Hand; shipment in July.

#### BOX A138

Care MACHINERY, 148 Lafavette Street, N. Y.

# **ROUX 2 HEYBERGER**

180 Rue Lafayette, Paris

Solicit Offers for\_

Seamless Steel Tubes Lap Welded Boiler and Steam Tubes.

MACHINE TOOLS

Presses. Draw Benches for Tubes. Forging Machines for Nuts, Bolts and Rivets. PUNCHING and SHEARING MACHINERY Radial Drills. Steel and Iron Products.

# MODERN GRINDER Plain Cylindrical, Self Contained 12" x 36"

Used less than 10 days. Same as brand new machine. No use for it here, so offer to help someone else. First come first gets it. A great bargain for quick sale.

W. B. MARVIN MFG. CO. URBANA, OHIO

# WANTED

# Steam Driven Air Compressor

about 1,000 cu. ft., two stage. 90 to 100 pounds pressure, for 125 pounds boiler pressure. Non-condensing.

DRIVER-HARRIS CO. NEWARK, N. J.

# 3/4" GRIDLEY

Four Spindle Screw Machine, absolutely new -price \$1500.

Nearly new Brass Tube Polishing Machine - price \$500 for prompt acceptance.

STANDARD METAL MFG. CO. NEWARK, N. J.

# **BOARD DROP HAMMERS**

We offer subject to previous sale

2-Chambersburg 2000-lb. Model 20-BH

3-E. W. Bliss 800-lb. Model 1-2100 1-Billings & Spencer 400-lb. Model D

All are in good condition. B. & S. for other equipment.

The Union Switch & Signal Co. SWISSVALE, PA.

#### REBUILT TOO

GRINDERS: No. 1 Landis universal, 8" x 20".
Landis Crank Grinder, 16" x 66", with plain and crank heads.

MILLING MACHINES: No.1-1/2 Grand Rapids, back geared, plain.

No. 13 Brown & Sharpe

TURRET LATHES: Jones & Lamson, 3" x 36", geared sliding head, bar equipment. ment.
Pond 21" Rigid, geared head
Hamilton, 20" x 8', engine
turret, friction head, pan
bed, p. f. turret on bed.

GEAR CUTTERS: 22" x 5" x 6 pitch, Gould & Eber-hardt, spur and bevel. Whiton, 24", spur gears only

No. 13 Brown & S Manufacturing, plain. No. 3 Aurora, plain, single back gear.

No. 1-1/2 American, universal, complete.

4-spindle Warner & Swasey Valve Miller.

PLANER: 42" x 42" x 10' Hewes & Phillips, one rail head, one side head, fine.

SEND FOR COMPLETE LIST

FEDERAL MACHINERY SALES CO. 14 N. Jefferson Street, CHICAGO

# REBUILT MACHINES

heads. 5—Sellers 25 x 25 x 6'. 2—Sellers 25 x 25 x 8'.

2—Sellers 25 x 25 x 8'.

1—Putnam 24 x 24 x 8'6.

1—Putnam 25 x 25 x 10'.

1—Wheeler Heavy 30 x 30 x 8'6.

1—Lathe-Morse 24 x 24 x 5'6.

1—New Haven 24 x 24 x 7', 1—Wood Light 30 x 30 x 8', 1—Putnam 42 x 40 x 12'6,

GRINDERS

1—LeBlond Universal Tool & Cutter, power feed, same as new.

1—Bridgeport Plain Grinder, 16 x 36, 1—No. 1 Landis Universal Grinder.

1—No. 3 Landis Universal Grinder.

2—No. 6X Diamond Double Disc Grinders.

1—Ford-Smith Plain Grinder.

MISCELLANEOUS

1—Ford-Smith Plain Grinder.

AUTOMATICS

1—1" National Acme Double Belt Type.

1—19%" National Acme Double Belt Type.

1—No. 55 National Acme.

1—1" National Acme four-sningles

2—No. 54 National Acme four-sningles

1—Jenokes Band Tameral

Type.

1—No. 55 National Acme.

1—1" National Acme four-spindle.

2—No. 54 National Acme four-spindle.

3—2" Cleveland.

1—2½" Cleveland.

2—2½" Gridley Single-spindle Motors.

1—3½" Gridley Single-spindle Motors.

1—3½" Gridley Single-spindle Motors.

1—3½" Gridley Single-spindle Motors.

1—80" Putnam Wheel Lathe, double quartering.

1-Sellers 36 x 36 x 10' with 2 1-32 x 12' Draper Lathe, C.R., heads. 1-36 x 22' Fitchburg Lathe, C.R., P.C.F.

1-30 x 8' Fitchburg, C.R., P.C.F. 3-16 x 8' Putnam, C.R., taper. 6-18 x 8' Porter, C.R., semi-quick,

taper. 2—18 x 8' Davis, C.R., pan, pump,

taper. -16 x 8' Greaves-Klusman, C.R.,

pan, pump. 9—20 x 6' Perkins Plain Turning,

This is only a Partial List-Send for Full List.

# SIMMONS MACHINE CO., Inc.

New York: 1001 Singer Building Telephone Cortlandt 6575

Albany, N. Y.: 987 Broadway Telephone 4876 Main

# **List of Machinery for Disposal** On hand at Hudson Motor Car Plant

Prices are all f.o.b. Detroit -sale terms, one-third cash with order, balance to be paid against sight draft attached to bill of lading.

1—14" Fay Automatic Lathe, 14" swing over-shears and 10" under-carriage, turn to 10" in length, with equalizing drive face plate, self-contained taper attachment, oil pump, piping and change gears, (Practically new).

1-19" x 8' LeBlond Heavy Duty Lathe, complete with countershaft, etc. (Never been used). 7-19" x 6 LeBlond Heavy Duty Automobile Lathes, complete with turret tool posts. (Absolutely new.)

1-12-spindle Foote-Burt Valve Grinder. (Practically new.)

1-99 Defiance Bow Chucking Machine, complete with counter belt, shifting apparatus, 2 chucking heads, knives, guards, 1 cast iron master cam and necessary oil cups and wrenches. (Very little service.)

1-No. 598 Bow Shaping and Equalizing Machine, complete with all standard equipment. (Practically new.)

2-Bryant Chucking Grinders No. 6-one new and one used.

1-Bryant Chucking Grinder-double spindle. (New.)

1 Serial No. 16-249 Gisholt
Lathe,
Diam. of chuck, 24".
Swing over ways, 24".
Swing over carriage, 13%".
Traverse of turret, 50%".
Bore of spindle, 2½".
Diam. of heles in turret, 3".

Width of belt, 4".
Length overall, 3' 10".
Shipping weight (approx.) 8000 lb.
H. P. motor for main drive 4½.
H.P. motor, turret rapid traverse 1.

(This machine has been in use about a year and is in excellent condition.)

1—No. 6-K Disc Grinder, manufactured by Diamond Machine Co, Serial No. 5125. (Slightly used.)

1-No. 4 Gardner Disc Grinder. (Slightly used.)

1-2 x 8 Barnes Horizontal Drill, double spindle. (In excellent condition.)

# **HUDSON MOTOR CAR CO., Detroit, Mich.**



Niles 42" Vertical Boring Mill. One Swivel Head. One Fixed Turret Head. Four Jaw Chuck Table. Self-contained.

Fellows 36" Gear Shaper.

Bardons & Oliver No. 5 Screw Machine.

Jones & Lamson 2" x 24" Flat Turret Lathe. Geared Head.

Warner & Swasey No. 2-A Hexagon Turret Lathe. Cone Drive.

Greenfield No. 1 Plain Grinder, 5" x 12". Hydraulic Table Feed. Landis No. 24 Plain Grinder, 12" x 66".

#### HILL, CLARKE & CO., Inc. THE MACHINERY MERCHANTS

156 Oliver Street, BOSTON

136 Cedar Street, NEW YORK

# M. J. WALSH MACHINERY CO.

141 Sycamore St., Milwaukee, Wisconsin

# **Second-Hand Machines**

LATHES

1-18" x 10' Rahn-Meyers Lathe, 5-step cone, single back gear, compound and steady rest, hollow spindle, power cross feed, chuck fitted countershaft.

1-16" x 8' Porter Lathe, 4-step cone, single back gear, compound and steady rest, nower cross feed, countershaft.

2-No. 6 Warner & Swasey Screw Machines geared friction head, power feed to the turret.

1-No. 2 A Warner & Swasey Lathe with bar equipment.

1-14 x 6 Hamilton Style A Lathe oil pan, taper attachment and relieving and tapping attachments.

1-11" x 5' Fratt & Whitney Lathe, 5-step cone, single back gear, plain rest, countershaft.

2-No. 6 Fotter & Johnston Automatic Chucking Lathes, with all regular equipment regularly furnished for chucking.

1-3 x 36 All Geared Head Jones & Lamson Turret Lathe, with bar equipment, friction feed.

DRILLS

equipment, friction feed.

DRILLS

1-14"-4-Spindle Henry & Wright Ball Bearing Drill.
1-Small Knight Drilling Machine and for Milling.
1-20"-2-Spindle W. F. & J. Barnes Drill. One spindle arranged with wheel, lever and power feed. Other spindle with wheel, lever and power feed, back gears and tapping attachment. Both drills are the same.
1-24" All Geared Drive Barnes Drill.

PUNCH PRESSES
1-No. 19 Bliss Open Back Inclined Press, with stationary legs, automatic feed, back geared.
1-No. 3 A Willard Oper Back Inclined Press,
1-No. 1 Solid Back Heartley Press.
1-No. 472 Consolidated Double Crank Press, with 4 stroke,
1-Walsh Hand Screw Press.
1-Perkins Screw Press.
1-16 x 60 Landis Plain C. GRINDERS

1-16 x 60 Landis Plain Grinder with two sets of heads. One for plain cylindrical grinding. Other for crank grinding.
1-12 x 36 Cincinnati Plain Grinder Self Contained Counter,
1-No. 1 Landis Universal Grinder.
1-8 x 16 Ott Plain Grinder.

MISCRIFT AND ACCOUNTS OF THE PROPERTY AND ACCOUNTS OF THE PROPERTY

-No. 1 Landis Universal Grinder.

- 8 x 16 Ott Plain Grinder.

- 8 x 16 Ott Plain Grinder.

- 8 x 16 Ott Plain Grinder.

- No. 1½ Grand Rapids Back Geared Plain Mfg. Milling Machine.

- No. 1½ Grand Rapids Back Geared Plain Mfg. Milling Machine.

- Kempsmith Lincoln Type Milling Machine, Machine, Four Spindle Warner & Swasey Valve Milling Machine, fitted with No. 2 M.E.C. valve milling air chuck, countershaft.

- Hacine Power Hack Saw No. 1.

- Circle Shears.

- 62" Bertch Foot Power Gap Squaring Shears.

- 50" Peck, Stow & Wilcox Cornice Brake.

- 10' Dreis & Krump Bending Brake.

- 10' Peck Stow and Wilcox Roll, 4" diameter rolls.

- 7' Roll. 6½" Rolls.

- 20"Whiton Gear Cutter.

- ½" Acme Bolt Cutter.

- ½" Acme Bolt Cutter.

- No. 91 Forbes Pipe Machine, for hand and power, cuts off and threads from 2½" to 6" inclusive.

- No. 119 Bliss Thread Roller,

- Peerless Combination Punch and Shear.

- ½" Shuster Riveter.

- ½" Shuster Riveter.

- Bliss Deep Throat Punch and Riveting Machine.

DRILL PRESSES

1—3-spindle 8" Overhang Henry & Wright High Speed Drill.
3—12" Leland & Gifford High Speed Bench Drills.
5—20" Buffalo Plain Drill Presses.
4—6 spindle Fox High Speed Drill Presses.
2—4 spindle Fox High Speed Drill Presses.
1—3' Mueller Plain Radial Drill.
1—4' Bickford Radial Drill with T.A.
1—6' Mueller Plain Radial Drill.
1—16 spindle Natco Drill.

SHAPERS AND PLANERS

PRESSES

1—Waterbury-Farrell Straight Sided Geared Press with double cam knock-out.

1—No. 10 Perkins Drawing Press.

5—No. 2-W Biliss Wiring Presses.

1—800-lb. B. & S. Roll Board Hammer.

1—800-lb. P. & W. Roll Board Hammer.

1—50-lb. Scranton Belt Hammer.

1—25-lb. Bradley Helve Hammer.

AIR COMPRESSORS

1—24" Ohio H.D. B.G. Crank Shaper.
1—24" New Barker Crank Shaper.
1—24" Lodge & Davis Geared Shaper.
1—18" Hendey Geared Shaper.
1—16" Hendey Geared Shaper.
1—16" Garvin Shaper.
2—16" New Springfield B.G. Crank Shapers.



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ENGINE LATHES

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1—28 x 15 Putnam Standard Engine Lathe.

3—New 18 x 8 Springfield Engine Lathe.

3—New 18 x 8 Springfield Engine Lathe.

1—New 16 x 8 Springfield Engine Lathe.

1—18 x 6 Jones & Lamson Standard Engine Lathe.

1—16 x 8 Porter Standard Engine Lathe.

2—16 x 8 Reed Stud Lathes.

1—14 x 8 Sebastian Standard Engine Lathe.

1—14 x 6 Lodge & Shipley Engine Lathe.

1—14 x 6 Springfield Engine Lathe.

1—14 x 6 Sebastian Engine Lathe.

1—14 x 6 Sebastian Engine Lathe.

2—14 x 6 Van Werk Engine Lathe.

1—14 x 6 Sebastian Engine Lathe.

1—14 x 6 Van Werk Engine Lathe.

1—14 x 6 Van Werk Engine Lathe.

1—15 Seneca Falls Engine Lathe.

1—10 Seneca Falls Engine Lathe.

TURRET AND SCREW MACHINES

TURRET AND SCREW MACHINES

1-2/4 x 24 Jones & Lamson Flat Turret Lathe, S.G.H.

1-2 x 24 Jones & Lamson Flat Turret Lathe, cone head.

2-No. 6-A Potter & Johnson Automatic Lathes.

3-No. 4 Foster F.G. H. Hand Screw Machines.

2-No. 3 Foster F.G.H. Hand Screw Machines.

1-No. 5 Pierson F.G.H. Hand Screw Machine.

1-No. 4 Smurr & Kamen Hand Screw Machine.

4-New 14" Pierce Turret Lathes.

2-New 1 x 8 Pierce Hand Screw Machines.

2-2" Cleveland Automatic Screw Machines, jogger feed.

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MILLING MACHINES AND GRINDERS

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-No. 11/2 Knight Milling and Drilling Machines.

-No. 13 Pratt & Whitney Lincoln Type Milling Machine.

-No. 13/2 Garvin Plain Milling Machine.

-No. 2 Hendey Plain Milling Machine.

-Fox Hand Milling Machines.

-Garvin Hand Miller.

-No. 21/2 Bath Universal Grinder.

-No. 170 Wells Cutter Grinder.

-Mina Valley Universal Cutter Grinder.

-No. 0 Burke Bench Mills. (New.)

AIR COMPRESSORS

1—8 x 6 Westinghouse Steam Air Compressor.

1—16 x 18 x 12 Union Steam Pump Co., Steam Driven Air Compressor.

1—10 x 10 Ingersoll Sargent Belt Driven Air Compressor.

1—10 x 10 Clayton Belt Driven Air Compressor.

1—8 x 8 Fairbanks Morse Electrical Driven Air Compressor.

1—8 x 8 Gardner Single Belt Driven Air Compressor.

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16" x 8' Walcott.

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Four-spindle No. 1½ Foote-Burt Rail.

Four-spindle No. 2 Avey.

Two-spindle No. 2 Avey.

Two-spindle No. 2 Avey.

LATHES

No. 2 Consolidated plai

No. 5 Stiles & Parke B

SAWS

6" Atkins "Kwick-Kut."

7" High Duty Paragon.

SCREW MACHINES

PRESSES

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No. 5 Stiles & Parke B

SAWS

6" Atkins "Kwick-Kut."

7" High Duty Paragon.

SCREW MACHINES

TWO-spindle No. 2 Avey.

Two-spindle No. 2 Avey.

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6" x 32" Norton.

10" x 50" Norton. 10" x 30" Landis.

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No. 2 Brown & Sharpe, universal.

No. 2 2 Bath, universal.

No. 3 Oesterlein.

No. 12 Gardner, duplex disc. 24" Double Wet Tool. 20 x 11/2 Single Wet Tool. No. 200 Heald, ring.

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welding. No. 3 Standard 300-lb. belt drop.

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No. 7-H Becker, Lincoln Type. No. 00 Brown & Sharpe.

No. 8 Pratt & Whitney, hand.

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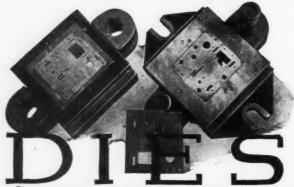
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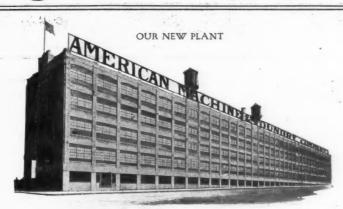
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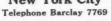


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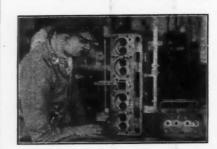


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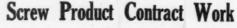
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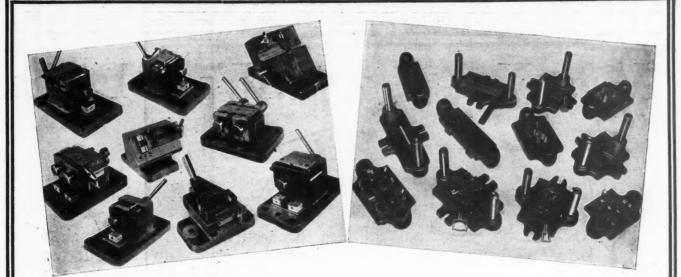
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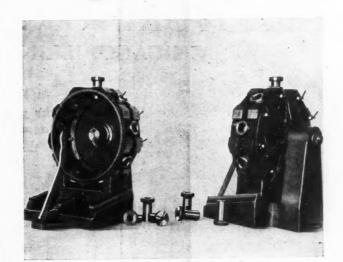
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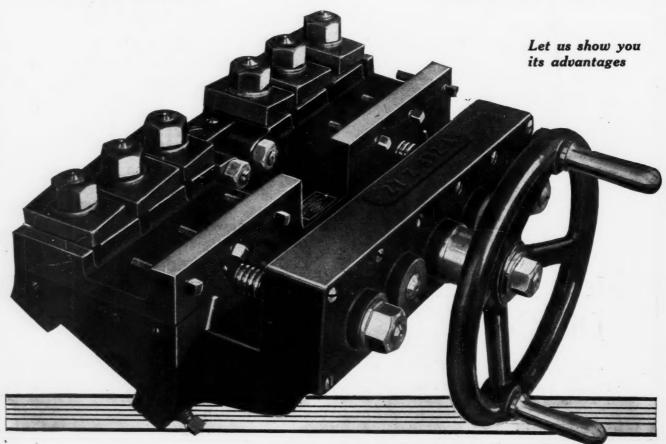
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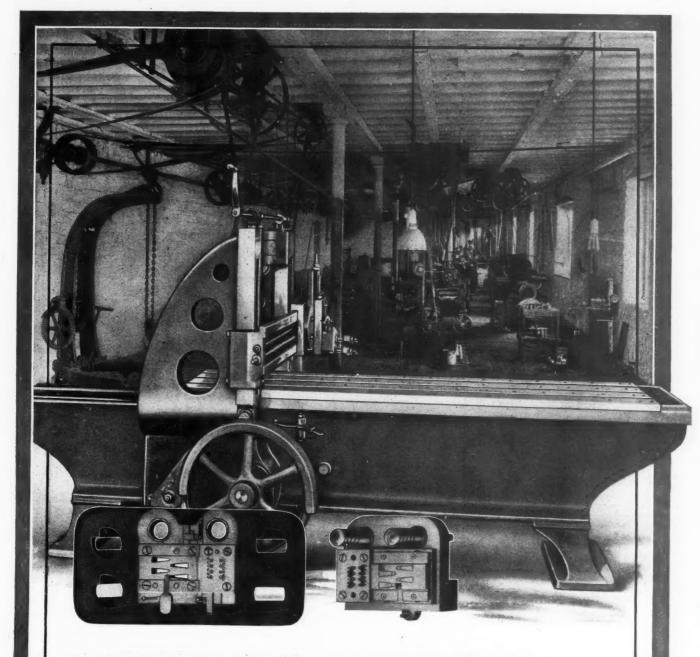
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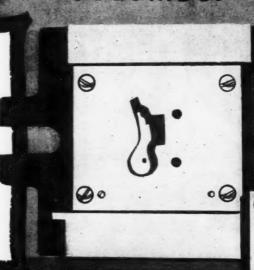


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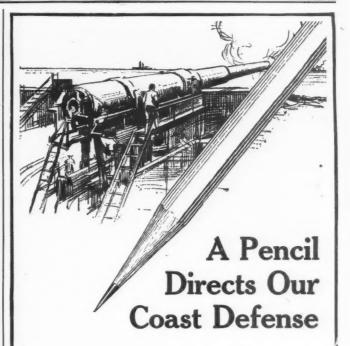
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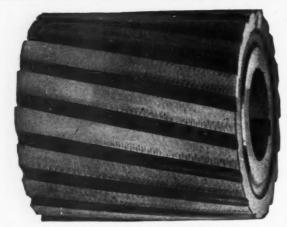
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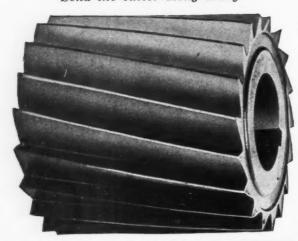
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Rockford Tool Co., Rockford, Ill.
Balls, Brass, Steel, Etc.
Abbott Ball Co., Emwood, Hartford, Conn.
Atlas Ball Co., Glenwood Ave. at 4th St., Philadelphia, Pa.
Auburn Ball Bearing Co., 33 Elizabeth St., Rochester,
N. Y.
Blum & Co., Julius, 510 W. 24th St., New York.
Frasse & Co., Inc., Peter A., 417 Canal St., New York.
Gwilliam Co., 253 W. 58th St., New York.
Hoover Steel Ball Co., Ann Arbor, Mich.
Metal Specialty Mfg. Co., Waterbury, Conn.
Rochester Ball Bearing Co., Inc., Rochester, N. Y.
S K F Ball Bearing Co., Hartford, Conn.

Kenffel & Esser Co., Hoboken, N. J.

Hoiler Tubes
National Tube Co., Pittsburgh, Pa.

Boile and Nut Machinery
Acme Mchy. Co., Cleveland, O.
Ajax Mfg. Co., Cleveland, O.
Foote-Burt Co., Cleveland, O.
Foote-Burt Co., Cleveland, O.
Greenfield Tap & Die Corp., Greenfield Tap & Die Corp., Greenfield Machine Co., Inc., Waynesbu ia, Pa.
Ball Bearing Co., 33 Elizabeth St., Rochester,

Bars, Boring See Boring Bara

See Boring Bars.

Bearings, Ball
Auburn Ball Bearing Co., 33 Elizabeth St., Rochester,
N. Y.
Ball & Roller Bearing Co., Danbury, Conn.
Bantam Ball Bearing Co., Bantam, Conn.
Bearings Co., of America, Lancaster, Pa.
Boston Gear Works, Norfolk Downs, Mass.
Fafnir Bearing Co., New Britain, Conn.
Gurney Ball Bearing Co., Jamestown, N. Y.
Gwilliam Co., 253 W. 58th St., New York.
Hese-Bright Mfg. Co., Front St. and Eric Ave.,
Philadelphis, Pa.
New Departure Mfg. Co., Bristol, Conn.
Norma Co. of America, 1790 Broadway, New York.
Rochester Ball Bearing Co., Inc., Rochester, N. Y.
S. K. F. Ball Bearing Co., Inc., Bothester, N. Y.
S. K. F. Ball Bearing Co., Thiladelphia, Pa.
Transmission Ball Bearing Co., Philadelphia, Pa.
Transmission Ball Bearing Co., Palmer St. and Kolmar
Ave., Chicago, Ill.

Bearing Mfg. Co., Palmer St. and Kolmar

Bearings, Roller
Ball & Roller Bearing Co., Danbury, Conn.
Bantam Ball Bearing Co., Bantam, Conn.
Gwilliam Co., 253 W. 58th St., New York.
Hyatt Roller Bearing Co., Newark, N. J.
Royersford Foundry & Mch. Co., 54 N. 5th St., Philadelphia, Pa.
Standard Roller Bearing Co., Philadelphia, Pa.

Belt Cement Schieren Co., Chas. A., 73 Ferry St., New York.

Belt Clamps Hoggson & Pettis Mfg. Co., New Haven, Conn.

Belt Dressing
Cling-Surface Co., 1018 Niagara St., Buffalo, N. Y.
Dixon Crucible Co., Joseph, Jersey City, N. J.
Graton & Knight Mfg. Co., Worcester, Mass.
Schieren Co., Chas. A., 73 Ferry St., New York.

Belt Fasteners, Metal, Leather, Etc. Bristol Co., Waterbury, Conn. Graton & Knight Mg. Co., Worcester, Mass. Greene, Tweed & Co., 109 Duane St., New York. Schieren Co., Chas. A., 73 Ferry St., New York.

Belting, Leather Chicago Rawhide Mfg. Co., 1301 Elston Ave., Chicago, Ill. Graton & Knight Mfg, Co., Worcester, Mass. Schieren Co., Chas. A., 73 Ferry St., New York.

Belts, Endless Woven
Gilmer Co., L. H., Tacony, Philadelphia, Pa.

Blowpipes, Gas
Buffalo Dental Mfg. Co., Buffalo, N. Y. Blueprint Filing Cabinets See Cabinets, Filing.

Blueprint Machines and Paper Buckeye Engine Co., Salem, O. Keuffel & Esser Co., Hoboken, N. J.

National Tube Co., Pittsburgh, Pa.

Bolt and Nut Machinery
Acme Mchy. Co., Cleveland, O.
Ajax Mfg. Co., Cleveland, O.
Foote-Burt Co., Cleveland, O.
Greenfield Tap & Die Corp., Greenfield, Mass.
Landis Machine Co., Inc., Waynesboro, Pa.
National Acme Co., Cleveland, O.
National Mchy. Co., Tiffin, O.
Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,
Philadelphis, Pa.
Standard Engineering Co., Ellwood City, Pa.

Bolts and Nuts
National Acme Co., Cleveland, O.
Toledo Screw Products Co., Toledo, O.

Books, Technical Industrial Press, 148 Lafayette St., New York.

Boosters
General Electric Co., Schenectady, N. Y.
Westinghouse Elec. & Mfg. Co., East Pittsburgh, Pa.

Boring and Drilling Machines,
Horizontal
Barnes Co., W. F. & John, 231 Ruby St., Rockford,
Ill. Ill.

Beaman & Smith Co., Providence, R. I.

Date-Brewster Mehy. Co., Inc., 545 W. Washington

Blvd., Chicago, Ill.

Fosdick Mch. Tool Co., Cincinnati, O.

Gisholt Mch. Co., Madison, Wis.

Lucas Machine Tool Co., Cleveland, O.

Manning, Maxwell & Moore, Inc., 119 W. 40th St.,

N. Y. U. S. Ball Bearing Mig. Co., Fasher.

Ave., Chicago, Ill.

Besly & Co., Chas. H., 120-B N. Clinton St., Standard Alloys Co., Pittsburgh Pa.

Link-Belt Company, Chicago, Ill.

Lunca Bearing Co., Buffalo, N. Y.

Standard Alloys Co., Pittsburgh Pa.

Standard Alloys Co., Buffalo, N. Y.

Boring and Drilling Machines, Vertical

Sellers & Co., Inc., Onc. Vis., Date W., Malson, Mass.

Cabinets, Filing

Economy Drawing Table Co., Boston, Mass.

Cabinets, Filing

Economy Drawing Table Co., Toledo, O., Keuffel & Esser Co., Hoboken, N. J.

Cabinets, Tool

Armstrong Bros. Tool Co., 313 N. Francisco Ave., Nies-Bement-Pond Co., 3639 N. Lawrence

Philadelphia, Pa.

Rockford Drilling Mach. Co., Rockford, Ill.

Sellers & Co., Inc., Wm., Philadelphia, Fa.

Britanium Alloy Mig. Co., New Bedford, Mass.

Sellers & Co., Inc., Wm., Philadelphia, Fa.

Britanium Alloy Mig. Co., New Bedford, Mass.

Tool Co., Bridgeport, Conn.

Bearings, Lineshaft
Hyatt Roller Bearing Co., Newark, N. J.

Bearings, Oilless
Arguto Oilless Bearing Co., 145 Berkley St., Junction, Philadelphia, Pa.
Bound Brook Oil-less Bearing Co., Bound Brook, N. J.

Bearings, Ring Oiling
Cresson-Morris Co., Philadelphia, Pa.
Link-Belt Company, Chicago, Ill.
Royersford Foundry & Mch. Co., 54 N. 5th St., Philadelphia, Pa.
Cleink Mch. Tool Co., Bridgeport, Conn.
Colburn Mch. Tool Co., Franklin, Pa.
Glick Mch. Tool Co., Clereland. O.
Footick Mch. Tool Co., Clereland. O.
Glick Mch. Tool Co., Madison, Wis.
Moline Tool Co., Madison, Wis.
Moline Tool Co., Moline, Ill.
NilesBement-Pool Co., 111 Broadway, New York,
Pedrick Tool & Mch. Co., 3639 N. Lawrence St.,
Philadelphia, Pa.
Cuint, A. E., Hartford, Conn.
Sellers & Co., Inc., Wm., Philadelphia, Pa.

Boring, Drilling and Milling
Machines, Horizontal
Beaman & Smith Co. Providence, R. I.
Cleveland Machine Tool Works, Cleveland, O.
Fosdick Machine Tool Co., Cincinnati, O.
Gisholt Mch. Co., Madison, Wis.
Landis Tool Co., Waynesboro, Pa.
Lucas Machine Tool Co., Cleveland, O.
Newton Mch. Tool Works, Inc., 23rd and Vine Sta.,
Philadelphia, Pa.
Niles-Bement-Pond Co., 111 Broadway, New York.
Rockford Drilling Mch. Co., Rockford, Ill.
Sellers & Co., Inc., Wm., Philadelphia, Pa.
Universal Boring Mch. Co. Hudson, Mass.

Universal Boring Mch. Co. Hudson, Mass.

Boring and Turning Mills, Vertical
American Tool Works Co., Gincinnati, O.
Bullard Mch. Tool Co., Bridgeport, Conn.
Cincinnati Planer Co., Cincinnati, O.
Colburn Mch. Tool Co., Franklin, Pa.
Gisholt Mch. Co., Madison, Wis.
Niles-Bement-Fond Co., 111 Broadway, New York.
Sellers & Co., Inc., Wm., Philadelphia, Pa.
Springfield Mch. Tool Co., 631 Southern Ave., Springfield, O.

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Boring Bars
Advance Tool Co., Cincinnati, O.
Armstrong Bros. Tool Co., 313 N. Francisco Ave.,
Chicago, Ill.
Beaman & Smith Co., Providence, R. I.
Gisholt Mch. Co., Madison, Wia.
Pedrick Tool & Mch. Co., 3639 N. Lawrence St.,
Philadelphia, Pa.
Ready Tool Co., Bridgeport, Conn.
Underwood & Co., H. B., Philadelphia, Pa.

Boring Heads, Offset Marvin & Casler Co., Canastota, N. Y. Porter-Cable Mch. Co., Syracuse, N. Y. Waterston, J. M., Detroit, Mich.

Waterston, J. M., Detroit, Mich.

Boring Tools
Armstrong Bros. Tool Co., 313 N. Francisco Ave.,
Chicago, Ill.
Kelly Reamer Co., Cleveland, O.
Maxwell-Hutchcroft Co., Cleveland, O.
Morse Twist Drill & Machine Co., New Bedford, Mass.
O. K. Tool Holder Co., Shelton, Conn.
Ready Tool Co., Bridgeport, Conn.
Ready Tool Co., Woonsocket, R. I.
Western Tool & Mig. Co., Springfield, O.

Brazing Equipment
Buffalo Dental Mfg. Co., Buffalo, N. Y.
Chicago Flexible Shaft Co., 149 W. La Salle St.,
Chicago, Ill.
Ferro-Brazing Paste Co., 1423 Farragut Ave., Chicago,

Broaching Machines
Lapointe Co., J. N., New London, Conn.
Lapointe Mch. Tool Co., Hudson, Mass.

Bronze Bruting Brass & Bronze Co., 748 Spencer St., Toledo, O. Light Mfg. & Foundry Co., Pottstown, Pa. Lumen Bearing Co., Buffalo, N. Y. Titanium Alloy Mfg. Co., Buffalo, N. Y.

Buffers
Blount Co., J. G., Everett, Mass.
Bridgeport Safety Emery Wheel Co., Inc., Bridgeport, 

Bulldozers

Ajax Mfg. Co., Cleveland, O.
Bliss Co., E. W., 5 Adams St., Brooklyn, N. Y.
National Mehy. Co., Tiffin. O.
Watson-Stillman Co., 192 Fulton St., New York.
Williams, White & Co., Moline, Ill.

Burnishing Machinery
Abbott Ball Co., Elmwood, Hartford, Conn.
Baird Mch. Co., Bridgeport, Conn.
Globe Mch. & Stamping Co., Cleveland, O.
Metal Specialty Mfg. Co., Waterbury, Conn.

Metal Specialty Mfg. Co., Waterbury, Conn.

Bushings, Brass, Bronze, Etc.

Bound Brook Oil-less Bearing Co., Bound Brook, N. J.

Brown Engineering Co., 133 No. 3d St.; Reading, Pa.

Bunting Brass & Bronze Co.,, 748 Spencer St.,

Toledo, O.

Johnson Bronze Co., Newcastle, Pa.

Light Mfg. & Foundry Co., Pottstown, Pa.

Lumen Bearing Co., Buffalo, N. Y.

Titanium Alloy Mfg. Co., Buffalo, N. Y.

Walworth Mfg. Co., Boston, Mass.

Caliper Gauges
Williams & Co., J. H:, 61 Richards St., Brooklyn,
N. Y.

Calipers, Bow Brown & Sharpe Mfg. Co., Providence, R. I. Goodell-Pratt Co., Greenfield, Mass. Greenfield Tap & Die Corp., Greenfield, Mass. Starrett Co., L. S., Athol, Mass. Union Tool Co., Orange, Mass.

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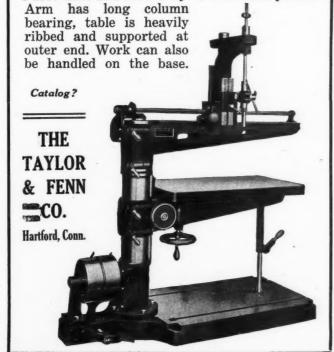
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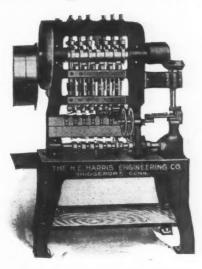
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Mass.

Brown & Sharpe Mig. Co., Providence, R. I.

Goodell-Pratt Co., Greenfield, Mass.

Slocomb Co., J. T., Providence, R. I.

Starrett Co. L. S., Athol, Mass.

Cams American Mch. & Foundry Co., 5520 Second Ave., Brooklyn, N. Y.

Brooklyn, N. Y.
Boston Gear Works, Norfolk Downs, Mass.
Garvin Mch. Co., Spring and Varick Sts., New York.
Rowbottom Mch. Co., Waterbury, Conn.

Cars, Industrial Chase Foundry & Mfg. Co., Columbus, O.

Cartridge Machinery Blackall, Frederck S., Woolworth Tower, New York. Case-hardening Kasenit Co., 11 Water St., New York. Meisel Press Mfg. Co., 948 Dorchester Ave., Boston, Mass. MRSS. & Co., J. H., 61 Richards St., Brooklyn, N. Y.

Case-hardening Compound Kasenit Co., 11 Water St., New York. Case-hardening Furnaces See Furnaces, Case-hardening.

Newman Mig. Co., Cincinnati, O.

Castings, Die or Die-Molded
Acme Die-Casting Corporation, Bush Terminal No. 5,
35th St. and 3rd Ave., Brooklyn, N. Y.
Doehler Die-Casting Co., Court and Ninth Sta.,
Brooklyn, N. Y.
Franklin Mig. Co., 738 Gifford St., Syracuse, N. Y.
Light Mig. & Foundry Co., Pottstown, Pa.
Lumen Bearing Co. Buffalo, N. Y.
Moberg, C. J., Inc., Mt. Vernon, N. Y.
Newman Mig. Co. Cincinnati, O.
Ohmer Fare Register Co. Dayton, O.
Phoenix Die-Casting Co., Syracuse, N. Y.
Stewart Mig. Co., Wells St. Bridge, Chicago, Ill.
Veeder Mig. Co., S9 Sargeant St., Hartford, Conn.
Castings, Iron and Steel

Castings, Iron and Steel Cresson-Morris Co., Philadelphia, Pa. West Steel Casting Co., Cleveland, O.

Castings, Nichrome Driver-Harris Co., Harrison, N. J.

Driver-Harris Co., Harrison, N. J.

Centering Machines

Hendey Mch. Co., Torrington, Conn.

Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,

Philadelphia, Pa.

Niles-Bement-Pond Co., 111 Broadway, New York.

Porter-Cable Mch. Co., Syracuse, N. Y.

Pratt & Whitney Co., Hartford, Conn.

Springfield Mch. Tool Co., 631 Southern Ave., Springfield. Springfield Mch. Tool Co., 631 Southern Ave., field, O. Wells & Son Co., F. E., Greenfield, Mass. Whiton Mch. Co., D. E., New London, Conn.

vention Mcn. Co., D. E., New London, Conn.

Centers, Planer and Miller
Bickford Mch. Co., Greenfield, Mass.
Cincinnati Planer Co., Cincinnati, O.,
Morse Twist Drill & Machine Co., New Bedford, Mass.
Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,
Philadelphia, Pa.

Chain Blocks
See Hoists, Chain, etc.

See Hoists, Chain, etc.

Chains, Driving, Etc.

Baldwin Chain & Mig. Co., Worcester, Mass.

Boston Gear Works, Norfolk Downs, Mass.

Diamond Chain & Mig. Co., 240 W. Georgia St.,

Indianapolis, Ind.

Frasse & Co., Inc., Peter A., 417 Canal St., New York.

Link-Belt Co., Chicago, Ill.

Morse Chain Co., Ethaca, N. Y.

Union Chain & Mig. Co., Seville, O.

Whitney Mig. Co., Hartford, Conn.

Woburn Gear Works, Woburn, Mass.

Checks, Time, Tool and Pay Matthews & Co., Jas. H., 3946 Forbes Field, Pitts-burgh, Pa. Noble & Westbrook Mfg. Co., Hartford, Conn. Schwerdtle Stamp Co., Bridgeport, Conn.

Schwerdite Stamp Co., Bridgeport, Conn.

Chucking Machines, Automatic

and Semi-Automatic

See also Lathes, Turret.
Cleveland Automatic Machine Co., Cleveland, O. Gisholt Mch. Co., Madison, Wis.
National Acme Co., Cleveland, O. New Britain, Conn.
Potter & Johnston Mch. Co., Pawtucket, R. I.
Pottering Machines, Multiple Spindle,
Automatic

New Britain Mch. Co., New Britain, Conn.

Chucks, Air

Salety Mneet Co., Springend, C., Standard Presed Steel Co., Philadelphia, Pa.

Counting Machines
National Counting Mch. Co., 39 Sargeant St., Hartiff Couplers, Hosse
Gene, Tweed & Co., 109 Duane St., N.
Ill.

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Gene, Tweed & Co., 119 Broadway, New York
Chicago, Ill.
Rivett Lathe & Grinder Co., Brighton, Boston, Mass.
Commutators

Commutators

Chucks, Air
Bardons & Oliver, Cleveland, O.
Garvin Mch. Co., Spring and Varick Sta., New York.
Hannifin Mfg. Co., Chicago, Ill.
Manufacturers Equipment Co., 175 N. Jefferson St.,
Chicago, Ill.

Chucks, Drill
Almod Mig. Co., T. R., 2 Maple Ave., Ashburuham,
Mass.
Clereland Twist Drill Co., Clereland, O.
Cushman Chuck Co., Hartford, Conn.
Detroit Twist Drill Co., Detroit, Mich.
Goodell-Pratt Co., Greenfield, Mass.
Greenfield Tap & Die Corp., Greenfield, Mass.
Horton & Son Co., E., Windsor Locks, Conn.
Accobs Mig. Co., Hartford, Conn.
McCrosky Reamer Co., Meadville, Pa.
Millers Falls Co., Millers Falls, Mass.
Modern Tool Co., 2d and State Sts., Erie, Pa.
Montgomery & Co. Inc., 104 Fulton St., New York.
Morse Twist Drill & Machine Co., New Bedford, Mass.
Narragansett Mch. Co., Providence, R. I.
National Twist Drill & Tool Co., Detroit, Mich.
Newman Mig. Co., Clincinnati, O.
Oneida National Chuck Co., Oneida, N. Y.
Skinner Chuck Co., New Britain, Conn.
Standard Tool Co., Clereland, O.
Swedish Gage Co., Inc., 16 W. 61st St., New York.
Trump Bros. Mch. Co., Willmington, Del.
Union Mig. Co., New Britain, Conn.
Waterston, J. M., Detroit, Mich.
Westcott Chuck Co., Oneida, N. Y.
Whiton Mch. Co., D. E., New London, Conn. Chucks, Drill Almond Mfg. Co., T. R., 2 Maple Ave., Ashburnham,

Chucks, Lathe, Etc.
Cushman Chuck Co., Hartford, Conn.
Gisholt Mch. Co., Madison, Wis.
Hardinge Bros., Inc. Berteau & Ravenswood Aves.,
Chicago, Ill.
Hoggson & Pettis Mfg. Co., New Haven, Conn.
Horton & Son Co., E., Windsor Locks, Conn.
McCrosky Reamer Co., Meadville, Pa.
Montgomery & Co., Inc., 104 Fulton St., New York.
Newman Mfg. Co., Cincinnati, O.
Oneida National Chuck Co., Oneida, N. Y.
Rivett Lathe & Grinder Co., Brighton District, Boston,
Mass.
Skinner Chuck Co., New Britain, Conn.

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Skinner Chuck Co., New Britain, Conn.
Thomas Elevator Co., 22 S. Hoyne Ave., Chicago, Ill.
Union Mfg. Co., New Britain, Conn.
Westcott Chuck Co., Oneida, N. Y.
Whiton Mch. Co., D. E., New London, Conn.

Chucks, Magnetic
D& W Fuse Co., Providence, R. I.
Heald Mch. Co., 20 New Bond St., Worcester, Mass.
Walker Co., O. S., Worcester, Mass.

Chucks, Planer
Cincinnati Planer Co. Cincinnati, O.
Cushman Chuck Co., Hartford, Conn.
Hoggson & Pettis Mfg. Co., New Haven, Conn.
Horton & Son Co., E., Windsor Locks, Conn.
Skinner Chuck Co., New Britain, Conn.
Union Mfg. Co., New Britain, Conn.

See Furnaces, Case-hardening.

Castings, Brass, Bronze and Aluminum
Light Mig. & Foundry Co., Pottstown, Pa.
Lumen Bearing Co., Buffalo, N. Y.
Newman Mig. Co., Clincinnati, O.
Titanium Alloy Mig. Co., Buffalo, N. Y.

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35th St. and 3rd Ave., Brooklyn, N. Y.
Doehler Die-Casting Co., Court and Ninth Sts.,
Brooklyn, N. Y.

Brooklyn, M. Y.

B III. rocunier, Wm. L., 549 Washington Blvd., Chicago, Ill. cully-Jones & Co., 647 Railway Exchange, Chicago, Ill.

Circuit Breakers

D & W Fuse Co., Providence, R. I.
General Electric Co., Schenectady, N. Y.
Westinghouse Elec & Mfg. Co., East Pittsburgh, Pa.

Clamps

Armstrong Bros. Tool Co., 313 N. Francisco Ave., Chicago, Ill.

Besly & Co., Chas. H., 120-B N. Clinton St., Chicago, Ill.

Westinghouse Elec & Mfg. Co., East Pittsburgh, Pa.

Conveyers, Gravity
Caldwell & Son Co., H. W., 17th St. & Western Ave., Chicago, Ill.

Link-Belt Co., Chicago, Ill.

Cotter Pins

Wittman & Barnes Mfg. Co. 1000 West 120th St.

Billings & Spencer Co., Hartford, Conn.
Brown & Sharpe Mfg. Co., Providence, R. I.
Goodell-Fratt Co., Greenfield, Mass.
Hammacher, Schlemmer & Co., 4th Ave. and 13th St.,
New York.
Hannifin Mfg. Co., Chicago, Ill.
Starrett Co., L. S., Athol, Mass.
Western Tool & Mfg. Co., Springfield, O.
Williams & Co., J. H., 61 Richards St., Brooklyn,
N. Y.

Clamps, Pipe National Tube Co., Pittsburgh, Pa.

Clocks, Watchmen's Hardings Bros., Inc., Berteau and Ravenswood Aves., Chicago, Ill.

Chicago, Ill.

Clutches, Friction, Etc.
Bicknell-Thomas Co., Greenfield, Mass.
Brown Clutch Co., Sandusky, O.
Brown Engineering Co., 133 No. 3d St., Reading, Pa.
Caldwell & Son Co., H. W., 17th St. and Western
Ave., Chicago, Ill.
Conway & Co., Cincinnati, O.
Cresson-Morris Co., Philadelphia, Pa.
Edgemont Mch. Co., 2700 National Ave., Dayton, O.
Johnson Mch. Co., Carlyle, Manchester, Conn.
Link-Belt Company, Chicago, Ill.
Moore & White Co., 2701-2737 N. 15th St., Philadelphia, Pa.
Reliance Gauge Column Co., 6008 Carnegie Ave.,
Cleveland, O.
Wood Sons Co., T. B., Chambersburg, Pa.
Collars, Safety

Collars, Safety
Bridgeport Safety Emery Wheel Co., Inc., Bridgeport,
Conn. Conn.
Brown Co., A. & F., 79 Barclay St., New York.
Link-Belt Company, Chicago, Ill.
Safety Emery Wheel Co., Springfield, O.
Standard Pressed Steel Co., Philadelphia, Pa.

Wagner Elec. Mfg. Co., St. Louis, Mo. Westinghouse Elec. & Mfg. Co., East Pittsburgh, Pa. Compound, Cleaning
Oakley Chemical Co., 26 Thames St., New York.

Compound, Cutting, Grinding, Etc.
Cataract Refining & Mfg. Co., Buffalo, N. Y.
Fiake Bros. Refining Co., 24 State St., New York.
Haws, Inc., Geo. A., 135 Front St., New York.
Oakley Chemical Co., 26 Thames St., New York.
Stuart & Co., Inc., D. A., 29 So. La Salle St., Chicago, III.

Compressors, Air and Gas
Chicago Pneumatic Tool Co., 1060 Fisher Bldg.,
Chicago, III.
Curtis Pneumatic Mchy. Co., 1568 Kienlen Ave., St.
Louis, Mo.
General Electric Co., Schenectady, N. Y.
Ingersoll-Rand Co., 11 Broadway, New York.
Worthington Pump & Mchy. Corp., 115 Broadway,
New York.

Carroll Engineering Co., Dayton, O. Columbus Die, Tool & Mch. Co., Columbus, O. Fox Gun Co., A. H., Philadelphia, Pa. Gisholt Mch. Co., Madison, Wis, Hanna Engineering Works, 1763 Elston Ave., Chicago, III.
Harris Engineering Co., H. E., Bridgeport, Conn.
Himoff Mch. Co., 45 Mills St., Astoria, N. Y.
Ingle Mch. Co., Rochester, N. Y.
Ingle Mch. Co., Rochester, N. Y.
Ingle Mch. Co., Providence, R. I.
Karsberg Mfg. Co., Providence, R. I.
Marvin Mfg. Co., W. B., Urbana, O.
Maute & Sons, J., Buffalo, N. Y.
Mehl Mch. Tool & Die Co., Roselle, N. J.
Meisel Press Mfg. Co., 948 Dorchester Ave., Boston,
Mass.

Mehl Mch. Tool & Die Co., Roselle, N. J.

Meisel Press Mfg. Co., 948 Dorchester Ave., Boston,
Mass.

Moore-Eastwood Mfg. Co., Dayton, O.

Nelson Tool Co., Inc., 781-788 R. 142d St., New York.

New Britain Mch. Co., New Britain, Conn.

North Side Tool Works, Dayton, O.

Ohmer Fare Register Co., Dayton, O.

Poole Engineering & Mch. Co., Baltimore, Md.

Rockford Metal Specialty Co., Bockford, Ill.

Sloan & Chace Mfg. Co., Ltd., Newark, N. J.

Slocum, Avram & Slocum Laboratories, Inc., 531 W.

21st St., New York.

Smalley-General Co., Bay City, Mich.

Solar Metal Products Co., Inc., Columbus, O.

S-P Mfg. Co., Cleveland, O.,

Steiner Bros., Lima, O.

Tatt-Peirce Mfg. Co., Woonsocket, R. I.

Taylor Mch. Co., Cleveland, O.

Taylor-Shantz Co., Rochester, N. Y.

T. C. M. Mfg. Co., Harrison, N. J.

Ulmer Co., J. C., Cleveland, O.

Urbana Tool & Die Co., Urbana, O.

Controllers

Controllers

Eck Dynamo & Motor Co., Belleville, N. J.

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Reliance Elec. & Eng. Co., 1056 Ivanhoe Road, Cleve-Eck Dynamo & Motor General Electric Co., Schenectady, N. 1. Reliance Elec. & Eng. Co., 1056 Ivanhoe Road, Cleve-land, O. Sprague Electric Works, 527 W. 34th St., New York Triumph Electric Co., Cincinnati, O. Westinghouse Elec. & Mfg. Co., East Pittsburgh, Pa.

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National Tool Co., Cleveland, O.
National Twist Drill & Tool Co., Detroit, Mich.
Pratt & Whitney Co., Hartford, Conn.
Standard Tool Co., Cleveland, O.
Starrett Co., L. S., Athol, Mass.
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Diamond Mch. Co., Providence, R. I.
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Hyatt Roller Bearing Co., Newark, N. J.
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Grant Mfg. & Mch. Co., N. W. Station, Bridgeport,

Conn. Veeder Mfg. Co., 39 Sargeant St., Hartford, Conn.

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National Counting Mch. Co., Chicopee Falls, Mass.
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National Tube Co., Pittsburgh, Pa.

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Brown Engineering Co., 133 N. 3d St., Reading, Pa.
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Nicholson & Co., W. H., 112 Oregon St., Wilkes-Barre, Pa.
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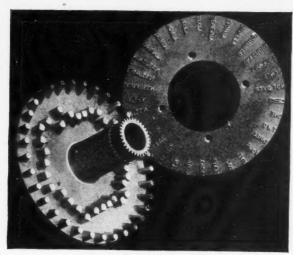
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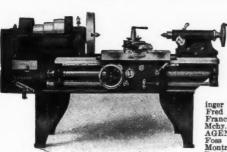
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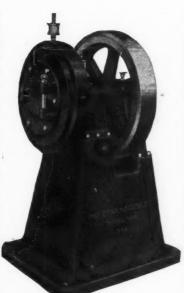
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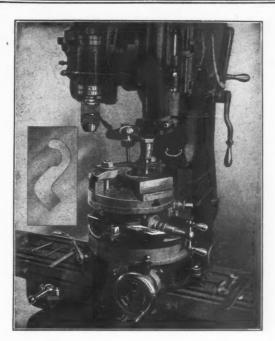


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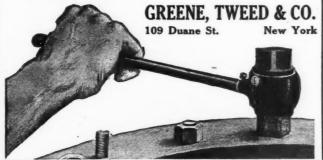
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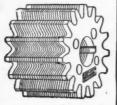
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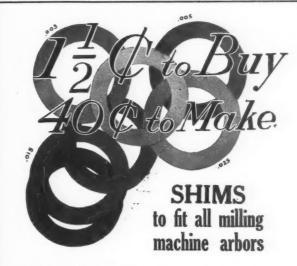
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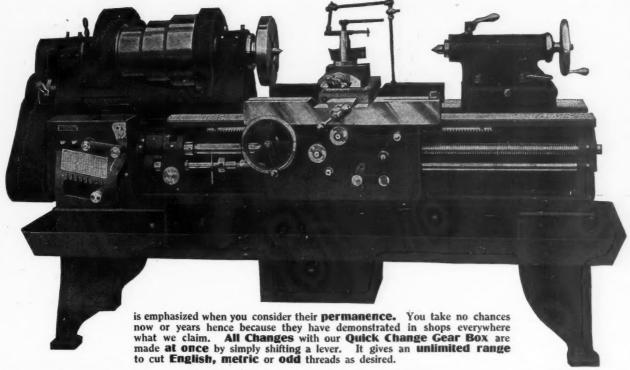
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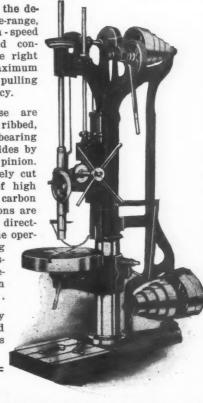
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Leather Belting, Round Schieren Co., Chas. A., 73 Ferry St., New York.

Levels
Goodell-Pratt Co., Greenfield, Mass.
Keuffel & Esser Co., Hoboken, N. J.
Starrett Co., L. S., Athol, Mass.
Lockers, Metal
Manufacturing Equipment & Eng. Co., Framingham,
Mass.

Lubricants
Besly & Co., Chas. H., 120-B N. Clinton St., Chicago, Il. Ill.
Cataract Refining & Mfg. Co., Buffalo, N. Y.
Dixon Crucible Co., Joseph, Jersey-City, N. J.
Fiske Bros. Refining Co., 24 State St., New York.
Haws, Inc., Geo. A., 135 Front St., New York.
Hosmer Co., G. A., Buffalo, N. Y.
Lumen Bearing Co., Buffalo, N. Y.
Oakley Chemical Co., 26 Thames St., New York.
Royersford Foundry & Mch. Co., 54 N. 5th St., Philadelphia, Pa. Boyersoru Funna, Pa.
delphia, Pa.
8 K F Ball Bearing Co., Hartford, Conn.
8 tuart & Co., Inc., D. A., 29 La Salle St., Chicago, n & Finch Co., 165 Broadway, New York.

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National Lathe Co., Cincinnati, O. 17" and 18".
Niles-Bement-Fond Co., 111 Broadway, New York.
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Pratt & Whitney Co., Hartford, Conn.
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Seneca Falls Mg. Co., 330 Fall St., Seneca Falls, N. Y. 9" to 16", inclusive.
Sidney Tool Co., Sidney, O. 17" and 19".
Simplex Mch. Tool Co., Hamilton, O. 16" to 32", incl. Smith Mfg. Co., Philip, Sidney, O. 13".
South Bend Lathe Works, South Bend, Ind. 13" to 24" inclusive.
Springfield Mch. Tool Co., Springfield, O. 14" to 36" inclusive.
Walcot Lathe Co., Jackson, Mich. 14" to 28", incl. Whitcomb-Blaisdell Mch. Tool Co., Worcester, Mass. 14" to 30", inclusive.
Walcot Lathe Co., Jackson, Mich. 14" to 28", incl. Whitcomb-Blaisdell Mch. Tool Co., Concinnati, O. 13".
Worcester Lathe Co., Worcester, Mass. 11", 13" and 16".

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Hill, Clarke & Co., Inc., Boston, Mass.
Hill, Clarke & Co., of Chicago, 625 Washington Blvd.,
Chicago, Ill.,
Manning, Maxwell & Moore, Inc., 119 W. 40th St.,
New York.
Marshall & Huschart Mchy. Co., 17 S. Jefferson St.,
Chicago, Ill.,
McDonough Mfg. Co., Eau Claire, Wis.
Motch & Merryweather Mchy. Co., Cleveland, O.,
Niles-Bement-Pond Co., 111 Broadway, New York.
Osgood Tool Co., J. L., Buffalo. N. Y.
Patterson Tool & Supply Co., Dayton, O.,
Simmons Mch. Co., 1001 Singer Bldg., New York,
Vandyck Churchill Co., 149 Broadway, New York,
Walls Tool Co., T. P., 75 Walker St., New York,
Young, Corley & Dolan, Inc., 115 Broadway, New
York.

Machinists' Small Tools
See Calipers, Hammers, Wrenches, Drills, Taps, etc.

Mallets, Rawhide Chicago Rawhide Mfg. Co., 1301 Elston Ave., Chicago, Ill.

Mandrels, Expanding and Solid See Arbors and Mandrels, Expanding and Solid. Marking Machines
Bickford Machine Co., Greenfield, Mass.
Grant Mfg. & Mch. Co., N. W. Station, Bridgeport, Conn.
Martin Mch. Co., Greenfield, Mass.
Noble & Westbrook Mfg. Co., Hartford, Com

Measuring Machines, Precision
Pratt & Whitney Co., Hartford, Conn.
Rogers Works, Inc., J. M., Gloucester City, N. J.
Swedish Gage Co., Inc., 16 W. 61st St., New York.

Metals, Bearing
See Bearings, Bronze, Babbitt, etc., and Bushings,
Brass, Bronze, etc.

Milling and Drilling Machines, Upright
Knight Mchy Co., W. B., 2019 Lucas Ave., St.
Louis, Mo.

Louis, Mo.

Milling Attachments
Adams Co., Dubuque, Iowa.
Becker Milling Machine Co., Hyde Park, Mass.
Brown & Sharpe Mig. Co., Providence, R. I.
Cincinnati Milling Machine Co., Oakley, Cincinnati. O.
Garvin Mch. Co., Spring and Varick Sts., New York.
Hendey Machine Co., Torrington, Conn.
Ingersoil Milling Machine Co., Rockford, Ill.
Kearney & Trecker Co. Milwaukee, Wis.
Kempsmith Mig. Co., Milwaukee, Wis.
Kempsmith Mig. Co., Milwaukee, Wis.
LeBlond Mch. Tool Co., E., K., Cincinnati, O.
Oesterlein Mch. Co., Cincinnati, O.
Porter-Cable Mch. Co., Syracuse, N. Y.
Pratt & Whitney Co., Hartford, Conn.
Rivett Lathe & Grinder Co., Brighton, Boston, Mass.
Rockford Milling Mch. Co., Rockford, Ill.
Seneca Falls Mig. Co., 330 Fall St., Seneca Falls,
N. Y.
Whitney Mig. Co., Hartford, Conn.

Milling Machines, Automatic

Milling Machines, Automatic Pratt & Whitney Co., Hartford, Con

Milling Machines, Bench
Ames Co., B. C., Waltham, Mass.
Carter & Hakes Co., Sterling Place, Winsted, Conn.
Hardinge Bros., Inc., Berteau and Ravenswood Aves.,
Chicago, Ill.
Rockford Milling Mch. Co., Rockford, Ill.
Sloan & Chace Mfg. Co., Newark, N. J.
Van Norman Mch. Tool Co., Waltham Ave., Springfield, Mass.

Milling Machines, Circular, Continuous Becker Milling Mch. Co., Hyde Park, Mass. Gould & Eberhardt, Newark, N. J.

Gould & Eberhardt, Newark, N. J.

Milling Machines, Hand
Adams Co., Dubuque, Iova.
Becker Milling Mch. Co., Hyde Park, Mass.
Bickett Mch. & Mfg. Co., Cincinnati, O.
Bickett Mch. & Co., Greenfield, Mass.
Biggs-Watterson Co., Cleveland, O.
Carter & Hakes Co., Sterling Place, Winsted, Conn.
Cleveland Milling Mch. Co., Cleveland, O.
Claveland Milling Mch. Co., Cleveland, O.
Claveland Milling Mch. Co., Rockford, Rockford Milling Mch. Co., Rockford, Ill.
Steptoe Co., John, Brighton, Cincinnati, O.
Van Norman Mch. Tool Co., Waltham Ave., Springfield, Mass. Steptoe Co., John, Brighton, Cincin Van Norman Mch. Tool Co., Walth field, Mass. Whitney Mfg. Co., Hartford, Conn.

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Whitney Mfg. Co., Hartford, Conn.

Milling Machines, Horizontal, Plain
Adams Co., Dubuque, Iowa.
Beaman & Smith Co., Providence, R. I.
Becker Milling Machine Co., Hyde Park, Mass.
Bilton Mch. Tool Co., Bridgeport, Conn.
Brown & Sharpe Mfg. Co., Providence, R. I.
Cincinnait Milling Mch. Co., Oakley, Cincinnait, O.
Cleveland Milling Mch. Co., Oakley, Cincinnait, O.
Cleveland Milling Mch. Co., Cleveland, O.
Garvin Mch. Co., Spring and Varick Sts., New York.
Gooley & Edlund, Inc., Cortland, New York.
Hendey Machine Co., Torrington, Conn.
Ingersoll Milling Machine Co., Rockford, Ill.
Kearney & Trecker Co., Milwaukee, Wis.
Kempsmith Mfg. Co., Milwaukee, Wis.
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Kempsmith Mfg. Co., Milwaukee, Wis.
LeBlond Mch. Tool Co., R. K., Cincinnati, O.
Newton Mch. Tool Co., R. K., Cincinnati, O.
Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,
Philadelphia, Pa.
. Niles-Bement-Pond Co., 111 Broadway, New York.
Oesterlein Mch. Co., Cincinnati, O.
Pratt & Whitney Co., Hartford, Conn.
Rockford Milling Mch. Co., Rockford, Iill.

Milling Machines, Hortzontal, Universal

Milling Machines, Horizontal, Universal
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Brown & Sharpe Mg. Co., Providence, R. I.
Cincinnati Milling Mch. Co., Oakley, Cincinnati, O.
Cleveland Milling Machine Co., Cleveland, O.
Hendey Machine Co., Torrington, Conn.

Kearney & Trecker Co., Milwaukee, Wis.
Kempsnith Mfg. Co., Milwaukee, Wis.
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Niles-Bement-Pond Co., 111 Broadway, New York.
Oestarlein Mch. Co., Cincinnati, O.
Rockford Milling Mch. Co., Rockford, Ill.
Rowbottom Mch. Co., Waterbury, Conn.
Van Norman Mch. Tool Co., Waltham Ave., Springfield, Mass.

Milling Machines, Lincoln Type
Beaman & Smith Co., Providence, R. I.
Becker Milling Mch. Co., Hyde Park, Mass.
Garvin Mch. Co., Spring and Varick Sts., New York.
Kempsmith Mfg. Co., Milwaukee, Wis.
Hendey Machine Co., Torrington, Conn.
Reynolds Pattern & Mch. Co., Massillon, O.
Van Norman Mch. Tool Co., Waltham Ave., Springfield, Mass.

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Milling Machines, Portable
Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,
Philadelphia, Pa.
Pedrick Tool & Mch. Co., 3639 N. Lawrence St.,
Philadelphia, Pa.
Underwood & Co., H. B., Philadelphia, Pa.

Milling Machines, Vertical
Adams Co., Dubuque, Iowa.
Beaman & Smith Co., Providence, R. I.
Becker Milling Machine Co., Hyde Park, Mass.
Brown & Sharpe Mfg. Co., Providence, R. I.
Cincinnati Milling Mach. Co., Oakley, Cincinnati, O.
Garvin Mch. Co., Spring and Varick Sis., New York.
Ingersoll Milling Mch. Co., Rockford, Ill.
Kearney & Trecker Co., Milwaukee, Wis.
LeBlond Mch. Tool Co., R. K., Cincinnati, O.
Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,
Philadelphia, Pa.
Niles-Bement-Pond Co., 111 Broadway, New York.
Van Norman Mch. Tool Co., Waitham Ave., Spring-field, Mass.

Milling Tools (Hollow Adjustable)

Milling Tools (Hollow Adjustable)
Geometric Tool Co., New Haven, Conn.
Rogers Works, Inc., J. M., Gloucester City, N. J. Model and Experimental Work See Special Machinery and Tools.

Molding Machines Adams Co., Dubuque, Iowa. Mumford Molding Mch. Co., 1763 Elston Ave., Chi-cago, Ill.

cago, Ill.

Motors, Electric

Eck Dynamo & Motor Co., Belleville, N. J.
General Electric Co., Schenectady, N. Y.
Reliance Elec. & Eng. Co., 1056 Ivanhoe Road, Cleveland, O.
Sprague Electric Works, 527 W. 34th St., New York.
Triumph Electric Co., Cincinnati, O.
Wagner Electric Mig. Co., St. Louis, Mo.
Westinghouse Elec. & Mig. Co., East Pittsburgh, Pa.
Name Plates, Cast Bronze,
Stamped and Etched
Matthews & Co., Jas. H., 3946 Forbes Field, Pittsburgh, Pa.
Newman Mig. Co., Cincinnati, O.
Noble & Westbrook Mig. Co., Hartford, Conn.
Schwerdtle Stamp Co., Bridgeport, Conn.
Nichrome Castings

Schwerdte Stamp Co., Bridgeport, Conn.

Nichrome Castings
Driver-Harris Co., Harrison, N. J.

Nipple Threading Machinery
Bignall & Keeler Mch. Works, Edwardswille, Ill.
Landis Mch. Co., Inc., Waynesboro, Pa.
Merrell Mig. Co., 15 Curtis St., Detroit, Mich.
Murchey Mch. & Tool Co., 34 Porter St., Detroit,
Mich.
Saunders' Sons. D., Yonkers, N. Y.

Mich.
Saunders' Sons, D., Yonkers, N. Y.
Standard Engineering Co., Ellwood City, Pa.
Nuts, Castellated, Etc.
Cincinnati Screw Co., Cincinnati, O.

Nut Tappers See Bolt and Nut Machinery.

Odometers Veeder Mfg. Co., 39 Sargeant St., Hartford, Conn. Veeder Mig. Co., 59 Sargeant St., Hartford, Conn.

Oll Cups
Besly & Co., Chas. H., 120-B N. Clinton St., Chicago,
Ill.
Gits Bros. Mfg. Co., 551 Monroe St., Chicago, Ill.
Tucker, W. M. & C. F., Hartford, Conn.
Winkley Co., Detroit, Mich.

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Ollers, Loose Pulley
Brown Engineering Co., 133 N. 3d Street, Reading, Pa.
Oll Hole Covers
Gits Bros. Mfg. Co., 551 Monroe St., Chicago, Ill.
Tucker, W. M. & C. F., Hartford, Conn.
Winkley Co., Detroit, Mich.
Oll Pans, Sheet Steel
Littleford Bros., Cincinnati, O.

Oils, Lubricating
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Cataract Refining & Mfg. Co., Buffalo, N. Y. Fiske Bros. Refining Co., 24 State St., New York. Haws, Inc., Geo. A., 135 Front St., New York. Hosmer Co., G. A., Buffalo, N. Y. Stuart & Co., Inc., D. A., 29 So. La Salle St., Chicago, Ill.
Swan & Finch Co., 165 Broadway, New York.

Swan & Finch Co., 165 Broadway, New York.

Olls, Quenching and Tempering
Cataract Refining & Mfg. Co., Buffalo, N. Y.
Fiske Bros. Refining Co., 24 State St., New York.
Haws, Inc., Geo. A., 135 Front St., Twey York.
Stuart & Co., Inc., D. A., 29 So. La Salle St., Chicago,
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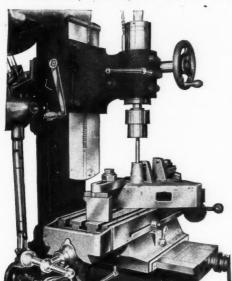
Ovens, Baking
American Gas Furnace Co., 24 John St., New York.

General Electric Co., Schenectady, N. Y.
Rockwell Co., W. S., 50 Church St., New York. Ovens, Tempering
Boker & Co., Inc., H., 101 Duane St., New York,
General Electric Co., Schenectady, New York.

Oxygen Linde Air Products Co., 42nd St. Bldg., New York. Linde-Air Products Co., 42nd St. Bldg., New Y Packings, Leather Graton & Knight Mfg. Co., Worcester, Mass. Swan & Finch Co., 165 Broadway, New York. Pans, Shop and Lathe New Britain Mch. Co., New Britain, Conn. Parallels Walker Co., O. S., Worcester, Mass.

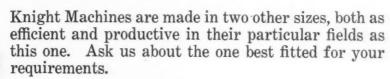
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Oliver Machinery Co., 7 Coldbrook St., Grand Rapids,

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Patterns, Wood and Metal Grant Mfg. & Mch. Co., N. W. Station, Bridgeport,

Mehl Mch. Tool & Die Co., Roselle, N. J. S-P Mfg. Co., Cleveland, O.

Pencils, Drawing
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Underwood & Co., H. B., Philadelphia, Pa.

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Bignall & Keeler Mch. Works, Edwardsville, Ill.
Curtis & Curtis Co., 8 Garden St., Bridgeport, Conn.
Foote-But Co., Clereland O.
Greenfield Tap & Die
Harrington, Son & Co., Inc., Edwin, Philadelphia, Pa.
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Harrington, Son & Co., Inc., Edwin, Philadelphia, Pa.
Harrington, Son & Co., Inc., Waynesboro, Pa.
Murchey Mch. Co., Inc., Waynesboro, Pa.
Murchey Mch. & Tool Co., 34 Porter St., Detroit,
Saunders' Sons, D., Yonkers, N. Y.
Saunders' Sons, D., Yonkers, N. Y.
Saunders' Boniseering Co., Elwood City, Pa.
Tradwell Engineering Co., Easton Pa.
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Tradwell Co., Woxbury, Mass.
Victor Tool Co., Waynesboro, Pa.
Walworth Mfg. Co., Boston, Mass.
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Planer Attachments
Cincinnati Planer Co., Cincinnati, O.
Gray Co., G. A., Cincinnati, O.
Reed-Prentice Co., F. E. Reed Dept. and Prentice
Bros. Dept., Worcester, Mass.

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Planers

American Tool Works Co., Cincinnati, O.
Cincinnati Planer Co., Cincinnati, O.
Cincinnati Planer Co., Cincinnati, O.
Cincinnati Shaper Co., Cincinnati, O.
Cleveland Planer Works, 3150-3152 Superior Ave.,
Cleveland, O.
Gray Co., G. A., Cincinnati, O.
Hamilton Machine Tool Co., Hamilton, O.
Morton Mfg. Co., Muskegon Heights, Mich.
Niles-Bement-Pond Co., 111 Broadway, New York.
Ohio Machine Tool Co., Kenton, O.
Sellers & Co., Inc., Wm., Philadelphia, Pa.
Whitcomb-Blaisdell Mch. Tool Co., Worcester, Mass.
Wilson Mch. Co., W. A., Rochester, N. Y.
Woodward & Powel Planer Co., Worcester, Mass.

Planers, Portable

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Morton Mfg. Co., Muskegon Heights, Mich.
Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,
Philadelphia, Pa.
Underwood & Co., H. B., Philadelphia, Pa.

Planers, Rotary
Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,
Philadelphia, Pa.
Niles-Benent-Pond Co., 111 Broadway, New York.
Pedrick Tool & Mch. Co., 3639 N. Lawrence St.,
Philadelphia, Pa.
Underwood & Co., H. B., Philadelphia, Pa.

Plate Rolls Niles-Bement-Pond Co., 111 Broadway, New York. Plates, Steel
Moltrup Steel Products Co., Beaver Falls, Pa.

Pneumatic Tools
Independent Pneumatic Tool Co., Chicago, Ill.
Ingersoll-Rand Co., 11 Broadway, New York.
Keller Pneumatic Tool Co., Fond du Lac, Wis.
Manning, Maxwell & Moore, Inc., 119 W. 40th St.,
New York.

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Polishing Machines
Abbott Ball Co., Elmwood, Hartford, Conn.
Besly & Co., Chas. H., 120-B N. Clinton St., Chicago, Ill.
Bridgeport Safety Emery Wheel Co., Inc., Bridgeport, Conn.
Brown & Sharpe Mfg. Co. Providence, R. I.
Builders Iron Foundry Co., Providence, R. I.
Builders Iron Foundry Co., Providence, R. I.
Forbes & Myers, 178 Union St., Worcester, Mass.
Gardner Mch. Co., Beloit, Wis.
Goodell-Pratt Co., Greenfield, Mass.
Hisey-Wolf Mch. Co., Cincinnati, O.
New Britain Mch. Co., New Britain, Conn.
Ransom Mfg. Co., Oshkosh, Wis.
Royersford Fdry. & Mch. Co., 54 N. 5th St., Philadelphia, Pa.
Safety Emery Wheel Co., Springfield, O.
Sterling Grinding Wheel Co., Tiffin, O.
Stow Mfg. Co., Binghamton, N. Y.
United States Electrical Tool Co., 6th Ave. and Mt.
Hope St., Cincinnati, O.
Wells & Son Co., F. E., Greenfield, Mass.
Portable Tools, Repair, Railroad, Etc.

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Newman Mfg. Co., Cincinnati, O.
Pedrick Tool & Mch. Co., 3639 N. Lawrence St., Philadelphia, Pa.
Underwood & Co., H. B., Philadelphia, Pa.
Underwood & Co., B., Philadelphia, Pa.
Underwood & Co., W. H., 12 Oregon St., Wilkes-Barre, Pa.

Barre, Pa.

Pulley Turning and Boring Macl.
American Tool Works Co., Cincinnati, O.
Niles-Bement-Pond Co., 111 Broadway, New Mass.

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Presses, Broaching
Ams Mch. Co., Max, Bridgeport, Conn.
Atlas Press Co., 323 N. Park St., Kalamazoo, Mich.
Bliss Co., E. W., 5 Adams St., Brooklyn, N. Y.
Ferracute Mch. Co., Bridgeton, N. J.
Hydraulic Press Mg. Co., 8 t Lincoln
Glead, O.
Metalwood Mfg. Co., Detroit, Mich.
Watson-Stillman Co., 192 Fulton St., New York.

Hydraulic Press Mg. Co., Petroit, Mich.
Swaine Mg. Co., Petroit, Mich.
Swaine Mg. Co., F. J., St. Louis, Mo.
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Fulflo Pump Co., Cincinnati, O.
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Presses, Drop. See Hammers, Drop.

Presses, Foot and Screw
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Etna Mch. Co., Toledo, O.
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Niagara Mch. & Tool Works, Buffalo, N. Y.
Royersford Fdry. & Mch. Co., 54 N. 5th St., Philadelphia, Pa.
Shuster Co., F. B., New Haven, Conn.
Swaine Mfg. Co., E. J., St. Louis, Mo.
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Presses, Forging

Ams Mch. Co., Max, Bridgeport, Conn.
Bethlehem Steel Co., South Bethlehem, Pa.
Bliss Co. E. W., 5 Adams St., Brooklyn, N. Y.
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Toledo Mch. & Tool Co., Toledo, O.
Treadwell Engineering Co., Easton, Pa.

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Presses, Hydraulic
Chambersburg Engineering Co., Chambersburg, Pa.
Elmes Engineering Works, Chas. F., 222 N. Morgan
St., Chicago, Ill.
Hydraulic Press Mfg. Co., 84 Lincoln Ave., Mt.
Gliead, O. Metalwood Mfg. Co., Detroit, Mich.
Metalwood Mfg. Co., Detroit, Mich.
Niles-Bement-Fond Co., 111 Broadway, New York.
Sellers & Co., Inc., Wm., Philadelphia, Pa.
Treadwell Engineering Co., Easton, Pa.
Watson-Stillman Co., 192 Fulton St., New York.

Presses, Power Forcing
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Automatic Mch. Co., Bridgeport, Conn.
Baird Mch. Co., Bridgeport, Conn.
Bigs-Watterson Co., Cleveland, O.
Bliss Co., E. W., 5 Adams St., Brooklyn, N. Y.
Buckeye Engine Co., Salem, O.
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Swaine Mg. Co., F. J., St. Louis, Mo.,
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West Tire Setter Co., Rochester, N. Y.

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Hydraulic Press Mfg. Co., 84 Lincoln Ave., Mt.
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Morse Twist Drill & Mch. Co., New Bedford, Mass.

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Cleveland Mch. & Mfg. Co., 4944 Hamilton Ave.,

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Eric Foundry Co., Eric, Pa.

Ferracute Mch. Co., Bridgeton, N. J.

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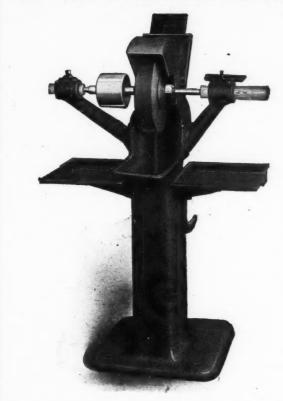
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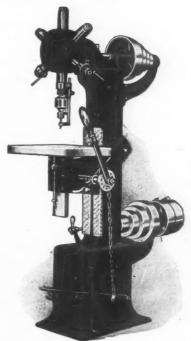


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Morse Twist Drill & Mch. Co., New Bedford, Mass. land, O. Morse Twist Drill & Mch. Co., New Bedford, Mass. Hjorth Lathe & Tool Co., Boston, Mass. Wells & Son Co., F. E., Greenfield, Mass.

crews, Cap and Set llen Mg. Co., Hartford, Conn. (ammacher, Schlemmer & Co., 4th Ave. and 13th St.,

Allen Mfg. Co., Harder & Co., 4th Ave Hammacher, Schlemmer & Co., 4th Ave New York. National Acme Co., Cleveland, O. Toledo Screw Products Co., Toledo, O.

National Actine Co., Ceverand, O.

Screws, Machine
Allen Mg. Co., Hartford, Conn.
Hammacher, Schlemmer & Co., 4th Ave. and 13th St.,
New York.
National Acme Co., Cleveland, O.
Toledo Screw Products Co., Toledo, O.
Screws, Special Lead, Feed, Etc.
Automatic Mch. Co., Bridgeport, Conn.
Second-hand Machinery, Etc.
Biggs-Watterson Co., Cleveland, O.
Brownell Machinery Co., Providence, R. I.
Cincinnati Planer Co., Cincinnati, O.
Davis Mch. Tool Co., Inc., Rochester, N. Y.
Davis Mch. Tool Co., W. F., 32 N. Clinton St.,
Chicago, Ill.
Federal Mchy. Sales Co., 14 N. Jefferson St., Chicago,
Ill.
Frasse & Co., Inc., Peter A., 417 Canal St., New York.
Ceir Co. Robert for Washington St. Brooklyn N. Y.

Ill.

Fig. 1. Fig. 1.

Hill, Clarke & Co., Inc., Boston, Mass.
Hill, Clarke & Co., of Chicago, 625 Washington Blvd.,
Chicago, Ill.
Hudson Motor Car Co., Detroit, Mich.
Marshall & Huschart Mchy. Co., 17 S. Jefferson St.,
Chicago, Ill.
McDonough Mfg. Co., Eau Claire, Wis.
McShane Bell Foundry Co., Baltimore, Md.
Motch & Merryweather Mchy. Co., Cleveland, O.
New Jersey Mchy. Exchange, Newark, N. J.
Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,
Philadelphia, Fa.
Hiladelphia, Fa.
Philadelphia, Fa.
Hers-Bement-Fond Co., 111 Broadway, New York.
Patterson Tool & Supply Co., Dayton, O.
Prentiss & Co., Inc., Henry, 149 Broadway, New York.
Puffer Mfg. Co. Winchester, Mass.
Riverside Machinery Depot. Detroit, Mich.
Simmons Mch. Co., 1001 Singer Bldg., New York.
Standard Metal Mfg. Co., Newark, N. J.
Strong, Homer, Rochester, N. Y.
Union Switch & Signal Co., Swissvale, Pa.
Vandyck Churchill Co., 149 Broadway, New York.
Worthington Pump & Mchy. Corp., 115 Broadway, New
York.
York,
Corley & Dolan, Inc., 115 Broadway, New
York.
Separators, 011 and Steam

Separators, Oil and Steam Nickolson & Co., W. H., 112 Oregon St., Wilkes-Barre, Pa.

Satte, ra.

Set Screws, Safety
Allen Mig. Co., Hartford, Conn.
Bristol Co., Waterbury, Conn.
Hammacher, Schlemmer & Co., 4th Ave. and 13th St.,
New York.
Standard Pressed Steel Co., Philadelphia, Pa.

Shafting, Steel

Blum & Co., Julius, 510 W. 24th St., New York.
Brown Co., A. & F., 79 Barclay St., New York.
Cresson-Morris Co., Philadelphia, Pa.
Standard Pressed Steel Co., Philadelphia, Pa.

Cresson-Morns Co., Finiaceipina, 1a.
Standard Pressed Steel Co., Philadelphia, Pa.

Shapers

American Tool Works Co., Cincinnati, O.
Cincinnati Shaper Co., Cincinnati, O.
Cochrane-Bly Co., Rochester, N. Y.
Davis Mch. Tool Co., Inc., Rochester, N. Y.
Gould & Eberhardt, Newark, N. J.
Hendey Mch. Tool Co., Torington, Conn.
Kelly Co., R. A., Xenia, O.
Morton Mfg. Co., Muskegon Heights, Mich.
Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,
Philadelphia, Pa.
Niles-Bement-Pond Co., 111 Broadway, New York.
Ohio Machine Tool Co., Kenton, O.
Potter & Johnston Mch. Co., Fawtucket, R. I.
Smith & Milis Co., Cincinnati, O.
Springfield Mch. Tool Co., 631 Southern Ave., Springfield, O., John, Cincinnati, O.
Shapers, Vertical
Ingersol-Rand Co., 11 Broadway, New York.
Pratt & Whitney Co., Hartford, Conn.
Shears, Rotary

Pratt & Whitney Co., Hartford, Conn.

Shears, Rotary

Bliss Co., E. W., 5 Adams St., Brooklyn, N. Y.

Niagara Mch. & Tool Works, Buffalo, N. Y.

Toledo Mch. & Tool Co., Toledo, O.

Shears, Squaring

Erie Foundry Co., Erie, Pa.

Sheet Metal Work

Littleford Bros., Cincinnati, O.

Sheet Metal Working Machinery,

(See Presses)

Savage Co., Inc., W. J., Knoxville, Tenn.

Shell Making Machinery

(See Presses)
Savage Co., Inc., W. J., Knoxville, Tenn.
Shell Making Machinery
Thurlow-Steel Works, Inc., Philadelphia, Pa.

Thurlow-Steel Works, Inc., Philadeiphia, Fa.

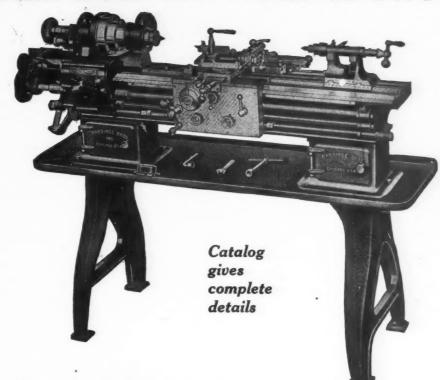
Slide Rests

National Acme Co., Cleveland, O.
Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,
Philadelphia, Pa.
Niles-Bement-Fond Co., 111 Broadway, New York.
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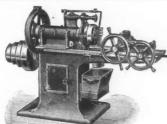
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Taylor-Shantz Co., Charrison, N. J.
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Treadwell Engineering Co., Easton, Ps.
Ulmer Co., J. C., Cleveland, O.
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Fox Gun Co., A. H., Philadelphia, Pa.
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Matthews & Co., Jas. H., 3946 Forbes Field, Pittsburgh, Pa.
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Noble & Westbrook Mfg. Co., Hartford, Conn.
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Bethlehem Steel Co., South Bethlehem, Pa.

Blum & Co., Julius, 510 W. 24th St., New York.

Boker & Co., Jun., H., 101 Duane St., New York.

Camden Forge Co. Camden, N. J.

Colonial Steel Co., Pittsburgh, Pa.

Firth-Sterling Steel Co., McKeesport, Pa.

Frasse & Co., Inc., Peter A., 417 Canal St., New York.

Halcomb Steel Co., Syracuse, N. Y.

Hawkridge Bros. Co., Boston, Mass.

Heller Bros. Co., Newark, N. J.

Lesson & Sons. Inc., Wm., 91 John St., New York.

Jessop & Sons, Inc., Wm., 91 John St., New York.
Johnston & Jennings Co., Addison Road and Lake
Shore R. R. Tracks, Cleveland, O.
Latrobe Electric Steel Co., Latrobe, Pa.
Standard Alloys Co., Pittsburgh, Pa.
Vunadium-Alloys Steel Co., Pittsburgh, Pa.
Vulcan Crucible Steel Co., Aliquippa, Pa.

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-Harris Co., Harrison, N. J. Driver Driver-Harris Co., Harrison, N. J.

Steel, High Speed, Tool

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Boker & Co., Inc., H., 101 Duane St., New York.
Colonial Steel Co., Hittaburgh, Pa.
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Hawkridge Bros. Co., Boston, Mass.
Jessop & Sons, Inc., Wm., 91 John St., New York.
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Standard Alloys Co., Pittsburgh, Pa.
Standard Gauge Steel Co., Beaver Falls, Pa.
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Yanadium-Alloys Steel Co., Aliquippa, Pa.
Yulcan Crucible Steel Co., Aliquippa, Pa.
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Etc.
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New Britain men. Co., Stellite Haynes Stellite Co., Kokomo, Ind. Stocks, Die See Taps and Dies.

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Caborundum Co., Niagara Falls, N. Y.
Norton Co., Worcester, Mass.
Vitrified Wheel Co., Westfield, Mass.

Stools, Steel
See Furniture, Shop and Drafting-room.
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Morse Twist Drill & Machine Co., New Bedford, Mass
Niles-Benent-Pond Co., 111 Broadway, New York.
Shuster Co., F. B., New Haven, Conn.

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Excelsior Needle Co., Torrington, Conn.

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General Electric Co., Schenectady, N. Y.
Westinghouse Elec. & Mfg. Co., East Pittsburgh, Pa.
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Bristol Co., Waterbury, Conn.
Brown Instrument Co., Philadelphia, Pa.
Veeder Mfg. Co., 39 Sargeant St., Hartford, Conn.
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Keuffel & Esser Co., Hoboken, N. J.
Starrett Co., L. S., Athol, Mass.
Ulmer Co., J. C., Cleveland, O.
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Bicknell-Thomas Co., Greenfield, Mass.
Cincinnati Bickford Tool Co., Oakley, Cincinnati, O.
Errington Mechanical Laboratory, 39 Cortlandt St.,
New York.
Geometric Tool Co., New Haven, Conn.
Hammond Mfg. Co., Cleveland, O.
Leland-Ginford Co., Worcester, Mass.
Modern Tool Co., and and State Sts., Erie, Pa.
Newman Mfg. Co., Cincinnati, O.
Peter Bros. Mfg. Co., 135 Railroad Ave., Algonquin,
III. P<sub>1</sub> nier, Wm. L., 549 Washington Blvd., Chicago, Ill. Ill. Quint, A. E., Hartford, Conn. Wells & Son Co., F. E., Greenfield, Mass. Whitney Mfg. Co., Hartford, Conn.

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Garvin Mch. Co., Spring and Varick Sta., New York.
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Hammond Mfg. Co., Cleveland, O.
Harrington, Son & Co., Inc., Edwin, Philadelphia, Pa.
Harris Engineering Co. H. E., Bridgeport, Conn.
Langelier Mfg. Co., Providence, R. I.
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Peter Bros. Mfg. Co., 135 Railroad Ave., Algonquin,
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Chicago, III.

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Butterfield & Co., Derby Line, Vt.

Card Mig. Co., S. W., Mansfield, Mass.

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Errington Mechanical Laboratory, 39 Cortlandt St.,

New York.

Geometric Tool Co., New Haven, Conn.

Greenfield Tap & Die Corp., Greenfield, Mass.

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Reed Mfg. Co., Erie, Pa.
Reiff & Nestor, Lykens, Pa.
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Saunders' Sons, D., Yonkers, N. Y.
Stnadard Tool Co. Cleveland, O.
Walworth Mfg. Co., Boston, hiass.
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Metalwood Mig. Co., Detroit, Mich.

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Bickford Machine Co., Greenfield, Mass.
Boston Gear Works, Norfolk Downs, Mss.
Geometric Tool Co., New Haven, Conn.
Greenfield Tap & Die Corp., Greenfield, Mass.
Lees-Bradner Co., Cleveland, O.
National Mchy. Co., Tiffin, O.
Newton Mch. Tool Works, Inc., 23rd and Vine Sts.,
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Pratt & Whitney Co., Hartford, Conn.
Rivett Lathe & Grinder Co., Brighton, Boston, Mass.
Wells & Son Co., F. E., Greenfield, Mass.

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Newton Mch. Tool Works, Inc., 23rd and Vine Sts.
Philadelphia, Pa.

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Gisholt Mch. Co., Madison, Wis.
Harrington, Son & Co., Inc., Edwin, Philadelphia, Pa.
Lees-Bradner Co., Cleveland, C.
Newton Mch. Tool Works, Inc., 23d and Vine Sts.,
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Pratt & Whitney Co., Hartford, Conn.
Smalley-General Co., Bay City, Mich.
Taft-Peirce Mfg. Co., Woonsocket, R. I.
T. C. M. Mfg. Co., Harrison, N. J.
Waltham Mch. Works, Waltham, Mass.

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Tire Welders and Benders Williams, White & Co., Moline, Ill.

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Hammacher, Schlemmer & Co., 4th Ave. and 13th St.,
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Starrett Co., L. S., Athol, Mass.
Union Tool Chest Works, 10 Railroad St., Rochester,
N. Y.
Wedell & Boers, Detroit, Mich.

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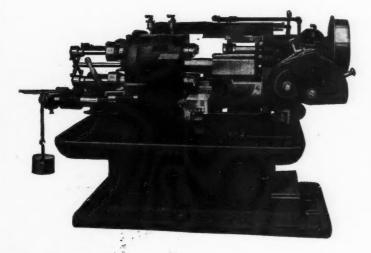
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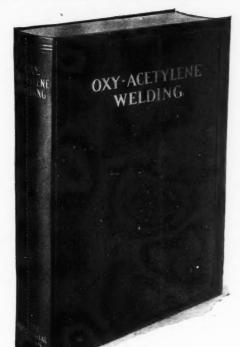
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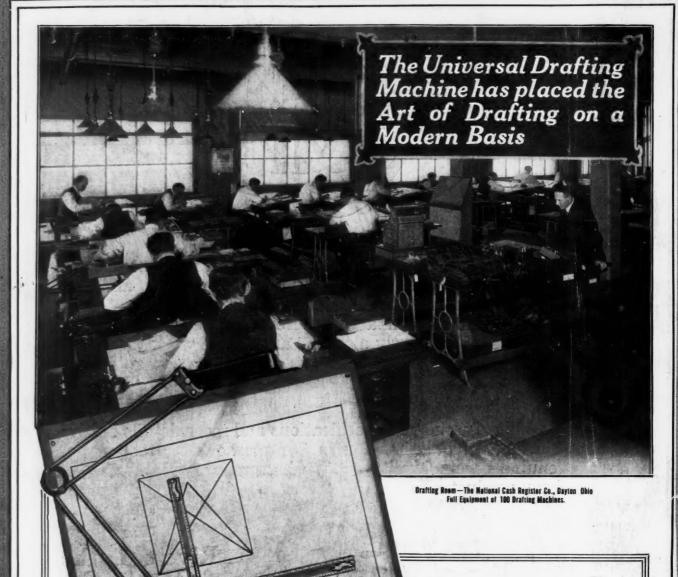
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